## AECENAR

Association for Economical and Technological Cooperation in the Euro-Asian and North-African Region


Institute for Chemical Process Technology (ICPT) http://aecenar.com/institutes/icpt

# Air Liquefaction and Cryogenics - Report 1 (2021) Part I: Basics 

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Filter dryer:122

So the refrigerant enters through the inlet, it passes across the spring, then surrounds the outside of the solid core. The refrigerant then passes through the solid core and as it does so the dirt, moisture and acids are absorbed, the refrigerant then collects in the groove at the centre of the core and then pass through the screen. It then passes through the perforated plate and exits the unit having been filtered and dried, it then continues to the expansion valve. ..... 122


R-22

- Nomenclature:

Chlorodifluoromethane

- Symbol: $\mathrm{CHClF}_{2}$
- Boiling point : $\mathrm{T}=-40.7^{\circ} \mathrm{C}(232.5 \mathrm{~K}) @$ 1 bar
$\mathrm{T}=4.9^{\circ} \mathrm{C}(278.05 \mathrm{~K})$ @ T .8 bar
$\mathrm{T}=45.6^{\circ} \mathrm{C}(318.75 \mathrm{~K}) @$ $\quad 4.8 \mathrm{bar}$
$\mathrm{T}=45.6^{\circ} \mathrm{C}(318.75 \mathrm{~K}) @$. 16.3 bar
thane

SIKLUS REFRIGERASI
(REFRIGERATION CYCLE)




126

| Number | Ozone Friendly | Uses | Chemical Components | Alternatives | Notes |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R410A <br> HFC | Yes | Designed for new R22 applications, but can <br> also be used to retrofit R13b1 systems. | HFC 125-50\% HFC 32-50\% |  |  |
| R500 <br> CFC | No; banned under <br> Montreal protocol | Low temperature R12 CFC. | CFC 12-CFC 115 - | R401b; R407d |  |
| replacement for R502 / R22 Low GWP |  |  |  |  |  |

CFCs: Chlorofluorocarbons. These products have ceased production within the RSA for internal consumption with effect from 1996.
HCFCs: Hydrochlorofluorocarbons. Full availability within the RSA, and the present production phase out date is 2015. There is a widespread belief that this will be reduced to 2005 within the next 2-3 years.
HFCs: Hydrofluorocarbons. At the moment there is no production phase out date for HFCs and there is unrestricted use on their applications. HCs \& NH3: This product group mainly used in industrial equipment due to flammability concerns.


## R-502 (High stage)

- Nomenclature:

Chlorodifluoromethane, Chloropentafluoroethane

- Symbol: CHC1F2, CC1F2CF3
- Compress: 375 psi $=25.85$ bar
- Boiling point :
$\mathrm{T}=-45.6^{\circ} \mathrm{C}(227.4 \mathrm{~K}) @ 1$ bar $\mathrm{T}=61.5^{\circ} \mathrm{C}$ (334.7 K) @ 25.85 bar


## R-503 (Low stage)

- Nomenclature: Azeotropic Blend
- Symbol: CHF3
- Compress: 375 psi $=25.85$ bar
- Boiling point :
$\mathrm{T}=-88.9^{\circ} \mathrm{C}$ (184.1 K ) @ 1 bar
$\mathrm{T}=-20^{\circ} \mathrm{C}(253.2 \mathrm{~K}) @ 25.85 \mathrm{bar}$


The cascade refrigeration system consists of a low-temperature loop (Low stage) and a high-temperature loop (high stage) ..... 130
Each stage consists of a compressor, condenser, expansion valve and evaporator ..... 130
The high stage condenser is cooled by air cooled, while the low stage condenser is cooled by the high stage evaporator ..... 130
So the high stage evaporator acts as a coolant for the pressurized refrigerant in the low stage ..... 130
Advantages of a cascade cooling system: ..... 130
- Repair is easy ..... 130
- The Cascade refrigeration allows to low-temperature operation. ..... 130- You can reduce the use of power up to $10 \%$ with the help of cascade refrigeration.130


## Basic Components



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طاتة الشسـلال
North Lebanon Alternative Power www.nlap-lb.com
Liquefaction of air(oxygen)

Process of purification and liquefaction of
air:


In this process at first air is filtered \& compressed to 6.8 atm in turbo compressor. During the compression cooling is done to maintain the

After compression the air is divided into two streams. One is $65 \%$ stream \& the other is $35 \%$, now the larger stream is then passed through after cooler and heat exchanger where it is cooled to $-150^{\circ} \mathrm{C}$ to $-170^{\circ} \mathrm{C}$ by the incoming pure nitrogen \& waste nitrogen streams produced from rectification columns.
The smaller stream is passed through reciprocating compressor to increase the pressure to about 200atm. Here the air temp is maintained at $4-8^{\circ} \mathrm{C}$ by intermediate cooling between stages using cold water obtained by ammonia refrigeration.
Then the air goes through high pressure heat exchanger where the temp of air is brought down to about $-120-140^{\circ} \mathrm{C}$. Now the air undergoes expansion to about 6.5 atm in the expansion engine.
The temperature of air is brought down from -170 to $-174^{\circ} \mathrm{C}$ by joule Thompson effect.
Now the air will be in liquid state \& mixes with the larger stream \& changes the whole air stream into saturated liquid state.
This saturation liquid is fed to Linde rectification column. This column may be single, double or compound depending on requirement. the liquid product coming out will have a purity of about 99.4-99.99\%.
This liquid is partially vaporized in condenser, to liquefy the nitrogen vapor \&the rest may be taken as liquid product or it may be obtained in gaseous state if it is used for cooling of incoming air, the other products that obtained are pure nitrogen of purity above $98 \%$ \& waste nitrogen product of purity of about 92-96\%.

 become still colder).
 heat is exchanged with the environment.

- The low pressure gas is now at its coolest in the current cycle Some of the gas may condense and become output product.
The low pressure gas is directed back to the countercurrent heat exchanger to cool the warmer, incoming, high-pressure gas.
After leaving the countercurrent heat exchanger, the gas is warmer than it was at its coldest, but cooler than it started out at step 1.
The gas is sent back to the compressor to make another trip through the cycle (and



## 2 Cryogenic air plant principle

A cryogenic air plant is an industrial facility that creates molecular oxygen at relatively high purity. Air is the most common element in the earth's crust and the second largest industrial gas.

### 2.1 Purpose

The cryogenic air separation achieves high purity oxygen of more than $99.5 \%$. The resulting high purity product can be stored as a liquid and/or filled into cylinders. These cylinders can even be distributed to customer in the medical sector, welding or mixed with other gases and used as breathing gas for diving. Typical production ranges from 50 normal $\mathrm{m}^{3} /$ hour up to $860,000 \mathrm{Nm}^{3} /$ hour

### 2.2 Plant modules



A cryogenic air plant comprises:

- Warm end (W/E) container
- Compressor
- Air receiver
- Chiller (Heat exchanger)
- Pre-filter
- Air purification unit (APU)
- Coldbox
- Main heat exchanger
- Boiler
- Distillation column

Cryogenic air plant principle

```
Expansion brake turbine
- Storage
Liquid oxygen tank
Vaporizer
Filling station
```


### 2.2.1 Annotated diagram


a) Water wash cooler; b) Reversing heat exchanger; c) Expansion turbine; d) Double column rectifier; e) Condenser; f) Subcooler; g) Adsorber; h) Compressor; i) Filter

- Raw materials
- Basis: 1000kg Oxygen (95\%)
- Air $=3600 \mathrm{Nm}^{3}$
- Steam $=1750 \mathrm{~kg}$
- Cooling water $=5000 \mathrm{~kg}$
- Electricity $=450-480 \mathrm{kWH}$


### 2.3 Linde's Method of liquefaction of gases. 1

The Hampson-Linde cycle or the Linde's liquefaction process is used by coupled with regenerative cooling and the Joule Thomson effect.

By this method, we can easily liquefy air, and many other gases too.


Linde's Method of Liquefaction of Gases - Howtrending.com

The above figure is Linde's method for Liquefaction of Air and some other gases too.

By this figure, you can understand that liquefaction of air or those gases that have a low value of critical temperatures is hard, as compared to those that have high critical temperature values.

### 2.3.1 About this apparatus

1. In this method, two compressors $\mathrm{C}_{1}$ at (25 atm pressure) and $\mathrm{C}_{2}$ (200 atm pressure) are used.
2. Heat exchangers $R_{1}$ and $R_{2}$ are used into which cold water and a freezing mixture is used as a refrigerant.
3. A Liquid solution of KOH (Potassium Hydroxide), that is required to get pure air.
4. Two chambers $E_{1}$ and $E_{2}$, and $P_{1}$ and $P_{2}$ are the two small nozzles.
5. At last, the liquid air is collected into a Dewar flask.

### 2.3.2 Principle

Linde's process of liquefaction is work on the principle of the Joule Thomson effect coupled with regenerative cooling.

### 2.3.3 Linde's process Working

This method is quite different as we compared to the previous one, the Cascade method.

First, the air is pumped at a pressure of 25 atm into the spiral tube. The air gets cooled after passing through the $\mathrm{R}_{1}$ heat exchangers. Here the gas becomes cool because of cool water inside the R1 heat exchangers. This cooled air then passes through a liquid solution of Potassium hydroxide (KOH).

The reason for the use of the KOH solution is that air contains many gases and water vapors too. To separate air from water vapors this solution is used, and also this solution absorbs $\mathrm{CO}_{2}$ gas from the air (The Critical temperature of water = $374{ }^{\circ} \mathrm{C}$ ). After this, the air further moves in the second compressor $\mathrm{C}_{2}$.

In the $\mathrm{C}_{2}$ compressor, the air is pumped at a pressure of 200 atm into the next spiral tube. Now the gas becomes cool again, after passing through the second heat exchangers $\mathrm{R}_{2}$. Here the gas-cooled because of the Freezing mixture inside the $\mathrm{R}_{2}$ heat exchangers.

Now the temperature of this air decreases to around $-20^{\circ} \mathrm{C}$. Then this pre-cooled air is allowed to expand through nozzle $P_{1}$ in a chamber $E_{1}$ and suffers the Joule Thomson effect. Due to this effect, more cooling is produced into the chamber $E_{1}$, and pressure reduces to about 50 atm .

This cooled air then returns back to the compressor $\mathrm{C}_{2}$ and where it again pumped at a pressure of 200 atm into the spiral tube. This air again suffers Joule Thomson effect, and more cooling produced in chamber $\mathrm{E}_{1}$.

Repeating some cycles of this process, more and more cooling is produced in chamber $\mathrm{E}_{1}$. After getting sufficient temperature, the cooled air is allowed to expand through nozzle $\mathrm{P}_{2}$ in chamber $\mathrm{E}_{2}$ and again suffers the Joule Thomson effect, and pressure reduces to about 1 atm .

Now the temperature decreases to around $-188^{\circ} \mathrm{C}$ in chamber $\mathrm{E}_{2}$ and the air gets liquefied. This liquefied air is collected into the Dewar flask.

Also, in chamber $\mathrm{E}_{2}$ the un-liquefied air is returned back to the compressor $\mathrm{C}_{1}$, this further cooled the air, and where it again pumped at a pressure of 25 atm into the spiral tube.

This is the overall Linde's process for liquefaction of air.

### 2.4 Claude's method of liquefaction of gases

Claude's process works on the same principle as Linde's process. Hence cooling of the air, or if we say liquefaction of gases is carried out by the help of the Joule Thomson effect.

But, the only difference between Linde Claude's process of liquefaction of air, or other gases is that in Claude's process there is an isentropic expansion.

That's why Claude's process is more efficient than Linde's process.

The principle used in Claude's Process
Claude's method works on two principles.
First, the Joule Thomson effect.
Second is a mechanical expansion (By, the use of an expansion turbine).

What is an expansion turbine or the turboexpander?
"The expansion turbine or the turboexpander is an axial-flow or centrifugal turbine, through which a high pressurized gas is allowed to expand to produce work. This work is used to rotate a shaft, which is often connected with a compressor or generator.

Due to the turbo-expander, the outcoming gas has a very low temperature as compared to the temperature of input gas. This is because, in this process, the work is done by the gas, and due to this the gas loses its kinetic energy and resulting in a decrease in temperature of the gas".

Working of Claude's process

As you know Claude's process is modified Linde's process, Therefore, like Linde's process, the gas which is at 200 atm pressure is pumped into the spiral tube, the gas then moved further. In Claude's process, this gas is divided into two sections. In the first section, the gas is allowed to expand through the expansion turbine (turbo-expander). In the second section, the gas is allowed to suffers the Joule Thomson effect.

Therefore, more cooling is produced inside the chamber. One is by turbo-expander, and the second is by the Joule Thomson effect. The overall process is repeated until the gas gets liquefied completely, and during each cycle of repetition, the un-liquefied gas is returned back to the Compressors.

The very low critical temperature of $\mathrm{H}_{2}$, and He
Now I will discuss the very low values of critical temperatures for gases like Neon, Hydrogen, and the Helium gas.

The Critical temperature ( $\mathrm{T}_{\mathrm{c}}$ ) values of these gases are
Neon (Ne) $\quad=-228.7^{\circ} \mathrm{C}$
Hydrogen $\left(\mathrm{H}_{2}\right)=-240^{\circ} \mathrm{C}$
Helium (He) $=-267.8^{\circ} \mathrm{C}$
For liquefying these, we need a very low-temperature range. The hydrogen and helium must be kept below their inversion temperature while suffers the Joule Thomson effect.

The principle used in Hydrogen and Helium's liquefaction.
Liquefaction of Hydrogen and helium works on the principle of the Joule-Thomson effect coupled with regenerative cooling.

Cryogenic air plant principle
In the liquefaction of Hydrogen, liquid air is used as a refrigerant, and in the liquefaction of Helium, Liquid hydrogen is used as a refrigerant.

By the use of previous processes, we can get liquefied Hydrogen and helium too.
https://www.sciencedirect.com/science/article/abs/pii/S0140700701000032

## 3 Large Scale Factory study

### 3.1 Overview

| Factory |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Equipment | Details | Price per unit | Total Price |  |
|  | Filter per year | unit per week | ~10\$ | $\sim 20 \$$$\sim$ |  |
|  | Air Compressor (364.5 KW) |  | ~ 2500 \$ |  |  |
|  | Air Receiver (Pre-Cooler) | unit ( $300 \mathrm{~L}, 0.8 \mathrm{Mpa}$ ) | 200\$ |  | قابل للتصنيع |
|  | Chiller |  |  |  |  |
|  | Air Purification Unit (13x Zeolite) | Stainless stell ( 710 Kg ) | 710\$ | 1707.4 \$ |  |
|  |  | Brazed Aluminum fins (1) | 10\$ |  |  |
|  |  | Aluminun ( 195 kg ) | 390\$ |  |  |
|  |  | Lagging (2.45\$/m2) | 29.4\$ |  |  |
|  |  | Bed packed with 13x Zeo | 520 \$ |  |  |
|  |  | Column (4 columns) | 48\$ |  |  |
| $\begin{aligned} & \text { 자 } \\ & \text { © } \\ & \text { O} \end{aligned}$ | Main Heat Exchanger |  | 3869 406.9\$ | 3869 406.9\$ | مذكور بpdf دراسة (المشروع |
|  |  |  | 1000\$-5500\$ | 1000 \$-5500\$ | حسب موقع درانح |
|  | Expansion Brake Turbine | Absorber Column (stains | 180\$ | 196\$ |  |
|  |  | Adsorption (Aluminum) | 16\$ |  |  |
|  |  | turbine ( 40 KW ) | 19300 \$ |  |  |
|  | Cryogenic Distillation column |  | 386562.4 \$ | 386562.4 \$ | قابل للتصنيع |
|  |  | HP Tower | $\begin{gathered} 499000 \$ \\ 1250000 \$ \\ 904000 \$ \end{gathered}$ | 2653000 \$ | ref: Study_Dynamic Design of a Cryogenic Air Separation Unit |
|  |  | LP Tower Crude Argon Tower |  |  |  |
|  | Boiler |  |  |  |  |
|  |  | Liquid Oxygen Tank |  |  |  |
| $\stackrel{\square}{0}$ | Cylinder 50L ( 50 \$/piece) | Liquid Nitrogen Tank |  |  |  |
| $\stackrel{\sim}{*}$ |  | Liquid Argon Tank |  |  |  |

### 3.2 Dynamic design of a cryogenic air separation unit (Source?)

|  | ASU will produce (per day) |  |
| :---: | :---: | :---: |
|  | Oxygen (99.5\%) | 1500 metric tons |
|  | Nitrogen (99.5\%) | 5000 metric tons |
|  | Argon | 58 metric tons |
|  | Total Annual Cost |  |
|  | Compressor capital cost | 16500000 \$ |
|  | Venture guidance appraisal | 118500000 \$ |
|  | Worth of products (Sell) | 113900000 \$ |
|  | Annual cost for equipment and utilities | 39000000 \$ |
|  | Yield yearly profit | 73400000 \$ |

### 3.3 Total annual cost of plant equipment

Large Scale Factory study

| Total annual cost of Plant Equipment |  |  |  |
| :---: | :---: | :---: | :---: |
| Equipment | Capital Cost (\$) | Utility Costs (\$) |  |
| Air receiver |  |  |  |
| Air Compressor | ~ 2500 \$ | ~ 850 \$ |  |
| Chiller |  | 0\$ |  |
| Air purification unit |  |  |  |
| Main heat exchanger | 1000\$-5500\$ |  |  |
| Distillation column |  |  |  |
| Reboiler/condenser | 1041000 \$ | 0\$ | ref: Study_Dynamic Design of a Cryogenic Air Separation Unit |
| Turbine |  |  |  |
| Pumps |  |  |  |
| Controls |  |  |  |

### 3.4 Costs of modules

### 3.4.1 Air receiver tank



- Filter

Prix pas cher De Chine Approvisionnement Commercial Et Industriel De Qualité Alimentaire Mini Haute


Produits de commerce électronique
10,00 \$US-50,00 \$US/ Unite
1 Unité (Commande minimum)

Guangzhou Jielv Environment Technology Co., Ltd. > $\qquad$ CN 3 YRs

$131 \nabla$
$\Rightarrow 93.9 \%$ Taux de réponse US $\$ 440,000+$ in 81 Transaction (s)
Contacter le fournisseur (i) Leave Messages $\square$ Comparer

### 3.4.2 Air/Oxygene Compressor

## Choice 1:

https://toplongcompressor.en.made-in-china.com/product/IvVmtGBbhyhA/China-5nm3-3stage-High-Pressure-Oil-Free-Oxygen-Compressor-Nitrogen-Compressor.html


ค

5nm3 3stage High Pressure Oil Free Oxygen Compressor Nitrogen Compressor

| Get Latest Price > |  |
| :--- | :--- |
| Min. Order / Reference FOB Price |  |
| 1 Piece | US $\$ 6,500-8,000 /$ Piece |
| Port: | Shanghai, China © |
| Production Capacity: | 200PCS/Month |
| Payment Terms: | L/C, T/T, D/P, Western Union, Paypal, Money Gram |
| Lubrication Style: | Oil-free |
| Cooling System: | Air Cooling |
| Cylinder | Balanced Opposed Arrangement |
| Arrangement: | Vertical |
| Cylinder Position: | Closed Type |
| Structure Type: | Multistage |

Product Description
Oil-free Special Gas Compressor

Oil-free special gas compressor booster is the kind of semi-hermetic compressor, it adopts hermetic construction for its motor without pollution to the medium to be compressed and without leakage. This series compressor has numerous advantage of reliable performance, simple operation, compact construction, quick connection and so on. It can be applied in the compression and recovery of toxic, rare and precious gas such as SF6, helium, methane, ammonia, Freon, carbon dioxide and so on.

Performance Characteristics

Oil free high pressure oxygen nitrogen helium Co 2 gas compressor
Principle 1: Oil-free type reciprocating piston
2 Cooling Type: Air-cooled or water-cooled
(3) Power consumption: $\leq 110 \mathrm{kw} 4$ Speed: . 300-560rpm

5 Flow. . 52000 Nm3 / h6
Suction pressure: . 0-5Mpa7
Exhaust pressure: . $\leq 16.5 \mathrm{Mpa} 8$ Compression Level: $1-4$ Winds oil-free compressors
Product Features: No oil lubrication with clean and non-polluting.
High efficiency, low energy consumption. High reliability, continuous 24 -hour operation. The unit uses air-cooled or water-cooled, compact structure, operation and low maintenance cost

All our models can be customized. For more information, pleaes do not hesitate to contact.

| Model | gas | inlet barg | outlet barg | flow rate NM3/hr | power.KW | voltage/frequency | inlet/outlet.mm | cooling way | net eight.kg | dimension.mm | pressure riato stage |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GOWW-4-10/4-150 | oxygen | 3-4 | 150 | 4-10 | 3 | $\begin{array}{\|l} 220 / 380 \\ / 440 / 50 / 60 / 3 \end{array}$ | DN15/M16X1.5 | air cooling | 380 | 1300X750X1000 | 3stage |
| GOWW-11-20/4-150 | oxygen | 3-4 | 150 | 11-20 | 4-7.5 | $\begin{aligned} & 220 / 380 \\ & / 440 / 50 / 60 / 3 \end{aligned}$ | DN15/M16X1.5 | air cooling | 420 | 1300X750X1000 | 3stage |

## Choice 2:

https://www.alibaba.com/product-detail/BROTIE-oxygen-
compressor 1600122723363.html?spm=a2700.galleryofferlist.topad classic.d image.35d821f d7VGM2u

BROTIE oxygen compressor

FOB Reference Price: Get Latest Price

$\mathbf{\$ 6 , 5 0 0 . 0 0} \mathbf{- \$ 1 0 , 0 0 0 . 0 0} /$ Set 1 Set/Sets (Min. Order)

Power
3-22kw
Warranty: 1 Year for machinery warranty 1 Year for Core Components (1)
Shipping: Support Express - Sea freight - Land freight - Air freight
Lead Time:

| Quantity(Sets) | $1-100$ | $>100$ |
| :--- | :--- | :--- |
| Est. Time(days) | 30 | Negotiable |

## Overview

## Quick Details

Applicable Industri... Garment Shops, Building Material Shops, Manufacturing Plant.
Local Service Locat...United Kingdom, United States, Germany, Viet Nam, Philippine.
Condition: New, New

Configuration: PORTABLE
Lubrication Style: Oil-free
Place of Origin: China
Model Number: $\quad 02-3 / 4-150,02-5 / 4-150,02-10 / 4-150,02-15 / 4-150,02-20 / 4 \ldots$
Dimension $\left(L^{*} W^{*} H\right)$ : customized
Certification: ISO
After-sales Service ...Field installation, commissioning and training
Air capacity: $\quad 3-75 \mathrm{Nm} 3 / \mathrm{h}$
Video outgoing-ins... Provided
Warranty of core co... 1 Year
Gas Type: oxygen
Flow Capacity: $\quad 3,5,10,15,20,25,30,40,50,75 \mathrm{Nm} 3 / \mathrm{h}$
Inlet Pressure: 4bar
Outlet Temperature: 50C
Outlet Size: $\quad 8-15 \mathrm{~mm}$
Lubrication: no oil lubricated

### 3.4.3 Main Heat exchanger



## Overview

## Quick Details

Applicable Industri... Hotels, Garment Shops, Building Material Shops, Machinery R...
Local Service Locat...None
Video outgoing-ins... Provided
Marketing Type: New Product 2021
Core Components: Pressure vessel
Place of Origin: China
Structure: Tube Heat Exchanger
Maximum Working ... 10MPa
Weight: 500-2500KG
Certification: ce
After-sales Service ... Video technical support, Online support
Key Selling Points: Competitive Price
Application: Cooling
Material: SS201
Tube material: S20100

After Warranty Serv... Video technical support, Online support, Spare parts
Showroom Location: None
Machinery Test Re... Provided
Warranty of core co... 1 Year
Condition: New
Brand Name: XINREN

| Liquid Flow Rate: | Max $75 \mathrm{M} 3 / \mathrm{h}$ |
| :--- | :--- |
| Voltage: | $220 \mathrm{~V} / 50 \mathrm{~Hz}$ |

Dimension( $\left.\mathrm{L}^{*} \mathrm{~W}^{*} \mathrm{H}\right)$ : CUSTOMIZED
Warranty: 1 Year
Working Temperatu...-100-370 ${ }^{\circ} \mathrm{C}$
Product Name: FINNED TUBE Heat Exchanger
Type: Fin
Name: finned tube heat exchanger
Fin material: $\quad$ AISI 201

|  | value |
| :--- | :--- |
| Applicable Industries | Hotels, Garment Shops, Building Material Shops, Machinery Repair <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> Restaurant, Home Use, Retail, Food Shop, Printing Shops, <br> Construction works, Energy \& Mining, Food \& Beverage Shops, <br> Advertising Company |

### 3.4.4 Distillation column tower


vertical pressure vessel distillation column towers

FOB Reference Price: Get Latest Price
$\mathbf{\$ 1 0 , 0 0 0 . 0 0} \mathbf{- \$ 9 0 0 , 0 0 0 . 0 0} /$ Set $1 \mathrm{Set} /$ Sets (Min. Order)


### 3.4.5 Industrial oxygen generator (whole system)



Pure oxygen generator industrial oxygen generator
FOB Reference Price: Get Latest Price
$\mathbf{\$ 8 , 0 0 0 . 0 0 - \$ 2 0 0 , 0 0 0 . 0 0} /$ Set $\quad 1$ Set/Sets (Min. Order)
Model Number: $\quad$ CBO
Power: $\quad 5-200 \mathrm{~W}$
Samples: $\quad \$ 100.00 /$ Set 1 Set (Min. Order) $\$$ Buy Samples
Warranty: $\quad \mathbf{1}$ Year for machinery warranty $\quad \mathbf{1}$ Year for Core Components (1)

High purity Medical and industrial oxygen generator


FOB Reference Price: Get Latest Price
$\mathbf{\$ 8 , 0 0 0 . 0 0} \mathbf{- \$ 2 0 0 , 0 0 0 . 0 0}$ / Set 1 Set/Sets (Min. Order)

| Model Number: | CBO |  |
| :--- | :--- | :--- |
| Power: | $5-200 \mathrm{~W}$ |  |
| Samples: | $\$ 100.00 /$ Set 1 Set (Min. Order) | Buy Samples |
| Warranty: | $\mathbf{1}$ Year for machinery warranty | $\mathbf{1}$ Year for Core Components (i) |

## Technical Parameters

| Oxygen Capacity | $3-400 \mathrm{Nm} 3 / \mathrm{h}$ |
| :---: | :---: |
| Oxygen Purity | $90 \%-93 \%$ |
| Output Pressure | $0.1-0.3 \mathrm{Mpa}(1-3 b a r)$ adjustable/15Mpa Filling pressure offered |

Oxygen Generator Specification

| Specification | Output ( $\mathbf{N m}^{\mathbf{3} / \mathbf{h})}$ | Effective gas <br> consumption ( $\left.\mathbf{N m}^{\mathbf{3}} \mathbf{/ h}\right)$ | air cleaning system |
| :---: | :---: | :---: | :---: |
| CBO-5 | 5 | 0.95 | $\mathrm{KJ}-1$ |
| CBO-10 | 10 | 2.1 | $\mathrm{KJ}-2$ |
| CBO-20 | 20 | 4.0 | $\mathrm{KJ}-6$ |
| CBO-40 | 40 | 8.2 | $\mathrm{KJ}-10$ |
| CBO-60 | 60 | 12.3 | $\mathrm{KJ}-12$ |
| CBO-80 | 80 | 16.3 | $\mathrm{KJ}-20$ |
| CBO-100 | 100 | 20.8 | $\mathrm{KJ}-20$ |
| CBO-150 | 150 | 30.7 | $\mathrm{KJ}-30$ |
| CBO-200 | 200 | 41 | $\mathrm{KJ}-40$ |

## 4 Process Flow Brief Description

## Process Flow Brief Description


4.1 ملخص_الهواء في حالة سائلة
4.2 نظرة عامة

محرك دورة الهواء السائل (LACE) هو نوع من محركات دفع المركبات الفضائية التي تحاول زيادة كفاءتها من خلال جمع جزء من مؤكسده من الجو. يستخدم محرك دورة الهواء السائل وقود الهيدروجين السائل (LH2) لتسييل الهواء . في صاروخ الأكسجين السائل / الهيدروجين السائل ، يكون الأكسجين السائل (LOX) اللازم للاحتراق هو الجزء الأكبر من وزن المركبة الفضائية عند الإقلاع ، لذلك إذا كان من المككن جمع بعض هذا من الهواء في الطريق ، فقد يحدث ذلك
 تمت دراسة LACE إلى حد ما في الولايات المتحدة الأمريكية خلال أواخر الخمينيات وأوائل الستينيات ، وفي أواخر عام 1960 ، كان لاى ماركوارت نظام اختبار يعمل. ومع ذلك ، عندما انتقلت ناسا إلى كبسولات بالستية خلال مشروع ميركوري ، اختفى تمويل البحث عن المركبات المجنحة ببطء ، ويعمل LACE معها

اللسائل الأي تم الحصول عليه عن طريق خفض درجة حرارة الهواءء ويسمى الهواء المسال في القانون. 1895 يقوم CPGRvon Linde بالضغط على الهواء وتوسيعه ، مما تسبب في انخفاض درجة حرارة الهواء تأثير جول طومسون باستخدام الهواء تمييع بالإضافة إلى ذلك ، جعل G. Claude الإنتاج الضخم الصناعي مدكنًا. في الآونة الأخيرة ، تم طرح سوائل نيتروجين الهواء في السوق التي تضغط غاز الهيليوم ثم تقوم بتوسيعه لإنشاء درجة حرارة منخفضة واستخدامه لتسييل الهواء. الجهاز صغير ومفيد مع القليل من القوى العاملة. الهواء اللائل عبارةٍ عن سائل أنرق فاتح ، وهو مزيجج من (لنيتروجين السائل) نقطة الغليان
77.3 كيلو ، الثقل النوعي 0.810) والأكسجين السائل (نقطة الغليان K 90.17، الثقل النوعي 1.144) ، الثقل النوعي حوالي 1 ، نقطة الغليان حوالي -190 Co . إذا تم السماح للهواء السائل بالوقوف ، فإن النيتروجين السائل ذو نقطة الغليان المنخفضة والضنظ الجزئي العالي يتم تبخيره أولاً ، ويزداد تركيز الأكسجين اللسائل في الهواء السائل. الاستفادة من هذه الخاصية ، يتم إرفاق برج تجزئة بوحدة تسييل النيتروجين في الهواء لفصل واستخدام النيتروجين السائل. من الناحية الصناعية ، يتم استخذام كمية كبيرة . من الهواء السائل لفصل الأكسجين المستخدم في صناعة الصلب والنيتروجين المستخدم في تخليق الأمونيا الأرجون ، اللنيون ، الخ الغاز النبيل يستخدم أيضا بشكل منفصل عن الهواء السائل. لا ينبغي أن يكون الهواء اللسائل على اتصال مباشل مع المواد القابلة للاشتعال ، وخاصة المذيبات العضوية القابلة للاشتعال مثل الكحول والإيثر وثاني أكسيد الكربون والأسيتون والمساحيق العضوية القابلة للاشتعال مثل (لسكر والنافثالين والكافور . وذلك لأن هذه المواد العضوية تتأكسد مرة واحدة وخطر الانفجار كبير. كان الهواء السائل عبارة عن مادة تجميد نموذجية في المختبر ، ولكن الآن يتم استخذام النيتروجين السائل الذي لا ينفجر ، ونادراً ما يستخذم الهواء السائل والأكسجين السائل. ومع ذلك ، فإن الأكسجين السائل )الحرارة (الكامنة 6820 (J / mol والهواء السائل الني يحتوي على الكثير منه أقل عرضة للتبخر من النيتروجين السائل (الحرارة الكامنة 5577 (J / mol ، لذلك فهو مناسب للاستخدام كمبرد طويل الأمد 2 .

يتم سائله عن طريق ضغط الهواء عند درجة حرارة منخفضة -140 درجة مئوية أو أقل. السائل السائل مع طفيف مزرق. درجة الغليان عند حوالي 1.1 الضغط الجوي حوالي -190 درجة مئوية. تستخدم في تجارب درجات الحرارة المنخفضة للحصول على الأكسجين والنيتروجين باستذدام الفرق في نقاط الغليان3 .
https://www.atlascopco.com/ar-eg/compressors/wiki/compressed-air-articles/what-is-nitrogen

## 5.1

https://www.atlascopco.com/ar-eg/compressors/wiki/compressed-air-articles/generating-nitrogen-membrane

| الإمتزاز بالصّفط المتأرجح (PSA) | غتالئى |  |
| :---: | :---: | :---: |
| كفاء |  |  |
| أعلى | عالثه20 | الكفاءs |
|  |  | الأداع مقابل درجةّ الحرارة |
| هتّوبط | 0نخفضن |  |
| من大亏ض | منخفتة | كتافة، الصبالة |
| دخل/خزج هنَّلب |  |  |
| دخل/خرج هنَّلّ | تَابِّ |  |
|  | نَّوبٌ | - |
|  | لا لا |  |
|  |  |  |
|  |  | مستّوى الصنوضناء |
| هنّوبط |  | الونة |



Parameters of Liquefaction of Oxygen

## 6 Parameters of Liquefaction of Oxygen

### 6.1 Properties of Oxygen

Vapour pressure curves of atmospheric gases


FLUID PROPEJTIES
HEF: IMBS TM No. 36, p. 41

| moperties | Liquid hydrogen | Iiquid witrogen | Water | Oxygen | Freon-12 | Freon-22 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Heat of Vaporization (cal./gr.) | 106.5 | 47.6 | 586 | 50.8 | 43.5 | 55.9 |
| Vapor Pressure (mmilg) | 760 | 760 | 18.8 | 760 | 760 | 760 |
| Nolecular Weight (gr./gr.mole) | 2 | 28 | 18 | 32 | 137.4 | 86.5 |
| Specific Volume (cc/gr.) | 14.1 | 1.24 | 1.00 | 0.871 | 0.673 | 0.706 |
| Temperature ( ${ }^{\circ} \mathrm{K}$ ) | 20 | 77 | $\left(70^{\circ} \mathrm{F}\right)$ | 90.13 | 297 | 232 |
| $C_{p}$ - Specific Heat (cal./sr. ${ }^{\circ} \mathrm{K}$ ) | 2.3 | 0.49 | 1.00 | 0.405 | 0.210 | 0.255 |
| Viscosity (centipoises) | 0.0130 | 0.158 | 0.98 | 0.190 | 0.429 | - - |



Table 11.1 Candidate refrigerant fluids

|  | Critical <br> pressure <br> $($ bar $)$ | Critical <br> temp. <br> $(K)$ | Saturation <br> temp. <br> @ 1.0 bar <br> $(K)$ | Latent <br> heat <br> $(\mathrm{kJ} / \mathrm{kg})$ | Gas <br> constant <br> $(\mathrm{kJ} / \mathrm{kg} \mathrm{K})$ | Ratio <br> $(30 / \mathrm{CV}$ <br> $(300 \mathrm{~K})$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Fluid | 50.9 | 154.77 | 90.18 | 212.3 | 0.2598 | 1.396 |
| Oxygen | 50.0 | 150.86 | 87.29 | 159.6 | 0.2082 | 1.670 |
| Argon | 50.0 | 77.35 | 197.6 | 0.2968 | 1.404 |  |
| Nitrogen | 33.96 | 126.25 | 27.09 | 86.1 | 0.4117 | 1.640 |
| Neon | 26.54 | 44.40 | 2.37 | 434.0 | 4.157 | 1.410 |
| Hydrogen | 12.76 | 32.98 | 20.27 | 21.0 | 2.075 | 1.662 |
| Helium | 2.3 | 5.25 | 4.2 |  |  |  |

Parameters of Liquefaction of Oxygen
Table 1 Properties of Principal Cryogens

| Name | Normal Boiling Point |  |  | Critical Point |  | Triple Point |  | Reference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $T$ (K) | Liquid Density $\left(\mathrm{kg} / \mathrm{m}^{3}\right)$ | Latent Heat ( $\mathrm{J} / \mathrm{kg} \cdot \mathrm{mole}$ ) |  |  |  |  |  |
|  |  |  |  | $T(\mathrm{~K})$ | $P(\mathrm{kPa})$ | $T(\mathrm{~K})$ | $P(\mathrm{kPa})$ |  |
| Helium | 4.22 | 123.9 | 91.860 | 5.28 | 227 |  |  | 1 |
| Hydrogen | 20.39 | 70.40 | 902,300 | 33.28 | 1296 | 14.00 | 7.20 | 2, 3 |
| Deuterium | 23.56 | 170.0 | 1,253,000 | 38.28 | 1648 | 18.72 | 17.10 | 4 |
| Neon | 27.22 | 1188.7 | 1,737,000 | 44.44 | 2723 | 26.28 | 43.23 | 5 |
| Nitrogen | 77.33 | 800.9 | 5,579,000 | 126.17 | 3385 | 63.22 | 12.55 | 6 |
| Air | 78.78 | 867.7 | 5,929,000 |  |  |  |  | 7, 8 |
| Carbon monoxide | 82.11 | 783.5 | 6,024,000 | 132.9 | 3502 | 68.11 | 15.38 | 9 |
| Fluorine | 85.06 | 1490.6 | 6,530,000 | 144.2 | 5571 |  |  | 10 |
| Argon | 87.28 | 1390.5 | 6,504,000 | 151.2 | 4861 | 83.78 |  | 11, 12, 13 |
| Oxygen | 90.22 | 1131.5 | 6,801,000 | 154.8 | 5081 | 54.39 | 0.14 | 6 |
| Methane | 111.72 | 421.1 | 8,163,000 | 190.61 | 4619 | 90.67 | 11.65 | 14 |
| Krypton | 119.83 | 2145.4 | 9,009,000 | 209.4 | 5488 | 116.00 | 73.22 | 15 |
| Nitric oxide | 121.50 | 1260.2 | 13,809,000 | 179.2 | 6516 | 108.94 |  |  |
| Nitrogen trifluoride | 144.72 | 1525.6 | 11,561,000 | 233.9 | 4530 |  |  |  |
| Refrigerant-14 | 145.11 | 1945.1 | 11,969,000 | 227.7 | 3737 | 89.17 | 0.12 | 16 |
| Ozone | 161.28 | 1617.8 | 14,321,000 | 261.1 | 5454 |  |  |  |
| Xenon | 164.83 | 3035.3 | 12,609,000 | 289.8 | 5840 | 161.39 | 81.50 | 17 |
| Ethylene | 169.39 | 559.4 | 13,514,000 | 282.7 | 5068 | 104.00 | 0.12 | 18 |

### 6.2 Liquefaction Methods of gases

## طرُق إسالة الغازات Liquefaction Methods of Gases



عملية الإسالة عكس عملية التبخير

- إن عملية التنييل معاكسة لعملية التبخير.

ـ تـتمد عملية الإسالة على طبيعة الغغاز فأبخرة المواد التي تكون سائلة في أو قرب درجة حرارة الغرفة والضغط الجوي تتكثف بسهولة بالتبريد.

- و أما المواد التي تكون سائلة في درجات حرارة منخفضة فإنها تتكثف إما بو اسطة الضغط أو بالضغط والتبريد.
- قد وجد أن الضغط وحده لا يكفي لتسبيل غازات مـينـة مثّل مـا يعرف بـالغازات الائمة
 درجات حرارة حرجة منخفضة جداً، ولكن بـالضغط العالي وتبريدها الى درجات حرارة أدنى

- يوجد لكل غاز درجة حرارة لا يمكن إسـالتّه فوقها مهمـا زاد الضغظ وتعرف هذا الارجة بدرجة الحرارة الحرجة critical temperature والضغط الحرج critical pressure هو الضغط اللازم لإسالة الغاز عند درجةٌ الحرارة الحرجة للفاز .
-الجدول التالي يمثّل درجات الحرارة الحرجة و الضغط الحرج لبعض الغغازات: قيم (P, V, and T) عند النقطة الحرجة. الغازات هرتبة حسب الكتل الجزينية

| الغاز | Pc, atm | Vc Liters/mol | Ic, K |
| :---: | :---: | :---: | :---: |
| $\mathrm{H}_{2}$ | 12.8 | 0.070 | 33.3 |
| He | 2.26 | 0.062 | 5.3 |
| $\mathrm{CH}_{4}$ | 45.6 | 0.099 | 190.2 |
| $\mathrm{NH}_{3}$ | 112.2 | 0.072 | 405.6 |
| $\mathrm{H}_{2} \mathrm{O}$ | 217.7 | 0.056 | 647.2 |
| CO | 35.0 | 0.090 | 134.4 |
| Ne | 26.9 | 0.044 | 44.8 |
| $\mathrm{N}_{2}$ | 33.5 | 0.090 | 126.0 |
| NO | 65 | 0.058 | 179 |
| $\mathrm{O}_{2}$ | 49.7 | 0.074 | 154.4 |
| $\mathrm{CH}_{3} \mathrm{OH}$ | 78.5 | 0.118 | 515.1 |
| HCl | 81.6 | 0.087 | 324.6 |
| Ar | 48.0 | 0.076 | 150.7 |
| $\mathrm{CO}_{2}$ | 72.8 | 0.094 | 304.2 |
| $\mathrm{SO}_{2}$ | 77.7 | 0.123 | 430.4 |
| $\mathrm{n}-\mathrm{C}_{2} \mathrm{H}_{12}$ | 33.0 | 0.310 | 470.3 |
| $\mathrm{Cl}_{2}$ | 76.1 | 0.124 | 417 |
| $\mathrm{C}_{6} \mathrm{H}_{6}$ | 47.9 | 0.256 | 561.6 |
| Kr | 54.3 | 0.107 | 209.4 |
| Xe | 57.9 | 0.120 | 289.8 |

Lind-Hampson’s الطريقة الأولى لتسييل الغازات: طريقة ليند و هامبسون 6.2.1.1 Method
-تتتمد طريقة ليند و هامبسون على تأتير جول- طومسون والآي ينص على أنه: عندما يسمح لأي غغز موجود تحت ضغط عال بالتمدد المفاجيء في منطقة ذات ضغط منخفض، فإن درجة حرارته سوف تنخفض. ويبرد الغاز بسبب حقيقة أنـه أثناء التمدل سوف تستغل الطاقة الحركية للغاز المتمدد في التظلب على قوى التجاذب بين الجزيئات حيث أن الغاز يقوم بشغل داخلي .
-الأشكال التالية توضح الجهاز الأي استخدمه ليند في إسالة الهواء :


Parameters of Liquefaction of Oxygen
لذا نستّيع تُبيل الأكسجين وذلك بالثتمدد المفاجئ للغاز المضغوط تـحت ضغوط عالية ممـا ينتّج عنه انخفاضاً في درجة حرارة ذللك الغاز .

## خطوات العمل 4

6.3
(1) ينقّى الأكسجين المراد ثبّريده من ثُاني أكسيد الكربون CO2 والمواد العضويـة والرطوبـة.
(2) يضتخ الأكسجين في أنبوبة حلزونية (جهاز ضغط Compressor)حيث يضغط إلى

ضغط حوالي (2 50 bar (لمسب الجدول المذكور أعلاه]
 ولمـا كان الغرض من هذه العملية تخفيض درجة الحرارة وليس زيـادتها فإن هذا الأكسجين الذي ارثنفعت درجة حرارتّه يتم التخلص من حرارتـه حيث يمرر في مبادل حراري (أنابيب نحاسبة حلّونية مبردة) لتخفيض درجة الحرارة. حيث [<150 K] (<-123º$C)$ تصل درجة تبريده إلى حوالـي
(4) حيّث يمرر هذا الأكسجين في أنبوب حلزوني (c) ينّهى بفو هةٌ صغيرة جاً لينتهي بالْمحيط ذي الضغظ المنخفض (الغرفة D) ليصل ضغطها إلى حوالى (1 atm) وذلك
 حرارة غاز الأكسجين الى حوالي (183ºC- ) أو أدنى [ حالةّ الأكسجين السائل ] .
(5) يمرر الأكسجين الذي تم تبريده بهذه الطريقة مرة ثـانية فوق الحلزونـات النحاسبية (C) وبهذه الطريقّة سوف يؤدي الى تّبريد الغاز الداخل الى درجةّ أقلّ حتى قبيل تمدده.
(6) بـد إتمام الاورة عدةٌ مرات (يعود اللى الضاغطة compressor) تـعاد العملية مرة ثانية وثالثة ...الخ حتى الوصول الى الضّغ ودرجة الحرارة الحرجين حيث يتحول الى
 السـائل سوف يتدفق عبر الصمـام (V) أمـا الأكسجين الذي لم يتكثف بعد، فِإنه يعاد مرة ثثاتبية الى جهاز الضغط حيث تكتمل الاورة .


Figure 9.6 Linde liquefaction process

## 7 Static Analysis

At the start of the first cycle, the oxygen gas passes from the oxygen inlet towards the compressor at the ambient temperature ( $300 \mathrm{~K}, 1 \mathrm{bar}$ ), through the mixer. It is at this stage that the mixer plays the role of the tank. The oxygen gas comes out hot from the compressor ( $400 \mathrm{~K}, 50 \mathrm{bar}$ ) in the direction of cooling in order to reduce the temperature of the compressed oxygen gas ( $280 \mathrm{~K}, 50 \mathrm{bar}$ ). Then the chilled oxygen gas goes to the heat exchanger, and here and in the first gas cycle the gas is not cooled through the heat exchanger due to the vacuum of the heat exchanger from the cold refrigerant gas. The compressed gas exits the heat exchanger with the cooling temperature ( $280 \mathrm{~K}, 50 \mathrm{bar}$ ) towards the throttle. In the throttle, the compressed gas ( $280 \mathrm{~K}, 50$ bar) passes through a small aperture, allowing the gas to expand and expand suddenly and expand causing a sudden drop in pressure (from 50 bar to 1 bar) accompanied by a sudden drop in the temperature of the oxygen gas. The table below shows the temperature change before and after the throttle (at the outlet of the heat exchanger).

| \# of <br> cycle | He at exchanger |  |  | Throttling | $\Delta \mathbf{t}(\mathbf{K )}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | T inlet (K) | T outlet (K) | H outlet (kJ/Kg) | T outlet (K) |  |
| 1 | 280 | 280 | 240.71 | 265 | 15 |
| 2 | 280 | $\sim 270$ | 230.55 | 255 | 15 |
| 3 | 280 | $\sim 260$ | 220.23 | 245 | 15 |
| 4 | 280 | $\sim 250$ | 209.78 | 231 | 19 |
| 5 | 280 | $\sim 237.5$ | 196.5 | 216.8 | 20.7 |
| 6 | 280 | $\sim 227.5$ | 185.55 | 204 | 23.5 |
| 7 | 280 | $\sim 210$ | 165.67 | 183 | 27 |
| 8 | 280 | $\sim 190$ | 140.79 | 156 | 34 |
| 9 | 280 | $\sim 165$ | 100.4 | 107.5 | 57.5 |
| 10 | 280 | $\sim 155$ | 62.646 | 90.062 | 64.94 |

Note: The temperature change at the outlet of the heat exchanger (throttle inlet) occurs due to the temperature change of the cold oxygen gas entering the heat exchanger.

When oxygen is out of the throttle, it goes directly to the separator. At 90 K , oxygen is in a mixture of a gas and a liquid. And oxygen is in a gas state with a temperature higher than 90 K , while it is in a liquid state with a temperature below 90 K . The separator has two outlets, one for liquid oxygen and the second for gas oxygen. Liquid oxygen exits from the outlet of the first separator to the tank, while the oxygen gas exits, at a temperature of approximately 90 K , from the outlet of the second separator towards the mixer, passing through the heat exchanger. The cold oxygen gas coming out from the separator plays an important role in cooling the hot gas entering the heat exchanger
(leaving the coolant) towards the throttle. After the cold gas passes through the heat exchanger, its temperature is heated up (about 220 K ) and then it reaches the mixer where it is mixed with the oxygen gas coming from the oxygen inlet.

### 7.1 Schema of Linde-Hampson liquefaction cycle of Oxgene with example values



## ENTROPY (kJ/kg-K)



Fig. 5.30. $T-S$ diagram for oxygen ( $T=50-300 \mathrm{~K}$ )

### 7.2 Drawing by FreeCad

Linde.FCStd

### 7.3 Detailes of calculation

- Thermodynamic properties of Oxygen with variation of pressure and temperature

$1 \rightarrow 2$ isothermal compressor
$3 \rightarrow 4$ Isenthalpic expansion
$2 \rightarrow 3^{\prime}, g \rightarrow 1$ isobaric heat exchange
$2 \rightarrow 3^{\prime}, g \rightarrow 1^{\prime}$ heat exchange (actual)

We choose 90 K as temperature of boiling point (see table above)

| Thermodynamic | Unit | $\mathrm{P}=1 \mathrm{bar}=0.1 \mathrm{Mpa}$ |  | $\mathrm{P}=50 \mathrm{bar}=5 \mathrm{Mpa}$ |  | $\mathrm{P}=100 \mathrm{bar}=10 \mathrm{Mpa}$ |  | $\mathrm{P}=200 \mathrm{bar}=20 \mathrm{Mpa}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Properties of Oxygen |  | T=90 K | $\mathrm{T}=300 \mathrm{~K}$ | T=90 K | $\mathrm{T}=300 \mathrm{~K}$ | $\mathrm{T}=90 \mathrm{~K}$ | $\mathrm{T}=300 \mathrm{~K}$ | $\mathrm{T}=90 \mathrm{~K}$ | T=300 K |
| Enthalpy | kJ/Kg | -133.69 | 272.71 | -131.04 | 260.88 | -128.28 | 249.39 | -122.61 | 229.99 |
| Entropy | kJ/Kg.K | 2.9383 | 6.4163 | 2.9202 | 5.3679 | 2.9029 | 5.1561 | 2.8712 | 4.9208 |

Note: The mass flow $\dot{\mathrm{m}}=2.75 \mathrm{Kg} / \mathrm{s}$ is an approximated value, a change in this value will affect Q-dot as well as mif and thus yield Y .

- In steady state conditions, the first Law around the compressor gives:

$$
\dot{\mathbf{W}} \mathrm{c}-(\mathrm{Q}-\mathrm{dot}) \mathrm{r}+\dot{\mathrm{m}}(\mathrm{~h} 1-\mathrm{h} 2)=0
$$

The second Law around the compressor gives:

$$
(\mathrm{Q}-\mathrm{dot}) \mathrm{r}=\dot{\mathrm{m}} \mathrm{~T} 1(\mathrm{~S} 1-\mathrm{S} 2)
$$

Combining, we have:

$$
\begin{array}{r}
\dot{\mathbf{W}} \mathrm{c}=\dot{\mathrm{m}}[\mathrm{~T} 1(\mathrm{~S} 1-\mathrm{S} 2)-(\mathrm{h} 1-\mathrm{h} 2)] \\
\\
=(\mathrm{Q}-\mathrm{dot}) \mathrm{r}-\dot{\mathrm{m}}(\mathrm{~h} 1-\mathrm{h} 2)
\end{array}
$$

Or $(\mathrm{Q}-\mathrm{dot}) \mathrm{c}=\dot{\mathrm{m}}(\mathrm{h} 1-\mathrm{h} 2)$

- Applying the $1^{\text {st }}$ Law around everything except the compressor gives:

$$
\begin{aligned}
\dot{\mathrm{m}}(\mathrm{~h} 1-\mathrm{h} 2) & =\dot{\mathrm{m} f}(\mathrm{~h} 1-\mathrm{hf}) \\
& \rightarrow \dot{\mathrm{mf}}=\frac{\dot{\mathrm{m}}(\mathrm{~h} 1-\mathrm{h} 2)}{\mathrm{h} 1-\mathrm{hf}}
\end{aligned}
$$

- Defining yield, $\mathrm{y}=\frac{\dot{\mathrm{m}} f}{\dot{\mathrm{~m}}}=\frac{h 1-h 2}{h 1-h f}$
- $\mathrm{FOM}=\frac{(h 1-h 2)(T 1-T c)}{[T 1(S 1-S 2)-(h 1-h 2)] T c}$

Thus, the table below contains the results of calculation with variation of pressure

| Pesure $\mathbf{P}$ | Unit | $\mathbf{1}$ bar $\boldsymbol{\rightarrow} \mathbf{5 0}$ bar | $\mathbf{1}$ bar $\boldsymbol{\rightarrow} \mathbf{1 0 0}$ bar | $\mathbf{1}$ bar $\boldsymbol{\rightarrow} \mathbf{2 0 0}$ bar |
| :---: | :---: | :---: | :---: | :---: |
| Gas mass flow rate $\dot{\mathbf{m}}$ | $\mathbf{K g} / \mathbf{s e c}$ | $\mathbf{2 . 7 5}$ | $\mathbf{2 . 7 5}$ | $\mathbf{2 . 7 5}$ |
| Heat transfer of compressor Qr | $\mathrm{kJ} / \mathbf{s e c}$ | 864.93 | 1039.665 | 1233.7875 |
| Heat transfert of evaporator Qc | $\mathrm{kJ} / \mathrm{sec}$ | 32.532 | 64.13 | 115.995 |
| Work transfert compressor W -dot | $\mathrm{kJ} / \mathbf{s e c}$ | 832.3975 | 975.535 | 1117.7925 |
| Liquid mass flow rate $\dot{\mathbf{m} f}$ | $\mathbf{K g} / \mathbf{s e c}$ | $\mathbf{0 . 0 8 0 0 5}$ | $\mathbf{0 . 1 5 7 8}$ | $\mathbf{0 . 2 8 5 4 2}$ |
| Yield Y |  | 0.02911 | 0.0573 | 0.10379 |
| FOM |  | $\mathbf{0 . 0 9 1 1 1}$ | $\mathbf{0 . 1 5 3 2 4}$ | $\mathbf{0 . 2 4 1 9 0 3}$ |

### 7.4 Heat exchanger

## - Heat Exchanger Design Process

1. Identify application - Temperature, heat loads, mass flow rates, etc.
2. Decide on construction type.
3. Evaluate LMTD, q and F
4. Determine dimensions.
5. Evaluate heat transfert coefficient on hot side
6. Evaluate heat transfer coefficient on cold side
7. Determine overall heat transfer coefficient.
8. Determine dimensions - iterate
9. Check power consumpltion

### 7.4.1 Calculation of heat exchanger 5

## Notes:

1- U value is taken approximate ( $40 \mathrm{~W} / \mathrm{m}^{2} . \mathrm{K}$ )

[^1]2- A base of inlet and outlet temperature (hot \& cold), the appropriate type of heat exchanger is 2 shells and 4 tubes

## Heat Exchanger



## Cold Side

Fluid $\mathrm{A}: \mathrm{O}_{\mathbf{2}}$ gas, in

## Hot Side

Fluid B: $\mathrm{O}_{\mathbf{2}}$ gas, in
Point 3
$\dot{\mathrm{m}}=2.75 \mathrm{Kg} / \mathrm{sec}$
$\mathrm{P}=50 \mathrm{bar}$
$\mathrm{T}=280 \mathrm{~K}$
Fluid $\mathrm{B}: \mathrm{O}_{2}$ gas, out


[^2]Fluid A: $\mathrm{O}_{2}$ gas, out

```
Point 6
```

Point 6
m}=2.6723 Kg/se
m}=2.6723 Kg/se
P = 1 bar
P = 1 bar
T=250 K

```
T=250 K
```


## Static Analysis

Heat Duty

| 318.56 | kW |
| :---: | :---: |
| U Value |  |
| 40 | $\mathrm{~W} / \mathrm{m}^{2} .{ }^{\circ} \mathrm{K}$ |


| Result |  |  |
| :--- | :--- | :--- |
| Tube Pitch | 106.3500 | mm |
| LMTD | 64.84 | ${ }^{\circ} \mathrm{K}$ |
| Correction Factor (F) | 0.8195 | ${ }^{\circ} \mathrm{K}$ |
| LMTD (Corrected) | 53.14 | $\mathrm{~m}^{2}$ |
| Shell in Series | 149.86 | $\mathrm{~m}^{2}$ |
| Total Area | 74.93 |  |
| Tubea per Shell | 48 | m |
| Shell ID (Estimate) | 0.91 |  |


| 90.06 | ${ }^{\circ} \mathrm{K}$ |
| :--- | :---: |
| Temperature Out |  |
| 220 | ${ }^{\circ} \mathrm{K}$ |


.

| Geometry |  | Tube Pitch | 1206.3500 | mm |
| :---: | :---: | :---: | :---: | :---: |
| Tube Pass |  | LMTD | 64.84 | ${ }^{\circ} \mathrm{K}$ |
| Multiple | $\checkmark$ |  |  |  |
| Tube Length |  | Correction Factor (F) | 0.8195 |  |
| 5 | m | LMTD (Corrected) | 53.14 | ${ }^{\circ} \mathrm{K}$ |
| Tube Outside Diameter (OD) |  | Shell in Series | 2 |  |
| 1200 | mm | Total Area | 149.86 | $\mathrm{m}^{2}$ |
| Tube Pattern |  |  |  |  |
| Square | $\checkmark$ | Area per Shell | 74.93 | $\mathrm{m}^{2}$ |
|  |  | Tubes per Shell | 4 |  |
|  |  | Shell ID (Estimate) | 2.79 | m |

### 7.5 Calculation of compressor

|  | Stage 1 | Stage 2 | Stage 3 | Total |
| :--- | :--- | :--- | :--- | :---: |
| Mass flow rate (Kg/s) | $1.12 \mathrm{E}-03$ | $1.12 \mathrm{E}-03$ | $1.12 \mathrm{E}-03$ |  |
| Pessure ratio | 3 | 4 | 3.6 | 43.5 |
| Pump efficiency | 0.6 | 0.6 | 0.6 |  |
| Input pressure (bar) | 1.18 | 3.56 | 14.25 |  |
| Outlet pressure (bar) | 3.56 | 14.25 | 51.67 | 51.67 |
| Intel density (Kg/m3) | 1.7 | 5.0 | 20.4 |  |
| Pump input power (W) | 265 | 397 | 344 | 1005 |

## - Compressor choice :

## Choice 1:

https://toplongcompressor.en.made-in-china.com/product/IvVmtGBbhyhA/China-5nm3-3stage-High-Pressure-Oil-Free-Oxygen-Compressor-Nitrogen-Compressor.html


Product Description
Oil-free Special Gas Compressor

Oil-free special gas compressor booster is the kind of semi-hermetic compressor, it adopts hermetic construction for its motor without pollution to the medium to be compressed and without leakage. This series compressor has numerous advantage of reliable performance, simple operation, compact construction, quick connection and so on. It can be applied in the compression and recovery of toxic, rare and precious gas such as SF6, helium, methane, ammonia, Freon, carbon dioxide and so on.

Performance Characteristics

Oil free high pressure oxygen nitrogen helium Co 2 gas compressor
Principle 1: Oil-free type reciprocating piston
2 Cooling Type: Air-cooled or water-cooled
(3) Power consumption: $\leq 110 \mathrm{kw} 4$ Speed: . 300-560rpm

5 Flow: . $\leq 2000 \mathrm{Nm} 3$ / h6
Suction pressure: . $0-5 \mathrm{Mpa} 7$
Exhaust pressure: : $\leq 16.5 \mathrm{Mpa} 8$ Compression Level: $1-4$ Winds oil-free compressors
Product Features: No oil lubrication with clean and non-polluting.
High efficiency, low energy consumption. High reliability, continuous 24 -hour operation. The unit uses air-cooled or water-cooled, compact structure, operation and low maintenance cost

All our models can be customized. For more information, pleaes do not hesitate to contact.

| Model | gas | inlet <br> barg | outlet .barg | flow rate NM3/hr | power.KW | voltage/frequency | inlet/outlet.mm | cooling way | net eight.kg | dimension.mm | pressure riato stage |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GOWW-4-10/4-150 | oxygen | 3-4 | 150 | 4-10 | 3 | $\begin{aligned} & 220 / 380 \\ & / 440 / 50 / 60 / 3 \end{aligned}$ | DN15/M16X1.5 | air cooling | 380 | 1300X750X1000 | 3stage |
| GOWW-11-20/4-150 | oxygen | 3-4 | 150 | 11-20 | 4-7.5 | $\begin{aligned} & 220 / 380 \\ & / 440 / 50 / 60 / 3 \end{aligned}$ | DN15/M16X1.5 | air cooling | 420 | 1300X750X1000 | 3 stage |

## Choice 2:

https://www.alibaba.com/product-detail/BROTIE-oxygen-
compressor 1600122723363.html?spm=a2700.galleryofferlist.topad classic.d image.35d821fd7VG
M2u

BROTIE oxygen compressor

FOB Reference Price: Get Latest Price

$\mathbf{\$ 6 , 5 0 0 . 0 0} \mathbf{- \$ 1 0 , 0 0 0 . 0 0} /$ Set 1 Set/Sets (Min. Order)

| Power: |  |  | $3-22 \mathrm{kw}$ |
| :--- | :--- | :--- | :--- |
| Warranty: | 1 Year for machinery warranty | 1 Year for Core Components (1) |  |
| Shipping: | Support Express - Sea freight - Land freight - Air freight |  |  |
| Lead Time: | Quantity(Sets) | $1-100$ | $>100$ |
|  | Est. Time(days) | 30 | Negotiable |

## Overview

## Quick Details

Applicable Industri... Garment Shops, Building Material Shops, Manufacturing Plant. Local Service Locat...United Kingdom, United States, Germany, Viet Nam, Philippine.
Condition: New, New
Configuration: PORTABLE
Lubrication Style: Oil-free
Place of Origin: China
Model Number: $\quad 02-3 / 4-150,02-5 / 4-150,02-10 / 4-150,02-15 / 4-150,02-20 / 4-\ldots$
Dimension $\left(L^{*} W^{*} \mathrm{H}\right)$ : customized
Certification: ISO
After-sales Service ...Field installation, commissioning and training
Air capacity: $\quad 3-75 \mathrm{Nm} 3 / \mathrm{h}$
Video outgoing-ins... Provided
Warranty of core co... 1 Year
Gas Type: oxygen
Flow Capacity: $\quad 3,5,10,15,20,25,30,40,50,75 \mathrm{Nm} 3 / \mathrm{h}$
Inlet Pressure: 4bar
Outlet Temperature: 50C
Outlet Size: $\quad 8-15 \mathrm{~mm}$
Lubrication: no oil lubricated

After Warranty Serv...Video technical support, Online support, Spare parts, Field ma... Showroom Location: Turkey, United Kingdom, United States, Viet Nam, Philippines, ...
Type: PISTON

Power Source: AC POWER
Mute: yes
Brand Name: BROTIE
Voltage: customized
Weight: $\quad 300-650 \mathrm{~kg}$

Warranty: $\quad 1$ Year
Working Pressure: 150bar, 200bar
Machinery Test Re... Provided
Marketing Type: New Product 2020
Core Components: Motor, compressor block
Model: $\quad 02-3,5,10,15,20,25,30,40,50,75 / 4-150$
Compressing Stage: 3 Stages
Outlet Pressure: 150,200bar
Inlet Size: DN20-DN32
Cooling System: Wind cooling/Water cooling

BROTIE Totally Oil-free Oxygen Compressor Specifications

| Item | Specification | Remarks |
| :--- | :--- | :--- |
| Model | $02-3,5,10,15,20,25,30,40,50,75 / 4-150$ |  |
| Flow Capacity | $3,5,10,15,20,25,30,40,50,75 \mathrm{Nm} 3 / \mathrm{h}$ |  |
| Compressing Stage | 3 Stages |  |
| Inlet Pressure | 4 bar |  |
| Outlet Pressure | 150 bar | Due to the model |
| Outlet Temperature | $\leq 50^{\circ} \mathrm{C}$ | Due to the model |
| Inlet Size | 8 mm -15mm |  |
| Outlet Size | Normal temperature | Due to the model |
| Ambient Temperature | Wind cooling/Water cooling | Due to the model |
| Cooling System | No Lubrication | Due to the model |
| Lubrication | $350-730$ rpm | Due the model |
| Rotating Speed | $3-22 \mathrm{Kw}$ |  |
| Power Consumption | Weight |  |

Totally oil-free model, no oil lubricated in the whole compressor.
All parts which contact with $\mathbf{O 2}$ gas are made of stainless steel.
Please confirm your power supply of 3phase before order

### 7.6 Expansion valve:

## Catalogue

https://www.parker.com/literature/Instrumentation\ Products\ Division/Catalogs/Cryogenic \%20Valves\%20for\%20Industrial\%20Gas\%20Applications.pdf

## Choice 1 :

https://www.alibaba.com/product-detail/Cryogenic-Turbo-Expander-China-MadePLPK 60832517222.html?spm=a2700.7735675.normal offer.d title.1e6742e1VyAiHQ\&s=p

China made PLPK-8.33/18.6-4.9 cryogenic turbo expander for air separation turbo expander

$>=1$ Units
$\$ 1,000.00$

| Model Number: | PLPK-8.33/18.6-4.9 |
| :--- | :--- |
| Warranty: | $\mathbf{1}$ Year for machinery warranty |
| Shipping: | Support Sea freight |
| (F) Alibaba.com Freight |  |

Payments: VISA T/T Online Transfe «Pay WesternUnionWU lity $\downarrow$

Parameters of turbo expander for air separation

| Models | technical parameter |  |  |  |  | matching air separation | remark |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | output <br> ( $\mathrm{Nm}^{3} \mathrm{~h}$ ) | intake pressure $(\mathrm{MP}, \mathrm{G})$ | discharge pressuret $\left(\mathrm{MP}_{2}, \mathrm{G}\right)$ | imtake temperature (K) | efficiency <br> (\%) |  |  |
| PLPK-6/6-0.42 | 360 | 0.6 | 0.042 | 130 | 76 | 180 m 'h o oxygen generating | $\rho$ |
| PLPK-8.33/18.6-4.9 | 500 | 1.86 | 0.49 | 173 | 76 | medium-pressure $150 \mathrm{~m}^{\prime} / \mathrm{h}$ oxygen generating | $\varphi$ |
| PLPK-7.1/3.6-0.3 | 425 | 0.36 | 0.03 e | 118.3 | 77. | oxygen producing truck | military ${ }^{\text {a }}$ |
| PLPK-10/8-0.47 | 600 | $0.8$ | $0.047$ | 150 | 76 | $350 \sim 750 \mathrm{~m}^{3} / \mathrm{h}$ oxygen generating | booster turbine |
| PLPK-18.33/7.7-0.38 | 1100 | 675 | -0.0.8 0 | 19, $0^{\text {a }}$ | - | oxygen generating plant | booster turbine |
| PLPK-25/6.25-0.45 | 1500 | 0.625 | 0.045 | 153 | 78 | $1500 \mathrm{~m} / \mathrm{h}$ oxygen generating | booster turbine |
| PLPK-30/5.5-0.4 | 1800 | 0.55 | 0.04 | 150 | 80 | $1600 \mathrm{~m}^{3} / \mathrm{h}$ oxygen generating | adjustable nozzle |
| PLPK-40/13.7-0.2 | 2400 | 1.37 | 0.02 | 150 | 78 | pure nitrogen plants | booster turbine |
| PLPK-46.17/13.4-0.19 | 2770 | 1.34 | 0.019 | 148 | 78 | pure nitrogen plants | booster turbine |
| PLPK-43.3/4.6-0.4 | 2600 | 0.46 | 0.04 | 110 | 81 | pure nitrogen plants | adjustable nozze |
| PLPK-80/9.5-5.2 | 4800 | 0.95 | 0.52 | 112 | 81 | pure nitrogen plants | adjustable nozze |
| PLPK-83.67/3.2-0.3 | 5020 | 0.32 | 0.03 | 116 | 81 | pure nitrogen plants | $\checkmark$ |

### 7.7 Materials suitable for cryogenic heat exchanger

## Material link: 6

### 7.7.1 Materials suitable down to $-45^{\circ} \mathrm{C}$

This first threshold is important because, besides being typically the lower limit of the temperatures naturally reached on the planet, it is also the temperature at which some industrial operations and some chemical processes are carried out.

Unfortunately, common construction steels are no longer usable at this level, either because of their intrinsic characteristics or because they are not usually tested for hardness and resistance to low temperatures. Some steelworks, however, have special carbon steels for these applications. These are mainly quenched and tempered low alloy steels.

Almost all aluminium alloys can be used at temperatures down to $-45^{\circ} \mathrm{C}$, except series such as 7075 T6 and 7178-T6, and titanium alloys $13 \mathrm{~V}-11 \mathrm{Cr}-3 \mathrm{Al}$ or 8 Mn . Copper and nickel alloys can generally all be used at these temperatures. PH stainless steels, i.e. precipitation hardening stainless steels, are not suitable for temperatures below $-20^{\circ} \mathrm{C}$ because of embrittlement and cracks.

### 7.7.2 Materials suitable down to $-75^{\circ} \mathrm{C}$

Some steels can be used at these temperatures, such as low alloy, quenched and tempered steels or ferritic nickel steels. Most low carbon ( $0.20-0.35 \%$ ) martensitic steels can be used with sufficient reliability. Many of these alloys contain manganese, nickel, chromium, molybdenum and vanadium, and some zirconium and boron.

### 7.7.3 Materials suitable down to $-100^{\circ} \mathrm{C}$

Low carbon, $3.5 \%$-nickel steels are often used in liquid gas storage tanks at temperatures down to $100^{\circ} \mathrm{C}$. Many aluminium, nickel, and titanium alloys are also suitable for these temperatures. Aluminium 7076-T6 can also be used up to $-128^{\circ} \mathrm{C}$, but not for critical applications.

### 7.7.4 Materials suitable down to $-196{ }^{\circ} \mathrm{C}$

The austenitic stainless steels of the 300 series are all suitable for working in this temperature range. Maraging steels with nickel content between $20 \%$ and $25 \%$ and the addition of cobalt, molybdenum, titanium, aluminium, and niobium are also suitable. Maraging steels have excellent malleability, toughness and hardness characteristics, and must be hardened at a temperature of just $400^{\circ} \mathrm{C}$.

Many aluminium alloys, such as 2024-T6, 7039-T6 and 5456-H343 have excellent fracture resistance at $-196^{\circ} \mathrm{C}$; also 2014-T6 but with the exception of welds. Other alloys resistant to even lower temperatures are the 5000 series aluminium-magnesium alloys, the 2219-T87 and the 6061-T6.

[^3]
## Static Analysis

The nickel-based materials are almost all resistant to $-196^{\circ} \mathrm{C}$. Titanium alloys such as $5 \mathrm{Al}-2.5 \mathrm{Sn}-\mathrm{Ti}$, $6 \mathrm{~A} 1-4 \mathrm{~V}-\mathrm{Ti}$ and $8 \mathrm{Al}-2 \mathrm{Cb}-1 \mathrm{Ta}-\mathrm{TiY}$ are also suitable, but should be kept free of impurities such as oxygen, nitrogen, carbon and iron as they cause embrittlement.
The aluminium alloys that can be used at the temperatures involved are typically in the 2000 and 5000 series, or the 6061-T6 alloy. In particular, welds on 2219-T87 have demonstrated excellent fracture resistance, while 5052-H38 and 5083-1138 have high crack resistance. The same applies to Monel, K-Monel, electroformed nickel, hardened nickel for thorium dispersion, and nickel alloys such as Inconel X, Inconel 718, René 41, and Hastelloy B. At these temperatures, only Ti45A and 5Al-2.5Sn-Ti titanium alloys can be used, both as base metal and welded.

Copper alloys are generally also used in contact with liquid hydrogen and helium, such as 70-30 brass, copper-beryllium, iron-silicon and aluminium bronzes. Magnesium alloys, on the other hand, tend to become brittle but can be used in low stress applications with careful design.

Materials suitable for cryogenic heat exchanger



Fig. 2.16. Temperature range for commonly used regenerator materials in cryogenic refrigerators. 7


Fig. 2.17. Comparison of the specific heats for three commonly used regenerator materials. 6


Figure 33 Percent elongation before rupture of some materials used in cryogenic service: 6


Figure 34 Yield and tensile strength of several AISI 300 series stainless steels. ${ }^{33}$ (Courtesy American Iron and Steel Institute.)

Table 6 Properties of Various Multilayer Insulations (Warm Wall at 300 K )

| Sample <br> Thickness <br> $(\mathrm{cm})$ | Shields <br> per <br> Centimeter | Density <br> $\left(\mathrm{g} / \mathrm{cm}^{3}\right)$ | Cold <br> Wall <br> $T(\mathrm{~K})$ | Conductivity <br> $(\boldsymbol{\mu W} / \mathrm{cm} \cdot \mathrm{K})$ | Material $^{\boldsymbol{a}}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |

[^4]

Figure 36 Thermal conductivity of materials useful in low-temperature service. (1) 2024TA aluminum; (2) beryllium copper, (3) K-Monel; (4) titanium; (5) 304 stainless steel; (6) C1020 carbon steel; (7) pure copper; (8) Teflon. ${ }^{35}$

Table 3.5. Specific Heat of Regenerator Materials $\boldsymbol{c}_{\boldsymbol{p}}$ ( $\mathbf{J} / \mathbf{k g}-\mathrm{K}$ )

| Temp. <br> (K) | Al | Cu | In | Pb | stainless steel | Bronze | Sn |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| 10 | 1.5 | 2.8 | 15.5 | 13.8 | 1.6 | - | 8 |
| $20\left(\mathrm{H}_{2}\right.$ bpt $)$ | 9 | 7.5 | 51 | 51 | 4.6 | 4.5 | 40 |
| 50 | 141 | 98 | 160 | 103 | 67 | 64 | 130 |
| $77\left(\mathrm{~N}_{2}\right.$ bpt) | 341 | 197 | 190 | 118 | 159 | 140 | 170 |
| $90\left(\mathrm{O}_{2}\right.$ bpt) | 427 | 232 | 200 | 119 | 209 | 200 | 180 |
| 100 | 485.6 | 254 | 205 | 120 | 238.6 | 220 | 187 |
| 150 | 686.5 | 324 | 210 | 125 | 356 | 340 | 203 |
| 200 | 799.5 | 357.5 | 220 | 128 | 414.4 | 400 | 205 |
| 300 | 900 | 387 | 220 | 130 | 477 | 490 | 210 |

### 7.8 Liquid oxygen tank

The liquid oxygen tank is an insulated vertical tank with double layer cover for storing liquid oxygen. The material used for inner tank is s30408 stainless steel.
The liquid oxygen tank is an insulated vertical tank with double layer cover for storing liquid oxygen. The material used for inner tank is S30408 stainless steel; The outer container materials are chosen as Q235-B, Q245R or 345R according to the national regulations according to the user's area. The inner and outer container sandwiches are filled with sand pearl thermal insulation materials, insulated and broomed.

The liquid oxygen tank has the features of high air tightness, low thermal conductivity, good thermal insulation performance, small evaporation loss and long service life, it is widely used in the pharmaceutical, chemical, manufacturing and other industries.

## The structure of the liquid oxygen tank8

Liquid oxygen tank (LO2 tank) consists of tank body, tools, tubes, valves, etc.

## 1. Relief device

2. Inner container
3. Insulation layer (sand pearl)
4.Shell
4. Instrument
(Differential pressure

oxygen pressure gauge, | gauge, |
| :--- |
| combination valve) |

6. Pump port and vacuum valve
7. Pipeline valve


## Describe:

(1) The liquid oxygen tank drive system is mostly centered on the bottom of the tank, and the instrument system and the built-in valve are arranged on the tank wall for easy monitoring and operation.
(2) Cryogenic storage tank contains booster and boost regulator to increase the tank pressure to the pressure required by the user.
(3) The inner container for liquid oxygen storage tanks is equipped with two safety valves, two rupture discs, a tube safety valve, an intermediate pressure relief device.


LOX tanks are stationary, vacuum-insulated pressure vessels and consist of an inner and an outer pressure vessel. The inner vessel, designed for the storage of lowtemperature, liquefied gas, is manufactured out of cold-stretched material (stainless steel 1.4311 or 1.4301 ). The outer vessel is manufactured out of carbon steel. The space between the inner and outer vessel is filled with perlite, a grained insulation material and is evacuated up to a pressure of below 50 microns in a warm state $\left(20^{\circ} \mathrm{C}\right)$. In addition, a molecular sieve ensures, by means of absorption, the long-term stability of the vacuum during the operation of the tank. An automatic regulation system helps maintain the working pressure and minimizes losses in case of lower
withdrawal rates. The quality of the welded seams is checked by a leak test with helium, which also ensures long-term durability of the vacuum. 9

To improve the efficiency of the cold converter, the tank is equipped with an additional pressure reducing system. This system works with a pressure reducing regulator which is installed in a connecting line between the gas phase and the highest point of the product withdrawal line. If, due to a prolonged standstill, the pressure in the tank is above the adjusted opening pressure of the regulator, and if valve is open, the economizer will open and opens the connection between gas phase and liquid phase. In case of product withdrawal through valve, it will now be taken out of the gas reserve of thetank and this measure will result in a rapid reduction of pressure. If the tank pressure is now below the opening pressure of the regulator, the economizer will close andwithdrawal will be done out of the liquid phase, consequently with a smaller pressure drop. The standard opening pressure is set 1 bar above the closing pressure of the pressure reducing regulator.
$9 \mathrm{https}: / /$ acprodbponlinebcc5.blob.core.windows.net/bp-publicfiles/bp_editor_div_mgs/TechnicalInformation/PMGS_LOX_Storage_Tanks_HTM_Instruction_Boo
k_EN_8102341086.pdf


## 10

## Flow diagram - tanks for nitrogen, oxygen, argon.

| Instrumentation and equipment, standard | Valves, standard |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| C/1 | Fill coupling | 1 | Filling | Optlons |

10 https://www.linde-engineering.com/en/images/P_3_3_e_12_150dpi_tcm19-5774.pdf


Liquefied gases are store at ultra-cold temperatures in a vacuum insulated tank. Controls on the tank keep the pressure at optimum levels to assure proper liquid delivery to the application.Vacuum insulated pipe connects the tank's liquid withdrawal to the application equipment. The pipe is the foundation for the system's heat-loss efficiency and long-term integrity. It must be engineered to work with the associated controls and accessories.

## Modular Piping Design Advantages 11

- Reduces your life-cycle costs by reducing the number of external piping joints, minimizing the risk of external piping leaks and the cost to repair.
- Simple by design yet robust and able to support a broad range of customer applications.
- Combination pressure building/economizer regulator for easy pressure adjustment and extended bonnet bronze control valves for ease of operation.
- Piping modules designed for ease-of-access to all operational control valves with stainless steel inter- connecting piping for improved durability.


High performance safety system with dual relief valves and rupture disks supplied as standard


New, innovative vertical fin pressure building system improves performance, while reducing frost and ice build up to further reduce your maintenance costs


Dual regulator econo-
mizer and pressure builder supplied as standard.


Full-trycock and economizer valves come standard with non-extended packing

|  | OXYGEN |  | NITROGEN |  | ARGON |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Saturation <br> Pressure <br> PSIG | Liquid <br> Density <br> Lbs/Ft | Gas <br> Density <br> SCF/Gal | Liquid <br> Density <br> Lbs/Ft $^{3}$ | Gas <br> Density <br> SCF/Gal | Liquid <br> Density <br> Lbs/Ft | Gas <br> Density <br> SCF/Gal |
| 0 | 71.17 | 115.10 | 50.44 | 93.11 | 87.51 | 112.50 |
| 5 | 70.42 | 113.72 | 49.62 | 91.55 | 85.77 | 110.89 |
| 10 | 69.80 | 112.73 | 49.00 | 90.40 | 84.77 | 109.60 |
| 25 | 67.86 | 109.59 | 47.50 | 87.63 | 82.46 | 106.61 |
| 50 | 65.55 | 105.86 | 45.69 | 84.18 | 79.90 | 103.31 |
| 75 | 63.76 | 102.97 | 44.19 | 81.53 | 77.90 | 100.71 |
| 100 | 62.43 | 100.82 | 42.88 | 79.12 | 76.15 | 98.45 |
| 150 | 59.80 | 96.57 | 40.70 | 75.08 | 73.16 | 94.59 |
| 200 | 57.62 | 93.05 | 38.76 | 71.51 | 70.28 | 90.87 |
| 250 | 55.60 | 89.79 | 36.83 | 67.95 | 67.79 | 87.65 |

Note: Density of water at $60^{\circ} \mathrm{F}=62.30 \mathrm{lbs} / \mathrm{cu}$ ft


Static Analysis

|  | Weight |  |  | Oxygen |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pounds <br> $(\mathrm{Lb})$ | Kilograms <br> $(\mathrm{Kg})$ | Cubic Feet <br> $(\mathrm{SCF})$ | Cubic Meters <br> $\left(\mathrm{Nm}^{3}\right)$ | Gallons <br> $(\mathrm{Gal})$ | Liters <br> $(\mathrm{L})$ |
| 1 Pound | 1.0 | 0.4536 | 12.076 | 0.3174 | 0.1050 | 0.3977 |
| 1 Kilogram | 2.205 | 1.0 | 26.62 | 0.6998 | 0.2316 | 0.8767 |
| 1 SCF Gas | 0.08281 | 0.03756 | 1.0 | 0.02628 | 0.008691 | 0.0329 |
| 1 Nm $^{3}$ Gas | 3.151 | 1.4291 | 38.04 | 1.0 | 0.3310 | 1.2528 |
| 1 Gal Liquid | 9.527 | 4.322 | 115.1 | 3.025 | 1.0 | 3.785 |
| 1 LLiquid | 2.517 | 1.1417 | 30.38 | 0.7983 | 0.2642 | 1.0 |

SCF (Standard Cubic Foot) gas measured at 1 atmosphere and $70^{\circ} \mathrm{F}$. Liquid measured at 1 atmosphere and boiling temperature.
$\mathrm{Nm}^{3}$ (normal cubic meter) measured at 1 atmosphere and $0^{\circ} \mathrm{C}$.

| الوزن (كلغ) | البعد (م) | متوسط | نموذج | لا |
| :---: | :---: | :---: | :---: | :---: |
| 3940 | Ф1916 * 5262 | LO2 | CFL-5 / 0.8 | 1 |
| 5970 | Ф2316 * 5981 | LO2 | CFL-10 / 0.8 | 2 |
| 8045 | Ф2316 * 8035 | LO2 | CFL-15 / 0.8 | 3 |
| 9855 | Ф2716 * 7377 | LO2 | CFL 20 / 0.8 | 4 |
| 14025 | Ф2920 * 8904 | LO2 | CFL-30 / 0.8 | 5 |
| 21570 | Ф3220 * 11204 | LO2 | CFL-50 / 0.8 | 6 |
| 38300 | Ф3424 * 18466 | LO2 | CFL-100 / 0.8 | 7 |
| 54700 | Ф3728 * 22128 | LO2 | CFL-150 / 0.8 | 8 |

- Choice 1:
https://www.alibaba.com/product-detail/5m3-8-bar-new-vertical-
liquid 62150227966.html?spm=a2700.galleryofferlist.normal offer.d title. 7011710 cmDfcd 2


| FOB Reference Price: Get Latest Price |  |  |  |
| :---: | :---: | :---: | :---: |
| \$10,000.00-\$20,000.00 / Set |  |  | 1 Set/Sets (Min. Order) |
| Model Number: | CFL-5/0.8mpa |  |  |
| Warranty: | 1 Year for machinery warranty |  |  |
| Lead Time: | Quantity(Sets) | 1-1 | >1 |
|  | Est. Time(days) | 45 | Negotiable |
| Customization: | Customized logo (Min. Order. 1 Sets) |  |  |

## Overview

Quick Details

| Capacity: | $5 \sim 120 \mathrm{M} 3$ |
| :--- | :--- |
| Applicable Industri... | Manufacturing Plant, Food \& Beverage Factory, Energy \& Mining |
| Brand Name: | Chengde |
| Weight: | 3412 |
| Warranty: | 1 Year |
| Working Pressure: | 0.8 MPa |
| Inner Material: | S30408 |
| Loading medium: | LIN,LO2,LN2,LAr |
| Filling Rate: | 0.95 |
| Type: | Vertical |


| Condition: | New |
| :--- | :--- |
| Place of Origin: | Henan, China |
| Dimension(L*W*H): | $5130 * 2000 * 2000$ |
| Certification: | CE,ASME,ISO9001 |
| After-sales Service ...Field installation, commissioning and training, Online support |  |
| Effective Capacity: | 5 m 3 |
| Outer Material: | Q345R |
| Standard: | as your requirement |
| Color: | White or Customer's Request |

Specification

| Item | Effective Volume (m3) | Max Working Pressure (Mpa) | Working medium | $\begin{aligned} & \text { Size } \\ & (\mathrm{mm}) \end{aligned}$ | Weight (KGS) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CFL-5/0.8 | 5 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | \$2000×5130 | $\sim 3412$ |
| CFL-5/1.6 |  | 1.6 |  | \$2000×5130 | $\sim 3945$ |
| CFL-5/0.2 |  | 0.2 |  | $\Phi 2000 \times 5130$ | ~3461 |
| CFL-10/0.8 | 10 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | \$2100×7170 | $\sim 5378$ |
| CFL-10/1.6 |  | 1.6 |  | $\Phi 2000 \times 7895$ | $\sim 6787$ |
| CFL-10/0.2 |  | 0.2 |  | \$2100×7130 | $\sim 5895$ |
| CFL-15/0.8 | 15 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | Ф2500×6950 | $\sim 6415$ |
| CFL-15/1.6 |  | 1.6 |  | \$2400×7552 | $\sim 8628$ |
| CFL-15/0.2 |  | 0.2 |  | \$2500×6950 | $\sim 7876$ |
| CFL-20/0.8 | 20 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | $\Phi 2500 \times 8756$ | $\sim 8255$ |
| CFL-20/1.6 |  | 1.6 |  | Ф2400×9371 | $\sim 10744$ |
| CFL-20/0.2 |  | 0.2 |  | Ф2500×8756 | $\sim 9284$ |
| CFL-30/0.8 | 30 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | Ф2900×8870 | ~12899 |
| CFL-30/1.6 |  | 1.6 |  | $\Phi 2700 \times 8960$ | $\sim 20392$ |
| CFL-30/0.2 |  | 0.2 |  | $\Phi 2900 \times 8900$ | $\sim 16093$ |
| CFL-50/0.8 | 50 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | \$3100×12058 | $\sim 18960$ |
| CFL-50/1.6 |  | 1.6 |  | Ф3000×12760 | $\sim 21590$ |
| CFL-50/0.2 |  | 0.2 |  | Ф3100× 12060 | ~19662 |
| CFL-100/0.8 | 100 | 0.8 | Liquid oxygen Liquid argon Liquid nitrogen LNG | Ф3600×17250 | $\sim 45218$ |
| CFL-100/1.6 |  | 1.6 |  | Ф3600× 17250 | $\sim 57258$ |
| CFL-100/0.2 |  | 0.2 |  | \$ $3600 \times 17250$ | ~38655 |


| أكبر من 20 <br> (متر) | حتى 20 طن <br> (متر) | المسافات الآمنة لتعرض صهاريح الأكسجين المُسال لإحتمالات التسريب أو الإنسكاب |
| :---: | :---: | :---: |
| 8 | 5 | عن الأماكن المسموح فيها بالتدخين أو إشعال النيران |
| 15 | 10 | عن أماكن التجمعات العامة |
| 8 | 5 | عن المكاتب، و المقاصف، و الأماكن المشغولة بالأشخاص. |
| 8 | 5 | عن الحفر، و القنوات، و مصارف المياه السطحية (غير المستغلة) |
| 8 | 5 | عن الفتحات المؤدية إلى الأنظمة الموجودة تحت الأرض |
| 8 | 5 | عن حدود الملكية |
| 8 | 5 | عن الطريق العام |

Liquid oxygen tank

| 15 | 10 | عن السكك الحديدية |
| :---: | :---: | :---: |
| 8 | 5 | عن أماكن إنتظار السِيارات (غير المُرَّهَّة) |
| 15 | 15 | عن الإنشاءات الخشبية الضخمة |
| 8 | 5 | عن المخزونات الصغيرة من المواد القابلة للإشتعال، و كراقانات المواقع، و ما إلى ذلك |
| 8 | 5 | عن معدات التشغيل (التي لِست حزء من منظومة شبكة الغازات الطبية) |
| 3 | 3 | عن خطوط الغازات القابلة للإشتعال |
| 15 | 15 | عن فلانشات >طوط الغازات القابلة للإشتعال (المقاسات التي تتعدى 50 mm) |
| 8 | 5 | عن مواسير تنفيس الوقود الغازي |
| 8 | 5 | عن مآخذ هواء الكباسات و أجحمرة التنفس الصناعي |
| 5 | 5 | عن إسطوانات الوقود الغازي (التي تصل إلى 7033) |
| 7.5 | 7.5 | عن صـاريج تخزين وقود الغاز المُسال (التي تصل إلى 4 أطنان) |
| 15 | 15 |  |
| 7.5 | 7.5 | عن صـهاريج تخزين الوقود السائل (التي تصل إلى 7.8 ${ }_{\text {(1) }}^{\text {(1) }}$ |
| 15 | 15 | عن صـهاريج تخّزين الوقود السائل (التي تصل إلى 117 m³ |
| 8 | 5 | عن محطات الجهد العالي HV و الجهد المتوسط MV الفرعية |

Cryogenic Liquid Storage Tank Flow Chart（B）


| V1 | Pressure building valve | V2 | Upper inlet valve | V3 | Lower inlet valve | V4 | Gas passing valve |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V5 | Liquid Outlet valve | V6 | Gas return valve | V7 | 3－way switch valve | R | Vacuum tube |
| VV | Vacuum Valve | MV | Full measuring valve | E1 | Vent valve | E2 | Raffinate vent valve |
| Pr | Turbo charger | T | Pressure regulating valve． | S1 | Inner tank safety valve | S2 | Inner tank safety valve |
| S3 | Inner tank safety valve | S4 | Outer tank safety device | L1 | Liquid gauge upper valve | L2 | Balancing valve |
| L3 | Liquid gauge lower valve | P | Pressure Gauge | LG | Liquid Level Gauge |  |  |
| Xinxiang Chengde Energy Technology Equipment Co．，Ltd |  |  |  |  |  |  |  |
| Phone：$+86-373-2677103$ |  |  | F a x ：＋86－373－2677983 |  |  |  |  |

［ E －新乡市诚德能源科技装备有限公司

1．Loading medium：LN2，LO2，LAr，LNG，LPG，etc．
2．Effective Volume： 20 m 3
3．Working pressure： 0.8 MPa
4．Overall dimension：$\Phi 3000 * 6100 \mathrm{~mm}$
5．Cylinder design temperature：$-196^{\circ} \mathrm{C}$
6．Shell material：Outer jacket：Q245－R；Inner：S30408．
7．Insulation：Vacuum powder insulation
8．Filling rate： 0.95
9．Relief Valve：All valves are high grade Chinese valves．
10．Delivery date：Within 60 days after received pre－payment，or more shorter time．
11．Payment model：We can negotiate，we suggest TT，LC．
12．Documents：Bill of Loading，Invoice，Packing list，Contract（3 originals）．

$$
\begin{aligned}
& \text { (الطرف أ: مـعمات المثتّجات } \\
& \text { 15CBM 0.8Mpa }
\end{aligned}
$$

$$
\begin{aligned}
& \text { 4. اللجد الكلى: } 002500 \text { × } 6912 \text { مم }
\end{aligned}
$$

$$
\begin{aligned}
& \text { 7. عزل: فراغ اع مسحوف الحزل } \\
& \text { 8.الونن الفارغ: حوالـى } 6415 \text { كجم } \\
& \text { 9. } 9 .
\end{aligned}
$$

| Cryogenic Liquid Storage Tank |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model | Volume(M3) | Pressure(MPa) | Size(mm) | Weight(kg) | Material | Medium | Filling rate |
| CFL-5/0.8 | 5 | 0.8 | $\varphi 2000 * 5130$ | 3412 | Outer:Q245-R Inner:S30408 | LO2/LAR/LN2 | 95\% |
| CFL-10/0.8 | 10 |  | ¢2100*7170 | 5378 |  |  |  |
| CFL-15/0.8 | 15 |  | ¢2500*6912 | 6415 |  |  |  |
| CFL-20/0.8 | 20 |  | $\varphi 3000 * 6100$ | 8673 |  |  |  |
| CFL-30/0.8 | 30 |  | ¢2900*8870 | 12899 |  |  |  |
| CFL-50/0.8 | 50 |  | ¢3100*12058 | 18960 |  |  |  |
| CFL-100/0.8 | 100 |  | ¢3600*15947 | 34480 |  |  |  |
| CFL-5/1.6 | 5 | 1.6 | ¢2000*5130 | 3945 |  |  |  |
| CFL-10/1.6 | 10 |  | ¢2000*7895 | 6787 |  |  |  |
| CFL-15/1.6 | 15 |  | ¢2400*7552 | 8628 |  |  |  |
| CFL-20/1.6 | 20 |  | Q2400*9371 | 10744 |  |  |  |
| CFL-30/1.6 | 30 |  | ¢2700*10310 | 14640 |  |  |  |
| CFL-50/1.6 | 50 |  | ¢ $3100 * 12058$ | 23370 |  |  |  |

* Another method of Oxygen liquefaction

12 http://ar.cncdtank.com/cryogenic-tank/50001-oxygen-liquid-tank.html 13 http://ar.cncdtank.com/news/safety-use-standards-that-liquid-oxygen-storag-26472706.html

Cascade system for Liquefaction of Oxygen Gas or Cascade Liquefier or Apparatus for Liquefaction of Oxygen Gas. 14


## Liquefaction of Oxygen by Cascade apparatus

## A Cascade Liquefier

As you can see in the above figure that, before getting liquid oxygen many stages of liquefaction are used. That's why we called it a cascade system or a Cascade liquefier, which is used to liquefy Oxygen or air.

As you know this process is first used by Pictet after sometime K Onnes (Kamerlingh Onnes) used this apparatus.

### 7.8.1 About the Apparatus

1. In this apparatus, three compressors $\mathrm{C}_{1}, \mathrm{C}_{2}, \mathrm{C}_{3}$ are used to fulfill the requirement of sufficient pressure. Also, the $\mathrm{C}_{1}, \mathrm{C}_{2}$, and $\mathrm{C}_{3}$ have a suction side which is used during the process.
2. Three condensers $R_{1}, R_{2}, R_{3}$ are used, into which three refrigerants cold water, Methyl chloride, and ethylene are used to get the desired result.
3. The Liquid oxygen is collected in the last, into a Dewar flask.

### 7.8.2 Principles

This apparatus work on two principles.

1. The first, Principle, compression of gases below its critical temperature resulting in a change to liquid.
2. Second is, producing cooling by the principle of evaporation of liquids.

### 7.8.3 How does it work?

First, the gaseous methyl chloride $\left(\mathrm{CH}_{3} \mathrm{Cl}\right)$ is pumped by the compressor $\mathrm{C}_{1}$ into the spiral tube. The refrigerant in condenser $\mathrm{R}_{1}$ surrounding this tube starts liquefying the methyl chloride.

This is because the critical temperature of methyl chloride is $143^{\circ} \mathrm{C}$, which is more than room temperature as well.

Now the liquid methyl chloride comes in Condensor $\mathrm{R}_{2}$ through the tube. Here one portion of condenser $\mathrm{R}_{2}$ is connected with the suction side of compressor $\mathrm{C}_{1}$.

Here due to the evaporation of liquid methyl chloride in reduced pressure, more cooling as a result produced, and the temperature of condenser $\mathrm{R}_{2}$ decreases more.

The evaporated methyl chloride return back to the compressor $\mathrm{C}_{1}$ through the suction side of the compressor.

Now the gaseous ethylene $\left(\mathrm{C}_{2} \mathrm{H}_{4}\right)$ pumped by the compressor $\mathrm{C}_{2}$ into the next spiral tube.
Here the refrigerant, liquid methyl chloride which is achieved in the previous stage, surrounding the tube which contains gaseous ethylene, starts to convert this gas into liquid ethylene.

This is because the critical temperature of ethylene is around $9.2^{\circ} \mathrm{C}$.
Now, this liquid ethylene comes in Condensor $\mathrm{R}_{3}$, and one portion of $\mathrm{R}_{3}$ condenser connected with the suction side of compressor $\mathrm{C}_{2}$.

Here evaporation of liquid ethylene takes place in reduced pressure like in the previous stage, and the evaporated ethylene return back to the compressor $\mathrm{C}_{2}$ through the suction side of the compressor.

Therefore, due to the evaporation process more cooling produced into the condenser $\mathrm{R}_{3}$, which is more than the cooling that we achieved in Condenser $\mathrm{R}_{2}$.

This cooling has a temperature of around $-160^{\circ} \mathrm{C}$.
Now, the oxygen (which is in gaseous form) is pumped by the compressor $\mathrm{C}_{3}$ into the next spiral tube.

Here, due to the very low temperature inside the Condenser $\mathrm{R}_{3}$ the oxygen gas into the spiral tube starts converting into liquid and later collected into a Dewar flask.

This is because the critical temperature of oxygen gas is around $-118^{\circ} \mathrm{C}$.

Here, likewise the previous stages, the evaporated oxygen return back to the compressor $\mathrm{C}_{3}$ through the suction side of the compressor.

If we continue this cascade system, we can liquefy air and other gases like Nitrogen, etc.
Note: But by this system, we cannot liquefy the gases that have very low critical temperatures, such as Hydrogen ( $\mathrm{T}_{\mathrm{c}}$ around $-240^{\circ} \mathrm{C}$ ) and Helium ( $\mathrm{T}_{\mathrm{c}}$ around $-267.8^{\circ} \mathrm{C}$ ).

## - Liquefaction of hydrogen

The principles of magnetic refrigeration and compressed-gas refrigeration are presented in the below figure. The temperature-entropy diagrams of magnetic material and gas as a refrigerant in liquefaction cycle are respectively shown in the below figure. The magnetic refrigeration for hydrogen liquefaction uses an external magnetic field to magnetize and demagnetize a magnetic material in repeated cycles, thus producing low temperatures through the magnetocaloric effect.


Comparison between magnetic refrigeration and compressed-gas refrigeration.
Magnetic refrigeration
(Reversed Carnot cycle)

|  | A-B : Adiabatic magnetization B-C : Isothermal magnetization C-D : Adiabatic demagnetization D-A : Isothermal demagnetization |
| :---: | :---: |
|  |  |

Comparison between magnetic refrigeration and compressed-gas refrigeration (temperature-entropy diagram).


Precooled Linde system

Because the inversion temp. of helium is 40 K , helium cannot be liquefied by this system.

Claude system
A part of compressed $\mathrm{H}_{2}$ gas is expanded in the expansion turbine to generate colder gas.

Simplified typical hydrogen liquefaction systems.


Comparison of hydrogen density in storage form of hydrogen 16

- Liquefaction of hydrogen by compressed-gas
http://sadanaresearch.com/liquid-helium-generator-overview/!
https://vorbuchner.com/en/helium-liquefaction/


## Liguenction Procedure



Liquid oxygen tank

| Compounds | $\mathrm{T}_{\mathrm{c}}, \mathrm{K}$ | $\begin{aligned} & \mathrm{P}_{\mathrm{c}} \\ & \mathrm{~atm} \end{aligned}$ | $\mathrm{Z}_{6}$ | Compounds | $\mathrm{T}_{\mathrm{c}, \mathrm{K}} \mathrm{K}$ | $\begin{gathered} \mathrm{P}_{\mathrm{C}}, \\ \mathrm{~atm} \\ \hline \end{gathered}$ | $\mathrm{Z}_{\mathrm{c}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 191 | 45.8 | 0.290 | Methyl Alcohol | 513 | 78.5 | 0.220 |
| U'Ethane | 306 | 48.2 | 0.284 |  | 416 | 65.9 | 0.276 |
| - | 370 | 42.0 | 0.276 | Methyl Ethyl Ketone | 533 | 39.5 | 0.26 |
| - | 425 | 37.5 | 0.274 | U/ Toluene | 594 | 41.6 | 0.270 |
| أيزو (Iso-butane | 408 | 36.0 | 0.282 | Tri-Chloro Fluoro MethaneM H ( F$)(11$ | 471 | 43.2 | 0.277 |
| juiupentane | 470 | 33.3 | 0.268 | Tri-Chloro Trifluoro Ethane(13 | 487 | 33.7 | 0.274 |
|  | 461 | 32.9 | 0.268 | برو2 Bromine ( $\mathrm{Br}_{2}$ ) | 584 | 102 | 0.307 |
| Neo-pentane | 434 | 31.6 | 0.260 | ${ }^{\text {a }}$ SChlorine, $\mathrm{Cl}_{2}$ | 417 | 76.1 | 0.276 |
| U-50.Hexane | 508 | 29.9 | 0.264 |  | 5.3 | 2.26 | 0.300 |
| - | 540 | 27.0 | 0.260 |  | 33.3 | 12.8 | 0.304 |
|  | 569 | 24.6 | 0.258 | dineon ( Ne ) | 44.5 | 26.9 | 0.307 |
| Winthylene | 282 | 50.0 | 0.268 |  | 126.0 | 33.5 | 0.291 |
| UPropylene | 365 | 45.6 | 0.276 | - Sioxygen ( $\mathrm{O}_{2}$ ) | 155 | 50.1 | 0.29 |
| 1- Butene | 420 | 39.7 | 0.276 | Fimmonia ( $\mathrm{NH}_{3}$ ) | 406 | 111 | 0.242 |
| U等-11-Pentene | 474 | 40.0 | - | STarbon Dioxide $\left(\mathrm{CO}_{2}\right)$ | 304 | 72.9 | 0.276 |
| Vin-Acetic Acid | 595 | 57.1 | 0.200 | 2icicarbon Monoxide (CO) | 133 | 34.5 | 0.294 |
|  | 509 | 46.6 | 0.237 |  | 653 | 145 | - |
| U'Acetylene | 309 | 61.6 | 0.274 |  | 325 | 81.5 | 0.266 |
|  | 562 | 48.6 | 0.274 |  | 374 | 88.9 | 0.284 |
| 1,3-Butadiene | 425 | 42.7 | 0.270 | Sitric Oxide (NO) | 180.0 | 64 | 0.25 |
| Ch Saclohexane | 553 | 40.0 | 0.271 |  | 310 | 71.7 | 0.271 |
| Dichloro-difluoro methane | 385 | 39.6 | 0.273 | تكبرك Sulfur (S) | 1313 | 116 | - |
| - | 282 | 50.0 | 0.268 |  | 431 | 77.8 | 0.268 |
| Niniethyle Ether | 467 | 35.6 | 0.261 |  | 491 | 83.8 | 0.262 |
| J-SEthyl Alcohol | 516 | 63.0 | 0.249 | ¢0Water ( $\mathrm{H}_{2} \mathrm{O}$ ) | 647 | 218 | 0.320 |
|  | 468 | 71.0 | 0.25 |  |  |  |  |

- Methane liquefaction
- Characteristics of Methane

Table 1 Properties of Principal Cryogens

| Name $\mathrm{P}=1 \mathrm{bar}=$ |  | Normal Boiling Point |  | Critical Point |  | Triple Point |  | Reference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 KPa | Liquid Density $\left(\mathrm{kg} / \mathrm{m}^{3}\right)$ | Latent Heat ( $\mathrm{J} / \mathrm{kg} \cdot \mathrm{mole}$ ) |  |  |  |  |  |
|  | $T$ (K) |  |  | $T$ (K) | $P(\mathrm{kPa})$ | $T(\mathrm{~K})$ | $P(\mathrm{kPa})$ |  |
| Helium | 4.22 | 123.9 | 91,860 | 5.28 | 227 |  |  | 1 |
| Hydrogen | 20.39 | 70.40 | 902,300 | 33.28 | 1296 | 14.00 | 7.20 | 2, 3 |
| Deuterium | 23.56 | 170.0 | 1,253,000 | 38.28 | 1648 | 18.72 | 17.10 | 4 |
| Neon | 27.22 | 1188.7 | 1,737,000 | 44.44 | 2723 | 26.28 | 43.23 | 5 |
| Nitrogen | 77.33 | 800.9 | 5,579,000 | 126.17 | 3385 | 63.22 | 12.55 | 6 |
| Air | 78.78 | 867.7 | 5,929,000 |  |  |  |  | 7, 8 |
| Carbon monoxide | 82.11 | 783.5 | 6,024,000 | 132.9 | 3502 | 68.11 | 15.38 | 9 |
| Fluorine | 85.06 | 1490.6 | 6,530,000 | 144.2 | 5571 |  |  | 10 |
| Argon | 87.28 | 1390.5 | 6,504,000 | 151.2 | 4861 | 83.78 |  | 11, 12, 13 |
| Oxygen | 90.22 | 1131.5 | 6,801,000 | 154.8 | 5081 | 54.39 | 0.14 | 6 |
| Methane | 111.72 | 421.1 | 8,163,000 | 190.61 | 4619 | 90.67 | 11.65 | 14 |
| Krypton | 119.83 | 2145.4 | 9,009,000 | 209.4 | 5488 | 116.00 | 73.22 | 15 |
| Nitric oxide | 121.50 | 1260.2 | 13,809,000 | 179.2 | 6516 | 108.94 |  |  |
| Nitrogen trifluoride | 144.72 | 1525.6 | 11,561,000 | 233.9 | 4530 |  |  |  |
| Refrigerant-14 | 145.11 | 1945.1 | 11,969,000 | 227.7 | 3737 | 89.17 | 0.12 | 16 |
| Ozone | 161.28 | 1617.8 | 14,321,000 | 261.1 | 5454 |  |  |  |
| Xenon | 164.83 | 3035.3 | 12,609,000 | 289.8 | 5840 | 161.39 | 81.50 | 17 |
| Ethylene | 169.39 | 559.4 | 13,514,000 | 282.7 | 5068 | 104.00 | 0.12 | 18 |

- Methane liquefaction basic cycle18

To liquefy natural gas methane taken at 1 bar and 280 K is compressed to 100 bar and then cooled to 210 K (it is assumed in this example that a refrigeration cycle is available for that).

Isentropic compression is assumed, but the very high compression ratio requires the use of several compressors ( 3 in this example) with intermediate cooling at 280 K . Intermediate pressures are equal to 5 and 25 bar.

The gas cooled at 210 K is isenthalpically expanded from 100 bar to 1 bar, and gas and liquid phases separated. As shown in the diagram in Figure below, the methane enters in the upper left, and liquid and gaseous fractions exit in the bottom right.


The compression work required per kilogram of methane sucked is 798.5 kJ , and 0.179 kg of liquid methane is produced, which corresponds to a work of 4.46 MJ per kilogram of liquefied methane.

- Linde cycle

The Linde cycle (Figure below) improves the previous on two points:

- gaseous methane is recycled after isenthalpic expansion;
- we introduce a heat exchanger between the gaseous methane and methane out of the cooler in order to cool the compressed gas not at 210 K but at 191 K .


Linde methane liquefaction cycle


- Conclusion related to methane liquefaction:

Each gas has a temperature it cannot be flushed over whatever the pressure. This temperature is known as critical temperature, and critical pressure is the pressure needed to liquefy the gas at the critical temperature of the gas.
Linde cycle can be applied to hydrogen gas, methane as well as oxygen, with consideration given to the critical point of each. Oxygen gas needs a temperature of 90 K (1 bar) to be in the liquid state, or it needs a pressure higher than 51 bar and a temperature of 154 K .

As for hydrogen gas, it needs a temperature of 20 K (atm pressure 1 bar ) to become in the liquid state, or it needs a pressure higher than 13 bar and a temperature of 33 K .
Finally, for gas, methane needs 110 K (1 bar air pressure) to become in the liquid state, or it needs a pressure higher than 46.2 bar and a temperature of 190 K .

## 8 COMPRESSORS

Various types of compressors are used in the oil and gas industry and the same can be said about the medical, dental and pharmaceutical industries.

Their variety ensures that each is specifically tailored to serve a particular purpose and to the best of its ability.

That being the case, the review of main types of compressors and their applications will give you a good knowledge of the best out there whose level of performance is on par with what you're out to get. 19

### 8.1 WHAT IS A COMPRESSOR?

A compressor is also known as a Heating, Ventilation \& AirConditioning (HVACR) machine.

It is a mechanical device that reduces the volume of a fluid such as gas or liquid while at the same time increasing its temperature and pressure.

A compressor features two major components and these are the power source and a compressing mechanism (for example piston and vanes).

What's more, these machines are similar to gas pumps because they transport compressed gas through pipes.

The latter has aided in the compression of natural gas in the oil and gas industry where the gas is pressurized in order to meet with the standards of certain jurisdictions that require at least 95 percent of the gas in petroleum to be compressed.

It is also worthy to note that certain factors influence a compressor's performance and these are:

- Speed of rotation
- Pressure at suction
- Pressure at discharge
- Type of refrigerant used


### 8.1. THE BASIC TYPES OF COMPRESSORS

A list of the major types of compressors by mechanical design has been outlined below and the feature of each, aids in its functionality.


Now, the best way to get a good idea of these devices is to compare them side by side and as such, a comparison between different types of compressors, how they work, and when to use them has also been given in this section.

Therefore, the two basic types of compressors are:

1. Positive displacement compressors
2. Dynamic compressors

### 8.1.1. POSITIVE DISPLACEMENT COMPRESSORS

In positive displacement compressors, gases are compressed due to the displacement of a mechanical linkage which reduces its volume.

First off, a certain amount of gas is passed into a confined space and the volume or space is subsequently reduced which helps to boost the gas' pressure levels.

The gas is then released into a discharge piping or vessel system once the pressure has been raised.

If you're wondering why this displacement is called positive in the first place, then reference can be made to thermodynamics where a displacement caused by the movement of a piston (as is the case of a reciprocating compressor) is known to be positive.


The movement can also be caused by rotation as is the case of a twin helical screw-rotating machine.

Consequently, the types of positive displacement compressors are:

COMPRESSORS
A) Reciprocating compressors
B) Rotary compressors

### 8.2.1.A) RECIPROCATING COMPRESSORS

Reciprocating compressors or piston compressors feature one or more pistons which are driven by a crankshaft; a component that also drives the piston rod, and connecting rod.

As the piston within the cylinder moves back and forth, the pressure of the gas is increased. This, in turn, helps in its compression. The compressed gas is then discharged into high pressure receiving tanks.

On the other hand, this positive displacement compressor can also be driven by electric motors or internal combustion engines.

They can be fixed to a particular location or portable enough to be moved around.
In terms of their horsepower, small compressors operate within the range of 5 to 30 horsepower ( hp ) and they are mostly used in the automobile sector of the economy.

Large compressors, on the contrary, have a horsepower above 1,000 hp ( 750 kW ). They are available in the oil and gas industry and generally in large industrial applications.

## - TYPES OF RECIPROCATING COMPRESSORS

## The various types of Reciprocating compressors are:

- Single-cylinder: A single cylinder reciprocating compressor features a suction, discharge area and compression. A double cylinder comes with dual suction, discharge areas, and compression, and it helps to achieve higher gas pressures.
- Multi-cylinder: While double cylinders are prevalent, there are instances where compressors are designed with as many as six cylinders.
$20 \mathrm{https}: / /$ cascousa.com/compressed-air-101/types-of-compressors/positive-displacementcompressors/
- Multi-stage design: As the name implies, more stages are incorporated to arrive at the final processed gas. Here, the gas is compressed multiple times in several compression cylinders to increase pressure levels.
- Diaphragm compressor: This differs from the conventional reciprocating compressor since the compression of gas is brought about by the to and fro movement of a flexible membrane. The movement is facilitated by a rod and the crankshaft.


### 8.2.1.B) ROTARY COMPRESSORS

Rotary compressors also have a positive displacement. These low capacity types of equipment have applications in home freezers and refrigerators.

They can either have a single vane that is located within the cylinder and kept away from the rotor, or multiple vanes located in the rotor.

The various types of rotary compressors include:

- ROTARY SCREW COMPRESSORS

It uses two meshed helical screws in rotation to force the gas into a smaller space.


They can be employed in industrial and commercial purposes and their application can range between 3 horsepower ( 2.2 kW ) to about 1,200 horsepower (890 kW).

Likewise, the discharge pressure can range between low to moderately high pressure ( $>1,200$ psi or 8.3 MPa ).

- ROTARY VANE COMPRESSORS

These machines feature a rotor that is mounted in a larger housing which has either a circular or complex shape.

The rotor also has several blades which are inserted in radial slots within the rotor.

As the rotor moves, the blades move in and out of the slots. This increases and decreases the volume of the gas.


In comparison with a piston
compressor, a rotary vane compressor operates more quietly and is best suited to the electric motor drive.

Like piston compressors, they can also be single or multi-staged, as well as stationary or portable.

Their discharge range can be between 29 psi as is the case of dry vane machines and 190 psi for oil-injected machines.

## - SCROLL COMPRESSORS

These are also known as scroll pump or scroll vacuum pump and they feature two spiral vanes that are interwoven.

While one of the vanes is fixed, the other moves around it which help in compressing the gas.

Scroll compressors also operate even more quietly and smoothly than other types of compressors in the lower volume range.

### 8.1.2. DYNAMIC COMPRESSORS

Dynamic compressors are also known as turbo compressors and they depend on a fluid's inertia and momentum to bring about its increased pressure levels.

In their mode of operation, velocity energy is impacted to a stream of gas and this energy is then converted to pressure energy.

There are two basic types of dynamic compressors and these are:
A. Centrifugal compressors
B. Axial compressors

### 8.2.2.A) CENTRIFUGAL COMPRESSORS

Centrifugal compressors make up about 80 percent of the entire dynamic processors, therefore, leaving 20 percent to axial compressors.

That being the case, they are widely used in oil refineries, natural gas processing plants, chemical and petrochemical plants.


CENTRIFUGAL COMPRESSOR

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Due to their high output pressures of over 1,000 psi (6.9 MPa) and horsepower range of a 100 to 1000, these machines can be used in:

- Snowmaking operations
- Refrigeration
- Air conditioning systems

For their mode of operation, compression is made possible by exerting inertial force on the gas with the use of high-speed rotating impellers

The gas is forced to the rim of the impeller which helps to increase its velocity. This velocity is then converted to pressure energy by a diffuser.

The process can also be carried out in a single stage or multi-stage where each stage takes advantage of an impeller (a rotating disk) and diffuser (a stationary element).
Both single and multistage machines are generally made up of standardized components. However, the multistage helps in improving the compression ratio since centrifugal compressors generally have lower compression ratios in comparison to displacement compressors.

Centrifugal compressor also features two casing designs and these are:

- HORIZONTALLY SPLIT CASING DESIGN

This compressor has an outer casing which can be split horizontally to aid in the maintenance of its internal component.

Within the compressor, the rotating disk or impellers are connected to one rotating shaft to form a multi-stage structure.

As the gas passes through the intake nozzle, a centrifugal force created by the high-speed movement of the impellers causes it to be compressed and pressurized before it is sent out to an ejection nozzle.


## - VERTICALLY SPLIT CASING DESIGN

While the internal components of this machine have a similar design to that of the horizontal split type casing, its outer design differs.

Here, the rotor bundle and the diaphragm seals are axially arranged in a steel barrel casing.

Generally, this design depends on the working pressure and the type of gas that is to be compressed.

### 8.2.2.B) AXIAL-FLOW COMPRESSORS

Another type of dynamic rotating compressors is the axial-flow compressor. They are mostly employed where compact design or high flow rates (large flow volumes) is desired.

These compressors have a pressure range between low to medium and you'll find their application in jet engines, natural gas pumping stations, chemical plants, and large gas turbine engines.


Axial Compressors-Centrifugal Compressors24

22 https://www.flowmorepumps.com/product/horizontal-split-casing-pumps.html 23 https://www.researchgate.net/figure/Axial-flow-compressor-engine fig4 261477455 24 https://cascousa.com/compressed-air-101/types-of-compressors/dynamic-displacementcompressors/

When it comes to how this compressor works, gas is compressed with the use of an array of airfoils which are arranged in rows.
The airfoils can exist as pairs, where one of the set is a rotating airfoil known as the blade or rotor and the other is a stationary airfoil also known as stators or vanes.

While the rotating airfoil accelerates the fluid; the stationary airfoil decelerates and also redirects its direction in preparation for the rotor blades of the next stage.

## -PROS AND CONS

What this means is that the velocity of the gas is first increased before it is slowed down and passed through the blades which help to increase the gas pressure.

In comparison with other compressors, axial machines are relatively expensive since they require more parts and materials of high quality. They, however, have high efficiencies and employ multi-stages where the cross-sectional area of the gas passing along the compressor diminishes to give an optimum axial Mach number.

### 8.2.2.C) HERMETICALLY SEALED, OPEN, OR SEMI-HERMETIC

There are also compressors that are specifically designed for refrigerators. These types can either be classified as hermetically open, sealed, or semi-hectic.

Each description refers to the way the motor drive is positioned in relation to the gas that is being compressed.

## THE COMPRESSION MECHANISM



PANASONIC COMPRESSOR MALAYSIA SDN. BHD.

## 25

Design of Oil-Less Compressors and Vacuum Pumps (pdf)
https://docs.lib.purdue.edu/cgi/viewcontent.cgi?article=1017\&context=icec
https://oaktrust.library.tamu.edu/bitstream/handle/1969.1/188625/TT02.pdf?sequence=1

Denair compressor to inquire about:
http://www.denair.net/Gas Compressor/Gas Compressor.html (\#8)
$25 \mathrm{https}: / /$ na.industrial.panasonic.com/complete-guide-rotary-compressors

COMPRESSORS

(b)
(a) Structural diagram and (b) 3D model of the multistage compressor unit.

### 8.2. Gas compressors 27

### 8.2.1. Positive displacement rotary blower



Two profiled rotors turn in a figure of eight shaped housing. They are geared together so that they run very close to each other, but cannot touch. There is no compression within the machine, it simply pushes gas into the system to which it is connected. Machines with semi-screw profile rotors are also available, which reduces noise and vibration.

Typical Performance Envelope



### 8.1.1 Centrifugal blower



An impeller is attached to a rotating shaft within a cylindrical housing. Gas drawn into the housing near the centre, is then thrown towards the perimeter. The imparted velocity of the gas causes a pressure rise and flow. Multi-stage machines direct the gas back to the centre of the next stage.

Typical Performance Envelope
|||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||||l|

|  | Imperial | Metric |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |
| Maximum swept flow | 40,000 cf | 70,000 m³/h |
| Maximum casing pressure | 30 psi | 2 bar |
|  | "! ${ }^{\text {, }}$ ! ${ }^{\prime}$ |  |
| Maximum pressure ratio | 2.2 |  |

## COMPRESSORS

### 8.1.2 Rotary vane compressor



A single rotor is mounted offset in a cylindrical housing. Slots in the rotor contain vanes, which are thrown against the wall of the housing as it rotates. Oil is injected into the compression space to lubricate the bearings and vanes. As the rotor is offset, the segments that are created by the vanes vary in size through the cycle, causing the trapped gas to be compressed. Ports in the housing wall are positioned to let the gas in and out at the points of minimum and maximum pressure. Fully oil flooded versions are also available, with no oil loss to process.
Typical Performance Envelope


| Imperial <br> Metric |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Minimum swept volume | 5 cfm | $8 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum swept flow | $3,500 \mathrm{cfm}$ | $6,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum casing pressure | 250 psi | 17 bar |
|  |  |  |
| Maximum pressure ratio per stage | 3.5 |  |

### 8.1.3 Oil flooded screw compressor



Twin screw shaped meshing rotors are mounted in a figure of eight shaped housing, which has suction and discharge ports at either end. As the rotors turn they form a space that traps gas, the space travels down the length of the housing, and because of the profile of the screws, is compressed as it goes. Oil is flood injected into the compression space to lubricate the bearings and screws, and to absorb the heat of compression. The oil and compressed gas mixture subsequently passes into a deoiling vessel. The oil is then cooled and filtered and goes back round the cycle once again.

Typical Performance Envelope


|  | Imperial | Metric |
| :---: | :---: | :---: |
|  |  |  |
| Minimum swept volume | 150 cfm | $250 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum swept flow | $10,000 \mathrm{cfm}$ | $17,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum casing pressure | 500 psi | 40 bar |
|  |  |  |
| Maximum pressure ratio | 20 |  |
| Minimum pressure ratio | 2 |  |

### 8.1.4 Oil free screw compressor



Twin screw shaped meshing rotors are mounted in a figure of eight shaped housing, which has suction and discharge ports at either end. As the rotors turn they form a space that traps gas, the space travels down the length of the housing, and because of the profile of the screws, is compressed as it goes. Due to no lubricant in the compression space, timing gears are employed to ensure that the two rotors do not touch.

Typical Performance Envelope


|  | Imperial | Metric |
| :---: | :---: | :---: |
|  |  |  |
| Minimum swept volume | 120 cfm | $200 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum swept flow | 60,000 cfm | $100,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum casing pressure | 750 psi 52 bar |  |
|  |  |  |
| Maximum pressure ratio | 4 |  |

> Advantages

- Flow controllable by speed variation.
- Vibration free operation.
- No special foundation required, lowering civil costs.
- Pulsation free gas discharge.
- Valve less porting means no drop off in efficiency between overhauls, and no valves to maintain or break in service.
- No oil in contact with gas.
- Resistant to damage by particulate.
> Disadvantages
- High capital cost.
- Low pressure ratio per stage, but can be mounted in series.
> Common applications
- Refinery service.
- Flare gas recovery.


### 8.1.5 Reciprocating compressor



Similar to an automotive combustion engine, except passive non return valves replace actuated valves. A piston travels up and down inside a cylinder, and is connected to a crank shaft by a connecting rod. On the intake stroke, the discharge valves are forced shut, and gas is therefore sucked into the cylinder.

## COMPRESSORS

On the compression stroke the suction valves are forced shut, and gas is expelled into the discharge port. On multi-stage machines, the gas must be cooled before entering the next stage.

Typical Performance Envelope



### 8.2.2. Diaphragm compressor

Based on a reciprocating compressor frame. In place of conventional
 cylinders, is a saucer shaped stainless steel head, inside of which is a thin stainless steel diaphragm. The diaphragm oscillates up and down, powered by oil that is in turn pushed up and down by the piston. Gas is drawn in to the top of the head, and pushed out, in a similar manner to a reciprocating compressor, by passive poppet valves. The diaphragm totally insulates the gas stream from the mechanics and lubrication system, and so is often specified for hazardous or poisonous gas applications.

Typical Performance Envelope


| Imperial <br> Metric |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Minimum swept volume | 6 cfm | $10 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum swept flow | 1,800 cfm | $3,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum casing pressure | 15,000 psi | 1,000 bar |
|  |  |  |
| Maximum pressure ratio per stage | 20 |  |

### 8.1.6 Centrifugal compressor



An impeller is attached to a rotating shaft within a cylindrical housing. Gas drawn into the housing near the centre, is then thrown towards the perimeter. The imparted velocity of the gas causes a pressure rise and flow. Multi-stage machines direct the gas back to the centre of the next stage. Differs from centrifugal blower in that pressure containment housing is much stronger. Two main layouts are Integrally Geared type, where several stages are mounted radially on a central speed increaser gearbox, and Barrel type, where stages are all mounted on a single shaft.

## Typical Performance Envelope

|  | Imperial | Metric |
| :---: | :---: | :---: |
|  |  |  |
| Minimum swept volume | 10,000 cfm | $17,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum swept flow | 180,000 cfm | $300,000 \mathrm{~m}^{3} / \mathrm{h}$ |
|  |  |  |
| Maximum casing pressure | 2,200 psi | 150 bar |
|  |  |  |
| Maximum pressure ratio | 4 |  |

## 8.3. ---

Graph showing operating regions of various compressors


Table showing operating conditions of various compressors

Table 1b. Summary of Typical Operating Characteristics of Compressors (US Units)

|  | Inlet Capacity (acfm) | Maximum Discharge Pressure (psig) | Efficiency <br> (\%) | Operating Speed (rpm) | Maximum Power (HP) | Application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dynamic Compressors |  |  |  |  |  |  |
| Centrifugal | $\begin{gathered} 100 \\ 200,000 \end{gathered}$ | 10,000 | 70-87 | $\begin{aligned} & 1,800= \\ & 50,000 \end{aligned}$ | 50,000+ | Process gas \& air |
| Axial | $\begin{aligned} & 30,000= \\ & 500,000 \\ & \hline \end{aligned}$ | 250 | 87-90+ | $\begin{aligned} & 1,500 \\ & 10,000 \\ & \hline \end{aligned}$ | 100,000 | Mainly air |
| Positive Displacement Compressors |  |  |  |  |  |  |
| Reciprocating (Piston) | 10-20,000 | 60,000 | $80-95$ | 200-900 | 20,000 | Air \& process gas |
| Diaphragm | 0.5-150 | 20,000 | 60-70 | 300-500 | 2,000 | Corrosive \& hazardous process gas |
| Rotary Screw (Wet) | 50-7,000 | 350 | 65-70 | 1,500-3,600 | 2000 | Air, refrigeration \& process gas |
| Rotary Screw (Dry) | $\begin{aligned} & 120- \\ & 58,000 \end{aligned}$ | 15-700 | 55-70 | $\begin{aligned} & 1,000- \\ & 20,000 \end{aligned}$ | 8,000 | Air \& dirty process gas |
| Rotary Lobe | 15-30,000 | 5-25 | $55-65$ | 300-4,000 | 500 | Pneumatic conveying, process gas \& vacuum |
| Sliding Vane | 10-3,000 | 150 | 40-70 | 400-1,800 | 450 | Vacuum service \& process gas |
| Liquid Ring | $5-10,000$ | 80-150 | 25-50 | 200-3,600 | 400 | Vacuum service \& corrosive process gas |

Capacity and Pressure Range of various compressors

| Type of compressor | capacity range (m $\left.\mathbf{m}^{3} / \mathbf{h}\right)$ | Working pressure <br> (bar) |
| :---: | :---: | :---: |
| Roots blower compressor |  | $0.1-1$ |
| Single stage | $100-30000$ |  |
| Reciprocating <br> compressor |  | $0.8-12$ |
| Single stage | $100-12000$ | $12-700$ |
| Multi stage | $100-12000$ | $0.8-13$ |
| Screw compressor | $100-2400$ | $0.8-24$ |
| Single stage | $100-2200$ | $0.1-450$ |
| Multi stage | $600-300000$ |  |
| Centrifugal |  |  |

Advantages and disadvantages of positive displacement
type compressor

|  | Advantages | Disadvantages |
| :--- | :--- | :--- |
| Positive displacement <br> compressor |  |  |
| Reciprocating | -Wide pressure ratios <br> -High efficiency | -Heavy foundation required <br> -Flow pulsation <br> -High maintenance |
| Diaphragm |  |  |
|  | -Very high pressure <br> -Low flow <br> -No moving seal | -Limited capacity range <br> -Periodic replacement of <br> diaphragm |
| Screw |  |  |

## selection of compressor lubricants

The major factors involved in the selection of compressor lubricants include:

- Type, size and speed of compressor
- Gas being compressed
- Number of stages
- Pressure and temperature at each stage
- Environment
- Type of lubrication system


### 8.4. Oil-free screw air compressor process



The oil-free industrial air compressor is a two-stage oil-free compressor unit. both compression stages comprise male and female rotors, with special protective coating. there's no physical contact either between the matched rotor pairs or the rotors and the air and casing. everything is separated by a precisely engineered air gap. The male rotors of both the first and second stages are driven by a single main gear at the back of the air end.


Helical timing gears at the front of both sets of rotors ensure perfect synchronization is kept between the rotor pairs at all times. This means no oil is needed to seal the compression process, making this air end a perfect solution wear oil-free compressed air is a critical requirement. Oil never enters the compression chambers, but is used to keep gears and bearings lubricated and cool. Special seals between the rotors and bearings prevent air passing into the oil system and oil passing into the compression chambers.
Hot oil drains to an oil reservoir located below the air and via to oil returned pipes. The hot oil is then pumped to a cooler and returns to the air environ oil filter. A pressure relief valve fitted to the front of the air and ensures that oil pressure doesn't exceed 2.5 bar or 36 psi.


Oil is topped up via a fillip pipe at the front to the air end. The compression process is kept cool by a constant flow of water passing through channels that surround the air end rotors. Heat transfers to the water which is then pumped through an external cooler before returning to the air end.

Air enters the third stage via the air intake valve and is trapped between the lobes and flutes on the underside of the compression rotors. As the rotors turn the volume of the trapped air reduces compressing the air and driving it towards the delivery port at the back of the air end. After leaving the first stage the compressed air passes through a pulsation damper, then on to a first stage or inter stage cooler. This can either be air or water cooled depending on the model of compressor. It's important to cool the air before it enters the second stage as hot air will have expanded.


When cooled, the air contract providing a greater number of air molecules in the same volume, this results in more efficient second stage compression. The cooled compressed air passes through a moisture separator, then on to the inlet port of the second stage. The volume of the air is greatly reduced after first stage compression, which means that the size of the second stage rotors can be smaller. The second stage further compresses the air to the required pressure in the same manner as the first stage. However, this time, the compression process takes place on the upper side of the rotors. the compressed air exits the air and fire a delivery silencer then through a non-return valve.


The air then passes through a final second stage air or water cooling process to ensure the delivery air is at the right temperature. Then after a final journey through a moisture separator, the air is ready to exit the compressor at the delivery port.

### 8.5. Overview of Screw Compressor Operation Oil Free

The obvious thought is that the term 'Oil free compressor' describes a compressor containing no oil. Unfortunately, that is not the case for most oil free compressors. An oil free compressor is the term used to describe a compressor that does not use oil in its compression stage.

## Basic Operation - Oil Free Rotary Screw Compressor

| Intake <br> Filter | LPAir End | Inter Cooler | After Cooler |
| :---: | :---: | :---: | :---: |



## Drive

Oil free rotary screw compressors are typically multi stage, driven by a single drive motor. This motor will drive a gear which in turn distributes the power to each air end. Some oil free screw compressors are now available where each compression stage driven by an individual motor

## Compression

Unlike the oil injected screw compressor which uses oil to seal the gaps between the rotors and provide compression, oil free variants achieve compression in an alternative way.

Rotor elements are manufactured in pairs with extremely tight tolerances to decrease the gap between them. During operation, rotors are spun at much higher speeds than an equivalent oil injected ompressor. Specialist coatings are often applied to the rotors to give some of the protection from water and heat usually provided by oil.

The rotors operate extremely close to each other, however as there is no oil in the compression stage to prevent the rotors from touching, the distance between each rotor is maintained by additional gearing.


## Cooling

As there is no oil in the compression chamber to provide direct cooling, indirect cooling is used. The air end housings of oil free compression stages typically contain gelleries in which cooling water (on water cooled machines) or oil (on air cooled machines) can be circulated. This process is not as efficient as direct cooling as it only cools the casing and not the compressed air or the rotors.

Due to the lack of direct cooling in an oil free compressor, the compressed air and rotors reach much higher temperatures. Oil-free compressors
 therefore obtain their final discharge pressure in stages (as opposed to oil injected machines which typically use only 1 stage). Between stages they will cool the compressed air with an inter-cooler. This keeps typical air end temperatures between $180^{\circ} \mathrm{C} \& 200^{\circ} \mathrm{C}$.
For example, on a typical oil free rotary screw compressor with 2 compression stages, an intercooler and aftercooler. Stage 1 will typically compress the air up to a pressure around 3.5 bar g, stage 2 will then compress the air to the discharge pressure of 7 bar $g$.

## Lubrication

On an oil free screw compressor, it is not only important that the individual rotors in each air end are synchronised with gears, with only one drive motor, additional gearing is also required to drive each of the air ends. All of the gearing and bearings require lubrication. So although the name implies that an oil free compressor is "oil less", for most oil free compressors sold, this is not the case. Oil is not used in the compression stages; however, oil is still required for lubrication and cooling of other components. This oil is pumped around the compressor forming a closed loop system which lubricates bearings and gears, is filtered, cooled and recirculated.

## Oil Reclamation (Air / Oil Separator)

As there is no oil used in the compression stage, there is no requirement for an air / oil separator on an oil free compressor.


Compressor \#1: (info completed)
https://www.oxygen-compressors.com/2m3-High-Pressure-Industrial-Booster-Oxygen-Compressor-pd46014866.html

GOW-3/4-150 Micro oxygen compressor function indication map cylinder material:



## suction pressure

## 1st stage discharge pressure discharge pressure


suction pressure switch discharge pressure switch

| Model 型号 | Working medium | suction <br> pressure <br> (Mpa,Psig) | Discharge pressure (Mpa,Psig) | Motor.KW | Flow <br> rate <br> Nm3/hr | Voltage | Cooling way | weight | dimension |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GOW-1.8/1-150 | oxygen | 0.1, 14.3 | 15,2150 | 1.5 | 1.8 | $\begin{aligned} & 220 \mathrm{~V} / 380 \mathrm{~V} \\ & / 415 \mathrm{~V} / 440 \mathrm{~V} \\ & 50 / 60 \mathrm{HZ} \end{aligned}$ | air cooling | 150kgs | $700 \times 650 \times 650$ |
| GOW-1.8/1-200 | oxygen | 0.1, 14.3 | 20,2875 | 1.5 | 1.8 | $\begin{aligned} & 220 \mathrm{~V} / 380 \mathrm{~V} \\ & / 415 \mathrm{~V} / 440 \mathrm{~V} \\ & 50 / 60 \mathrm{HZ} \end{aligned}$ | air cooling | 150kgs | $700 \times 650 \times 650$ |
| GOW-2.7/1-150 | oxygen | 0.1, 14.3 | 15,2150 | 2.2 | 2.7 | $\begin{aligned} & 220 \mathrm{~V} / 380 \mathrm{~V} \\ & / 415 \mathrm{~V} / 440 \mathrm{~V} \\ & 50 / 60 \mathrm{HZ} \end{aligned}$ | air cooling | 150 kgs | $700 \times 650 \times 650$ |
| GOW-3/4-150 | oxygen | 0.3-0.4,40-60 | 15,2150 | 3 | 3 | $\begin{aligned} & 220 \mathrm{~V} / 380 \mathrm{~V} \\ & / 415 \mathrm{~V} / 440 \mathrm{~V} \\ & 50 / 60 \mathrm{HZ} \end{aligned}$ | air cooling | 150kgs | $700 \times 650 \times 650$ |

[^5]NOTICE：THE OXYGEN MUST BE OIL FREE TOTALLY OIL FREE OXYGEN COMPRESSOR TECHNICAL DATA

| S／N |  | ITEMS | PARAMETER |
| :---: | :---: | :---: | :---: |
| 1 | WORKING MEDIUM |  | OXYGEN O2 |
| 2 | MODEL |  | GOW－3／4－150 |
| 3 | STRUCTURE |  | 100\％OIL FREE RECIPROCAIING COMPRESSOR |
| 4 | PRESSURE STAGE |  | 2 |
|  | Cylinder |  | 2 |
| 5 | OXYGEN CAPACITY（STANDARDCONDIIIONMNm |  | 3 |
| 6 | RATE INPUT MPa（G） |  | 0．3－0．4 |
| 7 | RATED OUTPUT MPa（G） |  | 15.0 |
| 8 | INLET TEMPERATUREC |  | $\leqslant 40$ |
| 9 | DISCHARGE TEMPERATURE＇C |  | $\leqslant 50$ |
| 10 | TRANSMIT TEMPERATURE＇${ }^{\text {c }}$ |  | $\leqslant 50$ |
| 11 | PUMP SPEED I／min |  | 400 漛 |
| 12 | COOLING WAY |  | AIR COOLING |
| 13 | $\begin{gathered} \text { LUBRIC } \\ \text { ATE } \\ \text { WAY } \end{gathered}$ | CRANK SHAFT－ CONNECTROD | SEAL GREASE |
|  |  | CYLINDER | OIL FREE LUBRICATE |
| 14 | MOTOR POWER Kw |  | 3 水 |
| 15 | TRANSMIT WAY |  | BELT DRIVEN |
| 16 | INSTALLATITON WAY |  | HAS BASEMENT |
| 17 | Automatic control items |  | Pressure over loading |
| 18 | Dimension $\mathrm{L} \times \mathrm{W} \times \mathrm{H}$ mm |  | $700 \times 650 \times 650$ 泳 |
| 19 | Inlet and outlet mm |  | 15 |
| 20 | Weight Kg |  | 150KGS 溫 |
| 21 | GW |  | 190KGS |
| 22 | Motor |  | 220V 60HZ 3PHASE |
| 23 | Working model |  | 6－8hours per day |

GOW－3／4－150 FOB SHANGHAI USD8000／PC


## COMPRESSORS



Compressor \#2: (info uncompleted)
https://toplongcompressor.en.made-in-china.com/product/lvVmtGBbhyhA/China-5nm3-3stage-High-Pressure-Oil-Free-Oxygen-Compressor-Nitrogen-Compressor.html


5nm3 3stage High Pressure Oil Free Oxygen Compressor Nitrogen Compressor

| Get Latest Price > |  |
| :--- | :--- |
| Min. Order/Reference FOB Price |  |
| 1 Piece | US $\$ 6,500-8,000 /$ Piece |
| Port: | Shanghai, China © $\varnothing$ |
| Production Capacity: | 200PCS/Month |
| Payment Terms: | L/C, T/T, D/P, Western Union, Paypal, Money Gram |
| Lubrication Style: | Oil-free |
| Cooling System: | Air Cooling |
| Cylinder | Balanced Opposed Arrangement |
| Arrangement: | Vertical |
| Cylinder Position: | Closed Type |
| Structure Type: | Multistage |

Product Description
Oil-free Special Gas Compressor
Oil-free special gas compressor booster is the kind of semi-hermetic compressor, it adopts hermetic construction for its motor without pollution to the medium to be compressed and without leakage. This series compressor has numerous advantage of reliable performance, simple operation, compact construction, quick connection and so on. It can be applied in the compression and recovery of toxic, rare and precious gas such as SF6, helium, methane, ammonia, Freon, carbon dioxide and so on.

Performance Characteristics

Oil free high pressure oxygen nitrogen helium Co2 gas compressor
Principle 1: Oil-free type reciprocating piston
2 Cooling Type: Air-cooled or water-cooled
(3) Power consumption: $\leq 110 \mathrm{kw} 4$ Speed: . $300-560 \mathrm{rpm}$

5 Flow: . $\leq 2000 \mathrm{Nm} 3 / \mathrm{h} 6$
Suction pressure: . 0-5Mpa7
Exhaust pressure: . $\leq 16.5 \mathrm{Mpa} 8$ Compression Level: 1-4Winds oil-free compressors
Product Features: No oil lubrication with clean and non-polluting.
High efficiency, low energy consumption. High reliability, continuous 24 -hour operation. The unit uses air-cooled or water-cooled, compact structure, operation and low maintenance cost

4-20m3 3 stage pressure high pressure bottle compressor oxygen concentrator
3stage pressure filling pressure 15 mpa
capacity from 4 nm 3 to 20 nm 3 per hour

All our models can be customized. For more information, pleaes do not hesitate to contact.

| Model | gas | inlet <br> .barg | outlet .barg | flow rate NM3/hr | power.KW | voltage/frequency | inlet/outlet.mm | cooling way | net eight.kg | dimension.mm | pressure riato stage |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GOWW-4-10/4-150 | oxygen | 3-4 | 150 | 4-10 | 3 | $\begin{array}{\|l\|} \hline 220 / 380 \\ / 440 / 50 / 60 / 3 \end{array}$ | DN15/M16X1.5 | air cooling | 380 | 1300X750X1000 | 3stage |
| GOWW-11-20/4-150 | oxygen | 3-4 | 150 | 11-20 | 4-7.5 | $\begin{array}{\|l} 220 / 380 \\ / 440 / 50 / 60 / 3 \end{array}$ | DN15/M16X1.5 | air cooling | 420 | 1300X750X1000 | 3stage |

Compressor \#3: (info uncompleted)
https://toplongcompressor.en.made-in-china.com/product/oXcQMuqdpshw/China-Totally-Oil-Free-Oxygen-Argon-Hydrogen-Compressor.html


## COMPRESSORS

Product Description
Oil-free Special Gas Compressor

Oil-free special gas compressor booster is the kind of semi-hermetic compressor, it adopts hermetic construction for its motor without pollution to the medium to be compressed and without leakage. This series compressor has numerous advantage of reliable performance, simple operation, compact construction, quick connection and so on. It can be applied in the compression and recovery of toxic, rare and precious gas such as SF6, helium, methane, ammonia, Freon, carbon dioxide and so on.

Performance Characteristics

Oil free high pressure oxygen nitrogen helium Co2 gas compressor
Principle 1: Oil-free type reciprocating piston
2 Cooling Type: Air-cooled or water-cooled
(3) Power consumption: $\leq 110 \mathrm{kw} 4$ Speed: . 300-560rpm

5 Flow: . $\leq 2000$ Nm3 / h6
Suction pressure: . 0-5Mpa7
Exhaust pressure: . $\leq 16.5 \mathrm{Mpa8}$ Compression Level: $1-4$ Winds oil-free compressors
Product Features: No oil lubrication with clean and non-polluting.
High efficiency, low energy consumption. High reliability, continuous 24 -hour operation. The unit uses air-cooled or water-cooled, compact structure, operation and low maintenance cost

All our models can be customized. For more information, pleaes do not hesitate to contact.

| Model | GOW-3/4-150 |
| :--- | :---: |
| Medium | O2,N2,argon,helium,hydrogen,biogas etc |
| Power(Hp,Kw) | 22KW |
| Working Pressure(Bar,Psi) | 150,2160 |
| Air Delivery(L/min,CFM) | $3 \mathrm{Nm} 3 / \mathrm{Hr}$ |
| Inlet pressure ,outlet pressure | $0.2-0.4 \mathrm{Mpa},<16.5 \mathrm{Mpa}$ |
| Speed(r.p.m) | $200-400$ |
| pressure stage | 2 |
| Net Weight(Kgs) | 110 |
| Cooling way | Air cooling |
| dimension | $830^{\star} 600 \star 640 \mathrm{~mm}$ |

Compressor \#4: (same family of compressor \#1)

## http://www.cnsouair.com/compressor/CompAirsGasCompressor/1326.htm

https://souair.en.alibaba.com/
email: ironcai@cnsouair.com
WhatsApp:008618121319076

## Oil-Free Lubricating Oxygen O2 Gas Compressor

## Technical data sheet:

Must keep the complete oil free for the gas(O2 before get into compressor

| SN. | Items | Unit | Performance parameters |
| :---: | :--- | :---: | :--- |
| 1 | Model |  | GOW-3/3-150 |
|  |  |  | Oil Free Reciprocating compressor |
| 2 | Structure |  | Vertical four stage compressed |
| 2 | Compressed stage |  | 4 |
| 3 | Compressed media |  | 0xygen 02 |
| 4 | Suction pressure | $\mathrm{MPa}(\mathrm{g})$ | $0.3-0.5$ |
| 5 | Discharge pressure | $\mathrm{MPa}(\mathrm{g})$ | 15.0 |
| 6 | Flow capacity | $\mathrm{Nm} / \mathrm{h}$ | $3 @$ suction Pressure= $0.3 \mathrm{MPa} \mathrm{(g)}$ |
| 7 | Running speed | rpm | 400 |
| 8 | Motor Power | kw | 2.2 |
| 9 | Cooling type |  | air cooled |
| 10 | Driven type |  | V -Belt |
| 11 | Lubricating | Cylinder: <br> crankcase, |  |
| 12 | connection rod: sealing grease |  |  |
| 12 | Inlet temperature | ${ }^{\circ} \mathrm{C}$ | $\leqslant 45$ |
| 13 | Outlet temperature | ${ }^{\circ} \mathrm{C}$ | $\leqslant 130$ |


| 13 | Gas Transport temperature | ${ }^{\circ} \mathrm{C}$ | $\leqslant 50$ |
| :---: | :--- | :---: | :--- |
| 14 | Inlet size |  | $\mathrm{M} 14 * 1.5$ |
| 15 | Outlet size |  | $\mathrm{M} 14 * 1.5$ |
| 16 | Control module |  | Automatic |
| 17 | Net weight | KG | 200 |
| 18 | Dimension $(\mathrm{L} * W * \mathrm{H})$ | mm | $900 \times 800 \times 1000$ |
| 19 | Installation |  | Fixed base |
| 20 | Unit price USD/SET | USD | 7100 (FOB Shanghai, China) |
| 21 | Lead Time | Davs | 30 |
| 22 | Power source |  | $380 \mathrm{~V} / 50 \mathrm{~Hz} / 3 \mathrm{PH}$ |

※ some parameter will be changed according to design.
Pipeline system,Cooler system,Valve system,Cylinder is all Stainless steel material.


GOW-3/4-150


Bidder: Shanghai Souair International Trade Co., Ltd

Add: R1403 A-Bld No. 1370Zhennan Road,Shanghai,China.

Buyer: NLAP (North Lebanon Alternative Porwer) Corporation,
Address: Harba Building, next to Hospital Albert Haykal, Ras Masqa, Lebanon
Commercial Quotation

| Name of Vendor : <br> Shanghai Souair International Trade Ltd |  |  | FCA Shanghai, China |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Currency: | USD |
| No. | Description | Model / <br> Main Parameters | Qty | Unit Price | Total Price |
| 1 | Oil Free Reciprocating Oxygen gas compressor | Model GOW-3/3-150, Inlet pressure 3-5Barg,Discharge pressure 150Barg,3Nm3/hr Flow capacity, 2.2 KW 380 V 50 HZ 3PH IP55,V-Belt Driven,Air Cooled Type,4stage compressed | 1 | 7,100.00 | 7.100.00 |
|  | Shipping charge from shanghai, china to Beirut seaport, Lebanon by sea |  |  |  | 400.00 |
|  | CNF Beirut,Lebanon(USD) |  |  |  | 7,500.00 |
|  | Shipping time to Beirut,Lebanon by sea: 25 Days |  |  |  |  |

Manufacturer of Compressor: souair
Country Of Origin: China
Lead Time: usual 30-40 Days upon order, confirmed by the order.
Payment term: $40 \% \mathrm{TT}$ in advance, then $60 \% \mathrm{TT}$ before delivery.
Price: USD Based on CNF Beirut,Lebanon.
Warranty: 12Month after commission or 18 month after the shipping.
Validity: one month

Compressor \#5:
https://www.oxywise.com/en/products/oxygen-hp-compressor?gclid=EAlaIQobChMI84-M8euo7wIVQe7tCh2CnAb-EAAYASAAEgLM3vD BwE
I am looking for an oxygen compressor (oil-free) taht has the following specifications:
inlet pressure : 1 bar - 5 bar
outlet pressure : 100 bar
flow rate: more than $800 \mathrm{~L} / \mathrm{hr}$
Oxywise Answer: (Monday 15.3.2021)
I'm sorry we don't have a RIX unit that small.
I can offer an unbranded CE marked Oxygen compressor?
Price is circa $€ 8 \mathrm{k}$. Leadtime 5 weeks.

## 9. Calculation of Oxygen flow rate outlet by electrolysis:

- Power : 2.4 kW (voltage $=4 \mathrm{~V}$; current $=150 \mathrm{~A}$ )

O Gas flow rate Hydrogen all stacks $=2.27 \mathrm{~L} / \mathrm{min}=136.2 \mathrm{~L} / \mathrm{hr}$
O Gas flow rate Oxygen all stacks $=1.13 \mathrm{~L} / \mathrm{min}=67.8 \mathrm{~L} / \mathrm{hr}$

- Power : 25 kW

O Gas flow rate Hydrogen all stacks $=23.65 \mathrm{~L} / \mathrm{min}=1418.75 \mathrm{~L} / \mathrm{hr}$
O Gas flow rate Oxygen all stacks $=11.77 \mathrm{~L} / \mathrm{min}=706.25 \mathrm{~L} / \mathrm{hr}$

## 10. Prototype of refrigerator

10.1. Prototype 1 : Laboratory fridge




reforgerator compressor R134A Fridge compressor

| Parameters |  |
| :--- | :--- |
| Specification |  |
| Production Facility | Brazil |
| Brand | Embraco |
| Compressor Type | Hermetic Reciprocating |
| Application | HBP $\left(+7,2^{\circ} \mathrm{C} /+54,4^{\circ} \mathrm{C}\right)$ |
| H.Power | $3 / 8$ |
| Power Supply | $220-240 \mathrm{~V}$ |
| Refrigerant | R 134 a |
| Cooling Capacity (Watt) | 1.316 |
| Motor Type | 1 Phase -RSIR |
| BoM. | 513200015962 A |
| Compressor Model | FFI 12 HBK |
| Diplacement (cm3/rev) | 11,14 |
| Frequency (Hz) | 50 |
| Suction Line | $5 / 16^{\prime \prime}$ |
| Discharge Line | $1 / 4^{\prime \prime}$ |

## embracs

## COMPRESSOR DEFINITION

| Designation | F FI12HBK |
| :--- | :--- |
| Nominal Voltage/Frequency | $\mathbf{2 2 0 - 2 4 0}$ V $\mathbf{5 0 ~ H z}$ |
| Engineering Number | $\mathbf{5 1 3 2 0 0 0 1 5}$ |

## A - APPLICATION / LIMIT WORKING CONDITIONS

| 1 Type | Hermetic reciprocating compressor |  |  |
| :---: | :---: | :---: | :---: |
| 2 Refrigerant | $\mathrm{R}-134 \mathrm{a}$ |  |  |
| 3 Nominal voltage and frequency | 220-240/50 [V/Hz] |  |  |
| 4 Application type | Low-Medium-High Back Pressure |  |  |
| 4.1 Evaporating temperature range | $-35^{\circ} \mathrm{C}$ to $15^{\circ} \mathrm{C}$ | $\left(-31^{\circ} \mathrm{F}\right.$ to $\left.59^{\circ} \mathrm{F}\right)$ |  |
| 5 Motor type | RSIR/CSIR |  |  |
| 6 Starting torque | LST - Low Starting Torque |  |  |
| 7 Expantion device | Capillary tube |  |  |
| 8 Compressor cooling |  | Operating voltage range |  |
|  |  | 50 Hz | 60 Hz |
| 8.1 LBP ( $32^{\circ} \mathrm{C}$ Ambient temperature) | Fan | 198 to 255 V | - |
| 8.2 LBP ( $43^{\circ} \mathrm{C}$ Ambient temperature) | Fan | 198 to 255 V | - |
| $8.3 \mathrm{HBP}\left(32^{\circ} \mathrm{C} \mathrm{Ambient} \mathrm{temperature)}\right.$ | Fan | 198 to 255 V | - |
| $8.4 \mathrm{HBP}\left(43^{\circ} \mathrm{C} \mathrm{Ambient} \mathrm{temperature)}\right.$ | Fan | 198 to 255 V | - |
| 9 Maximum condensing pressures/temperature |  |  |  |
| 9.1 Operating (gauge) | 16.2 | [kgf/cm ${ }^{2}$ ] (230 psig) | $1{ }^{\circ} \mathrm{C}-{ }^{\circ} \mathrm{F}$ |
| 9.2 Peak (gauge) | 20.6 | [kgf/cm²] (293 psig) | $1{ }^{\circ} \mathrm{C}-{ }^{\circ} \mathrm{F}$ |
| 10 Maximum winding temperature | 130 | [ ${ }^{\circ} \mathrm{C}$ ] |  |

B - MECHANICAL DATA

| 1 Commercial designation | 1/3+ | [hp] |
| :---: | :---: | :---: |
| 2 Displacement | 11.14 | [ $\mathrm{cm}^{3}$ ] (0.680 cu.in) |
| 2.1 Bore [mm] | 26.000 |  |
| 2.2 Stroke [mm] | 21.000 |  |
| 3 Lubricant charge | 280 | [ml] (9.47 fl.oz.) |
| 3.1 Lubricants approved |  |  |
| 3.2 Lubricants type/viscosity | ESTER / ISO22 |  |
| 4 Weight (with oil charge) | 10.9 | [kg] (24.03 lb.) |
| 5 Nitrogen charge | 0.2 to 0.3 | [kgf/cm ${ }^{2}$ ](2.84 to 4.27 psig$)$ |

C - ELETRICAL DATA

| 1 Nominal Voltage/Frequency/Number of Phases | 220-240 V $50 \mathrm{~Hz} 1 \sim$ (Single phase) |
| :---: | :---: |
| 2 Starting device type | Current Relay |
| 2.1 Starting device | 213516035/213516043 |
| 3 Start capacitor | 88-108(220) [ $\mu \mathrm{F}(\mathrm{VAC}$ minimum )] |
| 4 Run capacitor | [ $\mu \mathrm{F}$ (VAC minimum ) ] |
| 5 Motor protection | CP4TMF210N52A2 |
| 6 Start winding resistance | 29.90 [ $\Omega$ at $\left.25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)\right]+/-8 \%$ |
| 7 Run winding resistance | 5.70 [ $\Omega$ at $\left.25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)\right]+/-8 \%$ |
| 8 LRA - Locked rotor amperage ( 50 Hz ) | 20.00 [A] - Measured according to UL 984 |
| 9 FLA - Full load amperage L/MBP ( 50 Hz ) | 2.50 [A] - Measured according to UL 984 |
| 10 FLA - Full Load Amperage HBP ( 50 Hz ) | 3.00 [A] - Measured according to UL 984 |
| 11 Approval boards certification | CCC - IRAM - UL - VDE |

## COMPRESSORS

D - PERFORMANCE - CHECK POINT DATA

| TEST CONDITIONS: <br> @220V50Hz |  |  | ASHRAEHBP32 Fan |  | Evaporating temperature (Condensing temperature |  | $\begin{aligned} & 7.2^{\circ} \mathrm{C}\left(44.96^{\circ} \mathrm{F}\right) \\ & \left.54.4^{\circ} \mathrm{C}\left(129.92^{\circ} \mathrm{F}\right)\right) \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cooling capacity |  |  | Power consumption $+/-5 \%$ | Current consumption $+/-5 \%$ | $\begin{aligned} & \text { Gas flow } \\ & \text { rate } \\ & +/-5 \% \end{aligned}$ | EFFICIENCY RATE |  |  |
| [Btu/h] | [kcal/h] | [W] | [W] | [A] | [kg/h] | [Btu/Wh] | [kcal/ Wh ] | [W/W] |
| 4492 | 1132 | 1316 | 504 | 2.79 |  | 8.91 | 2.25 | 2.61 |
| TEST CON <br> @220V5 | ONS: | ASHRAELBP32 Fan |  |  | Evaporating temperature (Condensing temperature |  | $\begin{aligned} & -23.3^{\circ} \mathrm{C}\left(-9.94^{\circ} \mathrm{F}\right) \\ & \left.54.4^{\circ} \mathrm{C}\left(129.92^{\circ} \mathrm{F}\right)\right) \end{aligned}$ |  |
| Cooling capacity |  |  | Power consumption $+/-5 \%$ | Current consumption $+/-5 \%$ | $\begin{aligned} & \text { Gas flow } \\ & \text { rate } \\ & +/-5 \% \end{aligned}$ | EFFICIENCYRATE |  |  |
| [Btu/h] | [kcal/h] | [W] | [W] | [A] | [kg/h] | [Btu/Wh] | [kcal/Wh] | [W/W] |
| 1090 | 275 | 319 | 256 | 1.96 | 6.19 | 4.26 | 1.07 | 1.25 |

E - PERFORMANCE - CURVES

| TEST CONDITIONS: @220V50Hz | ASHRAE32 <br> Fan |  |  |  | (Condensing temperature $45^{\circ} \mathrm{C}\left(+113^{\circ} \mathrm{F}\right)$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Evaporating temperature | Cooling capacity$+/-5 \%$ |  |  | Power consumption $+/-5 \%$ | Current consumption $+/-5 \%$ | $\begin{aligned} & \text { Gas flow } \\ & \text { rate } \\ & +/-5 \% \end{aligned}$ |  | CIENCY $+/-7 \%$ |  |
| ${ }^{\circ} \mathrm{C} \quad\left({ }^{\circ} \mathrm{F}\right)$ | [Btu/h] | [kcal/h] | [W] | [W] | [ A ] | [kg/h] | [Btu/Wh] | [kcal/Wh] | [W/W] |
| -35 (-31) | 553 | 139 | 162 | 187 | 1.87 | 3.13 | 2.94 | 0.74 | 0.86 |
| -30 (-22) | 762 | 192 | 223 | 214 | 1.91 | 4.33 | 3.62 | 0.91 | 1.06 |
| -25 (-13) | 1038 | 262 | 304 | 242 | 1.97 | 5.90 | 4.35 | 1.10 | 1.27 |
| -20 (-4) | 1383 | 348 | 405 | 272 | 2.05 | 7.87 | 5.12 | 1.29 | 1.50 |
| -15 (+5) | 1799 | 453 | 527 | 303 | 2.13 | 10.26 | 5.94 | 1.50 | 1.74 |
| -10 (+14) | 2289 | 577 | 671 | 336 | 2.23 | 13.10 | 6.80 | 1.71 | 1.99 |
| $-5 \quad(+23)$ | 2853 | 719 | 836 | 370 | 2.35 | 16.41 | 7.69 | 1.94 | 2.25 |
| 0 (+32) | 3495 | 881 | 1024 | 406 | 2.47 | 20.21 | 8.60 | 2.17 | 2.52 |
| +5 (+41) | 4217 | 1063 | 1236 | 442 | 2.60 | 24.54 | 9.52 | 2.40 | 2.79 |
| +10 (+50) | 5019 | 1265 | 1471 | 480 | 2.75 | 29.41 | 10.46 | 2.64 | 3.07 |
| +15 (+59) | 5905 | 1488 | 1730 | 518 | 2.90 | 34.86 | 11.40 | 2.87 | 3.34 |


| TEST CONDITIONS: @220V50Hz |  |  | ASHRAE32 <br> Fan |  |  | (Condensing temperature ${55^{\circ}}^{\circ} \mathrm{C}\left(+131^{\circ} \mathrm{F}\right)$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Evap temp | ating <br> ature | Cooling capacity$+/-5 \%$ |  |  | Power consumption $+/-5 \%$ | Current consumption $+/-5 \%$ | $\begin{aligned} & \text { Gas flow } \\ & \text { rate } \\ & +/-5 \% \end{aligned}$ |  | CIENCY $+/-7 \%$ |  |
| ${ }^{\circ} \mathrm{C}$ | $\left({ }^{\circ} \mathrm{F}\right)$ | [Btu/h] | [kcal/h] | [W] | [W] | [A] | [kg/h] | [Btu/Wh] | [kcal/Wh] | [W/W] |
| -35 | (-31) | 514 | 130 | 151 | 184 | 1.89 | 2.91 | 2.71 | 0.68 | 0.79 |
| -30 | (-22) | 713 | 180 | 209 | 215 | 1.93 | 4.05 | 3.31 | 0.83 | 0.97 |
| -25 | (-13) | 974 | 245 | 285 | 247 | 2.00 | 5.54 | 3.95 | 1.00 | 1.16 |
| -20 | (-4) | 1300 | 328 | 381 | 282 | 2.08 | 7.40 | 4.62 | 1.16 | 1.35 |
| -15 | (+5) | 1693 | 427 | 496 | 319 | 2.18 | 9.65 | 5.32 | 1.34 | 1.56 |
| -10 | (+14) | 2155 | 543 | 631 | 357 | 2.30 | 12.33 | 6.03 | 1.52 | 1.77 |
| -5 | (+23) | 2687 | 677 | 787 | 398 | 2.44 | 15.44 | 6.76 | 1.70 | 1.98 |
| 0 | (+32) | 3292 | 830 | 965 | 440 | 2.59 | 19.03 | 7.50 | 1.89 | 2.20 |
| +5 | (+41) | 3972 | 1001 | 1164 | 483 | 2.75 | 23.11 | 8.23 | 2.08 | 2.41 |
| +10 | (+50) | 4729 | 1192 | 1386 | 528 | 2.93 | 27.71 | 8.97 | 2.26 | 2.63 |
| +15 | (+59) | 5565 | 1402 | 1631 | 575 | 3.12 | 32.85 | 9.69 | 2.44 | 2.84 |

## E - PERFORMANCE - CURVES

| TEST CONDITIONS: <br> @220V50Hz | ASHRAE32 <br> Fan |  |  |  | (Condensing temperature $65^{\circ} \mathrm{C}\left(+149{ }^{\circ} \mathrm{F}\right)$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Evaporating temperature | Cooling capacity$+/-5 \%$ |  |  | Power consumption +/-5\% | Current consumption $+/-5 \%$ | $\begin{aligned} & \text { Gas flow } \\ & \text { rate } \\ & +/-5 \% \end{aligned}$ |  | CIENCYR $+/-7 \%$ |  |
| ${ }^{\circ} \mathrm{C} \quad\left({ }^{\circ} \mathrm{F}\right)$ | [Btu/h] | [kcal/h] | [W] | [W] | [ A ] | [kg/h] | [Btu/Wh] | [kcal/Wh] | [WN] |
| -35 (-31) | 395 | 100 | 116 | 175 | 1.87 | 2.22 | 2.32 | 0.58 | 0.68 |
| -30 (-22) | 608 | 153 | 178 | 211 | 1.92 | 3.46 | 2.91 | 0.73 | 0.85 |
| -25 (-13) | 880 | 222 | 258 | 249 | 2.00 | 5.01 | 3.53 | 0.89 | 1.03 |
| -20 (-4) | 1212 | 305 | 355 | 289 | 2.10 | 6.90 | 4.16 | 1.05 | 1.22 |
| -15 (+5) | 1606 | 405 | 471 | 332 | 2.22 | 9.16 | 4.81 | 1.21 | 1.41 |
| -10 (+14) | 2065 | 520 | 605 | 377 | 2.37 | 11.82 | 5.45 | 1.37 | 1.60 |
| $-5 \quad(+23)$ | 2590 | 653 | 759 | 424 | 2.53 | 14.89 | 6.09 | 1.54 | 1.79 |
| 0 (+32) | 3183 | 802 | 933 | 474 | 2.71 | 18.40 | 6.73 | 1.70 | 1.97 |
| +5 (+41) | 3847 | 970 | 1127 | 525 | 2.91 | 22.38 | 7.34 | 1.85 | 2.15 |
| +10 (+50) | 4583 | 1155 | 1343 | 578 | 3.13 | 26.85 | 7.94 | 2.00 | 2.33 |
| +15 (+59) | 5394 | 1359 | 1581 | 633 | 3.36 | 31.84 | 8.51 | 2.14 | 2.49 |

F - EXTERNAL CHARACTERISTICS

| 1 Base plate | Universal EG/F/AMEM version 2 |  |  |
| :---: | :---: | :---: | :---: |
| 2 Tray holder | No |  |  |
| 3 Connectors |  |  |  |
| 3.1 SUCTION | $8.2+0.12 /-0.08$ | [mm] | (0.323" +0.005 "/-0.003") |
| 3.1.1 Material | Copper |  |  |
| 3.1.2 Shape | Straight |  |  |
| 3.2 DISCHARGE | $6.5+0.12 /-0.08$ | [mm] | (0.256" +0.005 "/-0.003") |
| 3.2.1 Material | Copper |  |  |
| 3.2.2 Shape | Straight |  |  |
| 3.3 PROCESS | $6.5+0.12 /-0.08$ | [mm] | (0.256" +0.005 "/-0.003") |
| 3.3.1 Material | Copper |  |  |
| 3.3.2 Shape | Straight |  |  |
| 3.4 Oil cooler (Copper) | No | [mm] |  |
| 3.5 Connector sealing | Rubber Plugs |  |  |

## - R134a refrigerant:

R134a is also known as Tetrafluoroethane (CF3CH2F) from the family of HFC refrigerant. With the discovery of the damaging effect of CFCs and HCFCs refrigerants to the ozone layer, the HFC family of refrigerant has been widely used as their replacement.

It is now being used as a replacement for R-12 CFC refrigerant in the area of centrifugal, rotary screw, scroll and reciprocating compresssors. It is safe for normal handling as it is non-toxic, nonflammable and non-corrosive.

Currently it is also being widely used in the air conditioning system in newer automotive vehicles. The manufacturing industry use it in plastic foam blowing. Pharmaceuticals industry use it as a propellant.

It exists in gas form when expose to the environment as the boiling temperature is $-14.9^{\circ} \mathrm{F}$ or $-26.1^{\circ} \mathrm{C}$.

This refrigerant is not $100 \%$ compatible with the lubricants and mineral-based refrigerant currently used in $\mathrm{R}-12$. Design changes to the condenser and evaporator need to be done to use this refrigerant. The use of smaller hoses and $30 \%$ increase in control pressure regulations also have to be done to the system.

## Properties of R-134a

| No | Properties | R-134a |
| :--- | :--- | :--- |
| 1 | Boiling Point | $-14.9^{\circ} \mathrm{F}$ or $-26.1^{\circ} \mathrm{C}$ |
| 2 | Auto-Ignition Temperature | $1418^{\circ} \mathrm{F}$ or $770^{\circ} \mathrm{C}$ |
| 3 | Ozone Depletion Level | 0 |
| 4 | Solubility In Water | $0.11 \%$ by weight at $77^{\circ} \mathrm{F}$ or $25^{\circ} \mathrm{C}$ |
| 5 | Critical Temperature | $252^{\circ} \mathrm{F}$ or $122^{\circ} \mathrm{C}$ |
| 6 | Cylinder Color Code | Light Blue |
| 7 | Global Warming Potential (GWP) | 1200 |

## COMPRESSORS

## Features and uses of R-134a

The refrigerant gas R-134a is a HFC replacing R-12 in new installations. As all HFC refrigerants not damage the ozone layer. It has a great chemical and thermal stability, low toxicity and is non-flammable, besides having an excellent compatibility with most materials. Its classification is A1 group L1.

Immiscible with traditional oils of R-12 (mineral and alkyl benzene), whereas its miscibility with oils polyesters (POE) is complete, so it should always be used with these oils.

R-134a is an alternative refrigerant to R-12 for the facility retrofitting or for new installations. It is widely used in automobile air conditioners and household refrigerators. It is also widely used in the industrial and commercial chillers in addition to transport in positive temperatures.

## Toxicity and storage

R-134a is a substance with very low toxicity. The index LCLO inhalation in rats during 4 hours is less than $500,000 \mathrm{ppm}$ and NOEL in relation to heart problems is about $75,000 \mathrm{ppm}$. In exposure for 104 weeks at a concentration of $10,000 \mathrm{ppm}$ was observed no effect. R-134a containers should be stored in a cool and ventilated area away from heat sources. R-134a vapors are heavier than air and tend to accumulate near the ground.

## Security

R-134a is not toxic, not flammable, high security.
It has been classified as A1 / group L1.

## Components

| Chemical Name | \% By weight | CAS N $^{\circ}$ | EC N ${ }^{\circ}$ |
| :---: | :---: | :---: | :---: |
| 1,1,1,2- Tetrafluoroethane (R-134a) | 100 | $811-97-2$ | $212-377-0$ |

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[^6]
## Chart Pressure / Temperature



## Thermodynamic properties

| TEMP. <br> $\left({ }^{\circ} \mathrm{C}\right)$ | ABSOLUTE PRESSURE (bar) |  | DENSITY$\left(\mathrm{Kg} / \mathrm{m}^{3}\right)$ |  | $\begin{aligned} & \text { ENTHALPY } \\ & (\mathrm{kJ} / \mathrm{Kg}) \end{aligned}$ |  | ENTROPY <br> (kJ/Kg.K) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | BUBBLE | DEW | BUBBLE | DEW | BUBBLE | DEW | BUBBLE | BUBBLE |
| -40 | 0.51 | 0.51 | 1413.94 | 2.76 | 149.45 | 375.65 | 0.8008 | 1.7710 |
| -35 | 0.66 | 0.66 | 1399.95 | 3.50 | 155.53 | 378.93 | 0.8266 | 1.7646 |
| -30 | 0.84 | 0.84 | 1385.72 | 4.39 | 161.67 | 382.20 | 0.8521 | 1.7590 |
| -25 | 1.06 | 1.06 | 1371.24 | 5.45 | 167.88 | 385.45 | 0.8773 | 1.7540 |
| -20 | 1.32 | 1.32 | 1356.46 | 6.71 | 174.16 | 388.69 | 0.9023 | 1.7497 |
| -15 | 1.63 | 1.63 | 1341.36 | 8.19 | 180.51 | 391.90 | 0.9270 | 1.7458 |
| -10 | 2.00 | 2.00 | 1325.92 | 9.92 | 186.93 | 395.07 | 0.9515 | 1.7425 |
| -5 | 2.42 | 2.42 | 1310.10 | 11.92 | 193.43 | 398.20 | 0.9759 | 1.7395 |
| 0 | 2.92 | 2.92 | 1293.86 | 14.23 | 200.00 | 401.28 | 1.0000 | 1.7369 |
| 5 | 3.49 | 3.49 | 1277.17 | 16.89 | 206.65 | 404.30 | 1.0240 | 1.7346 |
| 10 | 4.14 | 4.14 | 1259.99 | 19.93 | 213.38 | 407.25 | 1.0478 | 1.7325 |
| 15 | 4.88 | 4.88 | 1242.27 | 23.40 | 220.20 | 410.13 | 1.0714 | 1.7306 |
| 20 | 5.71 | 5.71 | 1223.96 | 27.34 | 227.11 | 412.92 | 1.0950 | 1.7288 |
| 25 | 6.65 | 6.65 | 1205.00 | 31.81 | 234.11 | 415.62 | 1.1184 | 1.7272 |
| 30 | 7.70 | 7.70 | 1185.33 | 36.88 | 241.21 | 418.20 | 1.1417 | 1.7256 |
| 35 | 8.88 | 8.88 | 1164.89 | 42.61 | 248.42 | 420.67 | 1.1650 | 1.7240 |
| 40 | 10.18 | 10.18 | 1143.58 | 49.08 | 255.74 | 423.01 | 1.1882 | 1.7223 |
| 45 | 11.62 | 11.62 | 1121.32 | 56.40 | 263.19 | 425.20 | 1.2114 | 1.7206 |
| 50 | 13.20 | 13.20 | 1197.98 | 64.66 | 270.77 | 427.23 | 1.2346 | 1.7187 |

## Mollier Diagram



- Expansion valve:

R134a refrigerant gas pressure - temperature chart
Refrigerant Temperature / Pressure Chart
Red numbers $=$ inches Hg Black numbers $=$ psig
Temp
Pressure PSI

| $\left.{ }^{\circ} \mathrm{F}\right)$ | R-11 | R-12 | R-22 | R-123 | 2-134A | R-500 | R-502 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -100 | 29.8 | 27.0 | 25.0 | 29.9 | 27.8 | 26.4 | 25.3 |
| -90 | 29.7 | 25.7 | 23.0 | 29.8 | 26.9 | 24.9 | 20.6 |
| -80 | 29.6 | 24.1 | 20.2 | 29.7 | 25.6 | 22.9 | 17.2 |
| -70 | 29.4 | 21.8 | 16.6 | 29.6 | 23.8 | 20.3 | 12.8 |
| -60 | 29.2 | 19.0 | 12.0 | 29.5 | 21.5 | 17.0 | 7.2 |
| -50 | 28.9 | 15.4 | 6.2 | 29.2 | 18.5 | 12.8 | 0.2 |
| $-40$ | 28.4 | 11.0 | 0.5 | 28.9 | 14.7 | 7.6 | 4.1 |
| -30 | 27.8 | 5.4 | 4.9 | 28.5 | 9.8 | 1.2 | 9.2 |
| -20 | 27.0 | 0.6 | 10.2 | 27.8 | 3.8 | 3.2 | 15.3 |
| -10 | 26.0 | 4.4 | 16.4 | 27.0 | 1.8 | 7.8 | 22.6 |
| 0 | 24.7 | 9.2 | 24.0 | 26.0 | 6.3 | 13.3 | 31.1 |
| 10 | 23.1 | 14.6 | 32.8 | 24.7 | 11.6 | 19.7 | 41.0 |
| 20 | 21.1 | 21.0 | 43.0 | 23.0 | 18.0 | 27.2 | 52.4 |
| 30 | 18.6 | 28.4 | 54.9 | 20.8 | 25.6 | 36.0 | 65.6 |
| 40 | 15.6 | 37.0 | 68.5 | 18.2 | 34.5 | 46.0 | 80.5 |
| 50 | 12.0 | 46.7 | 84.0 | 15.0 | 44.9 | 57.5 | 97.4 |
| 60 | 7.8 | 57.7 | 101.3 | 11.2 | 56.9 | 70.6 | 116.4 |
| 70 | 2.8 | 70.2 | 121.4 | 6.6 | 70.7 | 85.3 | 137.6 |
| 80 | 1.5 | 84.2 | 143.6 | 1.1 | 86.4 | 101.9 | 161.2 |
| 90 | 4.9 | 99.8 | 168.4 | 2.6 | 104.2 | 120.4 | 187.4 |
| 100 | 8.8 | 117.2 | 195.9 | 6.3 | 124.3 | 141.1 | 216.2 |
| 110 | 13.1 | 136.4 | 226.4 | 10.5 | 146.3 | 164.0 | 247.9 |
| 120 | 18.3 | 157.7 | 259.9 | 15.4 | 171.9 | 189.2 | 282.7 |
| 130 | 24.0 | 181.0 | 296.8 | 21.0 | 199.4 | 217.0 | 320.8 |
| 140 | 30.4 | 206.6 | 337.2 | 27.3 | 230.5 | 247.4 | 362.6 |
| 150 | 37.7 | 234.4 | 381.5 | 34.5 | 264.4 | 280.7 | 408.4 |


| R134a |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Temperature |  | Pressure |  |  |
| ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | Bar | Inches Hg | psig |
| -40 | -40 | 0.498 | 14.7 |  |
| -31 | -35 | 0.3241 |  |  |
| -30 | -34.44 | 0.3048 | 9.8 |  |
| -20 | -28.89 | 0.1016 | 3.8 |  |
| -10 | -23.33 | 0.1241 |  | 1.8 |
| 0 | -17.78 | 0.4344 |  | 6.3 |
| 10 | -12.22 | 0.7998 |  | 11.6 |
| 20 | -6.67 | 1.2411 |  | 18 |
| 30 | -1.11 | 1.7651 |  | 25.6 |
| 40 | 4.44 | 2.3787 |  | 34.5 |
| 50 | 10 | 3.0957 |  | 44.9 |
| 59 | 15 | 3.8404 |  |  |
| 60 | 15.56 | 3.9231 |  | 56.9 |
| 70 | 21.11 | 4.8746 |  | 70.7 |
| 80 | 26.67 | 5.9571 |  | 86.4 |
| 90 | 32.22 | 7.1843 |  | 104.2 |
| 100 | 37.78 | 8.5702 |  | 124.3 |
| 110 | 43.33 | 10.087 |  | 146.3 |
| 120 | 48.89 | 11.8521 |  | 171.9 |
| 130 | 54.44 | 13.7481 |  | 199.4 |
| 140 | 60 | 15.8924 |  | 230.5 |
| 149 | 65 | 17.996 |  |  |
| 150 | 65.56 | 18.2297 |  | 264.4 |

[^7]


30 https://www.ohio.edu/mechanical/thermo/Intro/Chapt.1_6/refrigerator/refrig_problems.html

## COMPRESSORS



31 https://www.ohio.edu/mechanical/thermo/Intro/Chapt. 1 6/Chapter4c.html

10.2. Prototype 2: Carrier Air conditioner




Filter dryer: 32
So the refrigerant enters through the inlet, it passes across the spring, then surrounds the outside of the solid core. The refrigerant then passes through the solid core and as it does so the dirt, moisture and acids are absorbed, the refrigerant then collects in the groove at the centre of the core and then pass through the screen. It then passes through the perforated plate and exits the unit having been filtered and dried, it then continues to the expansion valve.

[^8]

## R-22

- Nomenclature:

Chlorodifluoromethane

- Symbol: $\mathrm{CHClF}_{2}$
- Boiling point :
$\mathrm{T}=-40.7^{\circ} \mathrm{C}$ (232.5 K) @ 1 bar
$\mathrm{T}=4.9^{\circ} \mathrm{C}$ (278.05 K) @ 4.8 bar
$\mathrm{T}=45.6^{\circ} \mathrm{C}(318.75 \mathrm{~K})$ @ 16.3 bar


[^9]10.3. Fridge 2 : Kelvinator fridge


## COMPRESSORS



| Number | Ozone Friendly | Uses | Chemical Components | Alternatives | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l} \text { R410A } \\ \text { HFC } \end{array}$ | Yes | Designed for new R22 applications, but can also be used to retrofit R13b1 systems. | HFC 125-50\% HFC $32-50 \%$ |  | Long term ozone friendly replacement for R502 / R22 Low GWP |
| $\begin{aligned} & \text { R500 } \\ & \text { CFC } \end{aligned}$ | No; banned under Montreal protocol | Low temperature R12 CFC. | CFC 12 -CFC 115 - | R401b; R407d |  |
| $\begin{aligned} & \text { R502 } \\ & \text { CFC } \end{aligned}$ | No; banned under Montreal protocol | Widely used low temperature refrigerant in the United Kingdom. | HCFC $22-48 \%$ CFC $115-52 \%$ |  |  |
| $\begin{aligned} & \text { R503 } \\ & \text { CFC } \end{aligned}$ | No; banned under Montreal protocol | Low temperature refrigerant -80 to $-100^{\circ} \mathrm{C}$. |  | $\begin{aligned} & \text { R95, R508a, } \\ & \text { R508b } \end{aligned}$ |  |
| CFCs: Chlorofluorocarbons. These products have ceased production within the RSA for internal consumption with effect from 1996. HCFCs: Hydrochlorofluorocarbons. Full availability within the RSA, and the present production phase out date is 2015. There is a widespread belief that this will be reduced to 2005 within the next 2-3 years. <br> HFCs: Hydrofluorocarbons. At the moment there is no production phase out date for HFCs and there is unrestricted use on their applications. <br> HCs \& NH3: This product group mainly used in industrial equipment due to flammability concerns. |  |  |  |  |  |

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## 34 http://www.proairlda.com/gases.htm



[^10]
## R-502 (High stage)

- Nomenclature:

Chlorodifluoromethane,
Chloropentafluoroethane

- Symbol: CHC1F2, CC1F2CF3
- Compress: 375 psi $=25.85$ bar
- Boiling point :
$\mathrm{T}=-45.6^{\circ} \mathrm{C}$ (227.4 K) @ 1 bar $\mathrm{T}=61.5^{\circ} \mathrm{C}(334.7 \mathrm{~K}) @ 25.85 \mathrm{bar}$


## R-503 (Low stage)

- Nomenclature: Azeotropic Blend
- Symbol: CHF3
- Compress: 375 psi $=25.85$ bar
- Boiling point :
$\mathrm{T}=-88.9^{\circ} \mathrm{C}(184.1 \mathrm{~K})$ @ 1 bar $\mathrm{T}=-20^{\circ} \mathrm{C}(253.2 \mathrm{~K}) @ 25.85$ bar


[^11]

[^12]The cascade refrigeration system consists of a low-temperature loop (Low stage) and a high-temperature loop (high stage).
Each stage consists of a compressor, condenser, expansion valve and evaporator The high stage condenser is cooled by air cooled, while the low stage condenser is cooled by the high stage evaporator.
So the high stage evaporator acts as a coolant for the pressurized refrigerant in the low stage.
Advantages of a cascade cooling system:

- Repair is easy
- The Cascade refrigeration allows to low-temperature operation.
- You can reduce the use of power up to $10 \%$ with the help of cascade refrigeration.


## Basic Components


N.B. (process):

1- Pressure Controls
With the exception of a reverse acting control, the pressure controls will be standard, and used in the normal way. A high pressure control will usually be found on all second and third stages, and in some cases on the first stage. This protects the system against excessive pressures during pulldown, or if there is a failure of the first stage system. The control may cycle a few times at the start. A high pressure control with a 100 pound differential (to allow pressures to equalize) is sometimes used rather than a back pressure regulator.

Where continuous operation at the lowest temperature is desired, the high pressure control only is used on the low stage. Where control of the low side or fixture temperature is desired, a thermostat, connected in series with the high pressure control, is used. In special applications and on older units, a liquid line solenoid may be used with a low pressure control on the low stage. (A solenoid for such an application requires a waterproof coil in a well sealed housing.)

The addition of a reverse acting pressure control provides automatic operation even when starting warm. With the interstage condenser at room temperature, a pressure of 700 pounds or more would be required to condense the low temperature refrigerant, therefore the low stage compressor cannot be allowed to start until the high stage has lowered the temperature in the interstage condenser to operating temperatures. This has been accomplished in several ways, such as a thermostat sensing the temperature of the heat exchanger, or pressure controls with reverse acting contacts which open on pressure increase and close on a decrease. This control would be connected to the low side of the high stage.

## 2-Control Of High Pressure Equipment

Up until a few years ago, most cascade equipment used expansion valves and a low temperature refrigerant charge of at least 3 to 5 pounds which necessitated an interstage condenser receiver capable of holding the refrigerant pressure at 500 to 700 psi so that the charge could be contained there. To put the system in operation, the high stage had to be started and the inlet and outlet valves of the interstage condenser receiver opened when it was down to the working temperature. Any power failure or loss of refrigeration due to any failure in the high stage meant the loss of the low temperature refrigerant charge through the relief valve or rupture disc. The system could not be shut down until the low stage was pumped down and the charge locked in the interstage condenser receiver.

Small self-contained systems using less than 2 pounds of the low temperature refrigerants can be made completely automatic, if space is available to provide expansion tanks of sufficient volume to store the refrigerant in the vapor stage at or below 200 pounds pressure. Some of the small chest type units for temperatures down to $-130^{\circ} \mathrm{F}$ using capillary tubes and hermetic compressors can hold the charge in the low side, oil separators, heat exchangers, etc., plus the dome or shell of the unit. As the size of the low side is increased and more refrigerant is required, one or more expansion tanks are required for automatic operation. Good practice limits the maximum pressure to 150 or 200 pounds.

In some cases, the connection to the expansion tank may be a capillary tube. When the unit is shut down, the rise in pressure is slow and most of the charge is stored in the tank. This capillary tube is sized so that the charge in the tank is fed slowly into the system during a pull-down from room temperature. In larger installations where a pull-down imposes a severe load on the motor and compressor, the charge may be admitted to the expansion tanks through a check valve and returned

## COMPRESSORS

through a pressure reducing valve which can be adjusted to the capacity of the unit during such periods.

## 3- Water Cooling Circuitry

The condenser of a high stage does not always receive the incoming water first.
Water is used to remove superheat from the compressed low stage refrigerant before entering the interstage condenser and is also used in some motor cooling jackets. If it were also used on the compressor heads, the flow would be inadequate when the water regulator reduced the flow according to the demand of the high stage. By feeding the condenser last, an adequate flow is maintained at all times.

## 4- Frost Suppressors

While not so common today, these will be found on some units in the form of a heat exchanger between the low temperature suction line and the low temperature hot gas line before it enters the interstage condenser.

## 5- Liquid Line Accumulator

On some small units using capillary tubes in both systems, a small liquid accumulator may be found in the liquid line of the high stage. This is required, as the capillary tube is sized for continuous operation at low temperature, and during a start-up it can not pass the volume of refrigerant condensed by the unit at high temperatures, thus filling the condenser and causing excessively high pressures. The accumulator or reservoir prevents this pressure during the few minutes required to cool the interstage condenser.

## 6- SYSTEM CLEANUP

Cleanup is required any time a system has to be opened, for whatever reason, excluding the addition of refrigerant. Recover the charge according to EPA-approved procedures, and remove the dryer, disconnect the suction line from the compressor, and backflush the entire system with solvent to remove any contaminants or oil from the system. This is most important when replacing a compressor.

## Connecting 2 compressors to get combined pressure and volume.

In order to achieve the desired pressure and volume for our pneumatic equipment, I need to inter-connect 2 compressors.

I need advice on how to go about doing it and need a couple of questions answered:

1) Is it necessary that both compressors share the same specs?
2) Will the resultant pressure and volume be a sum of both compressors?

Both good questions, and both covered extensively on the pages of this site already.

Answer to question \#1 - no.
Answer to \#2 - no. If each compressor puts out 100 PSI, your downstream air line will not see 200 PSI. What you will do is increase the available compressed air flow at the pressure the system needs.

Both compressors will plumb to the same air main to your plant.
Both air compressors will have a one-way or check valve in their lines before the two lines connect to the single main.

In order for one compressor not to be the one that's always on first, undergoing greater wear, periodically change the pressure switch settings so that the alternate compressor comes on first.

## - Expansion valve

## How Thermostatic Expansion Valves Work



Superheat Adjuster cap
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# How Thermostatic Expansion Valves Work 



40 https://theengineeringmindset.com/thermostatic-expansion-valves-work/

# How Thermostatic Expansion Valves Work 



The TXV is used in many refrigeration systems, they can be found in the same location which is just before the evaporator.
The valve decreases the pressure to allow the refrigerant to boil at lower temperatures. The boiling is essential as the refrigerant will absorb the heat from the ambient air and carry this away to the compressor. Just remember that refrigerants have a much lower boiling point than water.

The high pressure liquid refrigerant is forced through a small orifice which causes a pressure reduction as it passes through. During this pressure reduction, some of the refrigerant will vaporise and the rest will remain as liquid.

## - Types of bulbs

There are three different types of bulbs:

- Liquid-charged bulbs
- MOP (Maximum Operating Pressure) bulbs - also called gas-charged bulbs
- Adsorption-filled bulbs

A liquid-charged bulb has a large charge of refrigerant and will never "run dry". It will always contain both liquid and gaseous refrigerant. The pressure inside the bulb increases as the superheating increases, due to additional evaporation. Historically, the refrigerant in the bulb was the same as the working refrigerant in the system
(parallel-charged). However, better characteristics have been achieved by using different refrigerants (cross-charged), which is now the most common arrangement.

An MOP bulb, also called gas-charged, has a much smaller quantity of refrigerant mixture inside the bulb than a liquid-charged bulb. As the evaporation pressure increases, the suction pipe will become increasingly warm as a result. A limited refrigerant charge in an MOP bulb will be totally evaporated at a predefined pressure, the MOP pressure. When the liquid refrigerant mixture has boiled off, the pressure inside the bulb will not increase greatly even if the evaporating pressure does. The needle valve will not open further, thus limiting the maximum mass flow through the valve. The reason for this is to protect the compressor from electrical overload, especially during start-up when the evaporation pressure can be much higher than under normal operating conditions. A disadvantage of the MOP valve is that the bulb always has to be colder than the valve housing to prevent the limited refrigerant charge from migrating and condensing at the membrane surface. If the MOP bulb were instead warmer than the valve housing, the MOP valve would close even if the operating pressure were well below the maximum operating pressure.

TEVs may also have an adsorption charge, where the bulb also contains a solid adsorbent such as charcoal or silica gel. The adsorbed refrigerant reacts more slowly to temperature changes than direct-charged bulbs, and gives a slower response. This can sometimes help to stabilize oscillation tendencies. However, adsorptionfilled bulbs work best over a limited range, which is why they are often specially designed for the operating conditions.


In this project (Liquefaction of air), We need to cool the air from $27^{\circ} \mathrm{C}(300 \mathrm{~K})$ to $-194.35^{\circ} \mathrm{C}(78.8 \mathrm{~K})$, and to achieve this we will use an air compressor ( 10 bar ). The compressor will compress ambient air from $1 \operatorname{bar}\left(27^{\circ} \mathrm{C}, 300 \mathrm{~K}\right)$ to $10 \operatorname{bar}\left(126.85^{\circ} \mathrm{C}, 400 \mathrm{~K}\right)$.

To cool the air from 400 K to 90 K , two heat exchangers will be used, the first will be a heat exchanger to cool the compressed air from ( $126.85{ }^{\circ} \mathrm{C}, 400 \mathrm{~K}$ ) up to $\left(-73.15{ }^{\circ} \mathrm{C}, 200 \mathrm{~K}\right)$ due to the cascade refrigeration cycle (R-502 and R-503 (Kelvinator fridge)) and a second heat exchanger to cool the compressed air from 200 K to 90 K , this exchanger will work with the temperature of the nonliquefied cold air (about $-195^{\circ} \mathrm{C}, 78.8 \mathrm{~K}$ ).

After the cooling process, the compressed air will pass into the expansion valve, where the air will be subjected to a sudden pressure drop, causing a similar temperature drop, from $10 \mathrm{bar}\left(-183.15^{\circ} \mathrm{C}\right.$, $90 \mathrm{~K})$ to 1 bar ( $-194.24^{\circ} \mathrm{C}, 78.91 \mathrm{~K}$ ). ).

After expanding, the liquefied air (air liquid) will be separated from the non-liquefied air (air in gas state). Where the liquid will be stored in special containers, while the non-liquefied cold air will be used to cool the compressed air as mentioned earlier (in the second heat exchanger).

Therefore, to obtain liquefied air with a 10 bar compressor, the air must be cooled to $90 \mathrm{~K}\left(-183^{\circ} \mathrm{C}\right)$.

| \# of cycle | Point 3 | Point 4 (10 bar, 1 MPa) |  | Point 5 (1 bar, 0.1 MPa) | Point g | Point 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | T (K) | T (K) | H (kJ/Kg) | T (K) | T (K) | T (K) |
| 1 | 200 | 200 | 195.2 | 195.54 | 300 | 300 |
| 2 | 200 | 249.06 | 246.092 | 246.11 | 246.11 | 249.49 |
| 3 | 200 | 222.17 | 218.32 | 218.5 | 218.5 | 223.97 |
| 4 | 200 | 208.79 | 204.39 | 204.66 | 204.66 | 209.45 |
| 5 | 200 | 202.2 | 197.5 | 197.82 | 197.82 | 202.4 |
| 6 | 200 | 198.98 | 194.13 | 194.47 | 194.47 | 198.88 |
| 7 | 200 | 197.41 | 192.48 | 192.46 | 192.46 | 197.14 |
| 8 | 200 | 196.47 | 191.49 | 191.48 | 191.48 | 196.1 |
| 9 | 200 | 196.01 | 191 | 190.99 | 190.99 | 195.59 |
| 10 | 200 | 195.78 | 190.76 | 190.75 | 190.75 | 195.33 |
| 11 | 200 | 195.67 | 190.64 | 190.64 | 190.64 | 195.21 |
| 12 | 200 | 195.62 | 190.59 | 190.58 | 190.58 | 195.15 |
| 13 | 200 | 195.59 | 190.56 | 190.55 | 190.55 | 195.12 |
| 14 | 200 | 195.58 | 190.55 | 190.54 | 190.54 | 195.11 |
| 15 | 200 | 195.57 | 190.54 | 190.53 | 190.53 | 195.1 |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\sim 1000$ | 200 | 90 | -103.73 | 78.91 | 80 | 131.86 |

We notice that the temperatures in the first five stages were changing significantly as the heat exchanger was cooling down, then with the beginning of the sixth stage, the heat exchanger began to play its primary role, which is cooling the air entering the exchanger before passing through the expansion valve, but after several stages we notice that the heat difference between The stages due to the decrease in the temperature difference before and after the expansion valve (+ -5 degrees), which slows down the process of cooling the air and prevents it from reaching temperatures as low as 90 kelvin except after
many many stages. Here the problem appears in practice, as in the event of any thermal leakage from the thermal insulating materials, this leakage will further delay the process of liquefying the air, and we may be vulnerable to not reaching the liquefaction temperature.


[^0]:    2. Connecting 2 compressors to get combined pressure and volume133
[^1]:    5 https://checalc.com/solved/LMTD Chart.html \& https://checalc.com/calc/ShortExch.html

[^2]:    Point 4
    $\dot{\mathrm{m}}=2.75 \mathrm{Kg} / \mathrm{sec}$
    $\mathrm{P}=50$ bar
    $\mathrm{T}=155 \mathrm{~K}, 160 \mathrm{~K}, 165 \mathrm{~K}, 170 \mathrm{~K}$

[^3]:    6 https://www.gasparini.com/en/blog/metals-and-materials-for-low-temperatures/

[^4]:    ${ }^{a} 1, \mathrm{Al}$ foil with glass fiber mat separator; $2, \mathrm{Al}$ foil with nylon net spacer; $3, \mathrm{Al}$ foil with glass fabric spacer; $4, \mathrm{Al}$ foil with glass fiber, unbonded spacer; 5 , aluminized Mylar, no spacer.

[^5]:    1. The above parameters are for reference only, and is subject to our technical quotation
    2. More displacement, higher filling pressure, such $20 \mathrm{Mpa}, 23 \mathrm{Mpa}, 30 \mathrm{Mpa}$, please feel free consult us
[^6]:    28 https://gas-servei.com/shop/docs/technical-data-sheet-r-134a-gas-servei.pdf

[^7]:    29 https://www.pinterest.com/pin/333829391133607747/

[^8]:    $32 \mathrm{https}: / /$ theengineeringmindset.com/filter-driers-how-do-they-work/

[^9]:    33 https://refrigerants.com/product/r22/

[^10]:    35 https://www.eevblog.com/forum/chat/refrigerator-with-two-compressors-how-do-they-do-it/

[^11]:    $36 \mathrm{https}: / /$ secureservercdn.net/198.71.233.179/m9v.7b6.myftpupload.com/wp-content/uploads/2019/12/SDS-R22.pdf?time=1618519493 37 https://www.cc.kyushu-u.ac.jp/scp/system/library/PROPATH/manuals/p-propath/r503.pdf

    38 https://www.arma.org.au/wp-content/uploads/2017/02/SDS-R503.pdf

[^12]:    39 https://www.quora.com/What-is-a-cascade-refrigeration-system

