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## A Simple Computational Form for Maxwellian **Reactivities**

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# A SIMPLE COMPUTATIONAL FORM FOR MAXWELLIAN REACTIVITIES

PLASMA ENGINEERING

## TECHNICAL NOTE

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A simple form is given for the evaluation of Maxwellian reactivities for the reactions  $T(d,n)^4$ He, D(d,p)T,  $D(d,n)^3$ He, and  $^3$ He(d,p)<sup>4</sup>He, with applications to the analytical treatment of fusion reactor problems.

There are a variety of forms to evaluate Maxwellian fusion reactivities<sup>1-7</sup> as a function of ion temperature T (keV). In addition to the more convenient computational forms,<sup>1-5</sup> there are also analytical forms obtained from first principles<sup>6,7</sup> that are computationally inconvenient.

Brunelli<sup>5</sup> recently published a simple form for the Maxwellian reactivity of a deuterium-tritium (D-T) plasma:

$$\langle \sigma v \rangle_{\text{D-T}}(\text{cm}^3/\text{s}) = 9 \times 10^{-16} \exp[-0.476|\ln(T/69)|^{2.25}]$$
, (1)

which is accurate to 2% for  $10 \le T \le 100$  keV and to 10% for  $2 \le T \le 150$  keV. Equation (1) can be generalized to the form:

$$\langle \sigma v \rangle = \exp[A_1 + A_2 |\ln(T/A_3)|^{A_4}]$$
 (2)

Equation (2) has been fitted to reactivity data by Miley et al.<sup>8</sup> using the ISML routine ZXSSQ (Ref. 9). The routine ZXSSQ determines the set  $\{A_1, \ldots, A_4\}$  by minimizing the sum of squares of the differences between the given data and Eq. (2). The results are shown in Table I, together with the curve-fitting errors:

$$\delta = 100(1 - \langle \sigma v \rangle_{calc} / \langle \sigma v \rangle_{real}) \quad , \tag{3}$$

where  $\langle \sigma v \rangle_{calc}$  is obtained from Eq. (2) and  $\langle \sigma v \rangle_{real}$  is taken from Ref. 8. A comparison of the present results to previous computational forms<sup>1-5</sup> is shown in Table II. Although the results of Ref. 4 are most accurate, Brunelli<sup>5</sup> illustrates several advantages in using Eq. (2), which are restated in generalized form here. In particular, the logarithmic derivative of  $\langle \sigma v \rangle$  is

TABLE I

Best-Fit Parameters for Eq. (2) in Cubic Centimetres per Second, with Corresponding Curve-Fitting Errors,  $\delta$ 

	$T(d,n)\alpha$ $D(d,p)T$ $D(d,n)^{3}He$		$^{3}$ He(d, p) $\alpha$	
$ \begin{array}{c} A_1 \\ A_2 \\ A_3 \\ A_4 \\  \delta_{max}  \end{array} $	-34.629731 -0.57164663 64.221524 2.1373239 3.7	-37.061587 -3.4503954 × 10 <sup>-5</sup> 3.0774327 × 10 <sup>5</sup> 5.0816753 4.6	$\begin{array}{r} -36.799066 \\ -1.0041572 \times 10^{-5} \\ 7.4173511 \times 10^{5} \\ 5.4366402 \\ 4.0 \end{array}$	-35.235392 -0.15172469 802.58671 2.6497885 9.3
$\delta(T = 1)$	2.3	(-10.8)	(-10.8)	(-21.8)
$\delta(T = 1.5)$	2.8	-1.9	-2.3	1.9
$\delta(T = 5)$	-2.3	2.7	2.7	2.5
$\delta(T = 10)$	2.6	-0.5	0.1	-7.1
$\delta(T = 20)$	2.8	-3.8	-2.8	-4.7
$\delta(T = 40)$	-1.3	-4.3	-3.9	4.7
$\delta(T = 60)$	-1.6	-2.4	-2.9	4.3
$\delta(T = 80)$	-0.4	0.4	-1.1	-0.5
$\delta(T = 100)$	2.7	3.6	1.0	-6.9
Range of T (keV)	1 to 100	1.5 to 100	1.5 to 100	1.5 to 100

Reference	$T(d,n)^4$ He	D(d, p)T	$D(d,n)^{3}$ He	$^{3}$ He $(d, p)^{4}$ He
Gamow (Ref. 1)	57	12	10	$     \begin{array}{r}       25 \\       15 \\       2 \\       0.4 \\       \\       9     \end{array} $
Gamow + first-order corrections (Ref. 2)	27	6	4	
Kozlov (Ref. 3)	8	1	0.6	
Hively (Ref. 4)	1 <sup>a</sup>	0.052	0.02	
Brunelli (Ref. 5)	10			
Present work	4	5	4	

TABLE II

Accuracy Comparisons,  $\delta_{max}$ , for Various Simple Forms for  $1.5 \le T \le 80 \text{ keV}^*$ 

\*See Ref. 4 for details.

<sup>a</sup>There is a typographical error in Table I of Ref. 4: The coefficient  $a_5$  of  $s_5^*$  for the reaction  $T(d, n)^4$ He should be negative; the magnitude is correct.

$$\mu(T) \equiv \frac{d \ln\langle \sigma v \rangle}{d \ln T} = A_2 A_4 |\ln(T/A_3)|^{\alpha} \quad , \tag{4}$$

where  $\alpha = A_4 - 1$ . In addition, the maximum value  $y_m$  of the function  $y = \langle \sigma v \rangle / T^m$  (which arises frequently in reactor power balances) occurs at temperature  $T_m$  by solving  $\mu(T) = m$ . The value of  $T_m$  can be found explicitly as

$$T_m = A_3 \exp[\pm (m/A_2A_4)^{1/\alpha}]$$
,  $\pm \text{ for } m \le 0$ . (5)

Thirdly, a truncated expansion of  $\ln y$ , near  $T_m$ , can be obtained in powers of  $\ln(T/T_m)$ :

$$\ln(y/y_m) = \frac{1}{2} \left( \frac{d\mu}{d \ln T} \right)_{T_m} \ln^2(T/T_m)$$
$$= A_2 A_4 (A_4 - 1) (m/A_2 A_4)^{\beta} \ln^2(T/T_m) , \qquad (6)$$

where  $\beta = (A_4 - 2)/(A_4 - 1)$ . Following Brunelli, Eq. (6) can be rewritten as

 $\langle \sigma v \rangle = y_m T^m$ ,

which is a local approximation to Eq. (2) with a relative error given by the right side of Eq. (6). The remainder of Brunelli's results can be trivially generalized and will not be repeated here. It is concluded that Eq. (2) provides a good computational form for Maxwellian reactivities, with applications to the analytical treatment of fusion reactor problems.

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