



AECENAR

Association for Economical and Technological Cooperation
in the Euro-Asian and North-African Region

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Air Liquefaction and Cryogenics - Report 1 (2021), Part II: LOX Prototype System Concept & Mechanical Design

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System Design of LOX Production Prototype

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1 System Design of LOX Production Prototype

1.1 Air Compressor

#1 (with oil)



Makute Portable Air Compressor Oil Air Pump 50L

[Get Latest Price >](#)

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Purchase Qty. / Reference FOB Price

100-499 Pieces **US \$95.44**

500+ Pieces **US \$93.5**

Port: Ningbo, China

Production Capacity: 10000PCS/Month

Payment Terms: L/C, T/T, D/P, Western Union, Paypal, Money Gram

Lubrication Style: Lubricated

Cooling System: Air Cooling

Cylinder Arrangement: Balanced Opposed Arrangement

Cylinder Position: Angular

Model:	XZ-0.036/8
Rated Volatge:	220-240/110V
Rated Frequency:	50/60Hz
Air Tank	30-50L
No Load Speed:	2850 r/min
Pressure	8Bar

#2 (oil free)



(CE/GS) 8bar Air Compressor (5050BM)

[Get Latest Price >](#)

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Purchase Qty. / Reference FOB Price

500-999 Pieces **US \$62.28**

1,000+ Pieces **US \$62.43**

Port: Ningbo, China

Production Capacity: 40000PCS/Month

Payment Terms: L/C, T/T, Western Union, Money Gram

Lubrication Style: Oil-free

Cooling System: Air Cooling

Cylinder Arrangement: Balanced Opposed Arrangement

Cylinder Position: Vertical

Structure Type: Semi-Closed Type

Model:	5050BM
Rated Voltage:	220-240/110V
Rated Frequency:	50/60HZ
Rated Input power:	5.0HP
No Load Speed:	2850R/MIN
Air Tank:	50L
Pressure:	8BAR

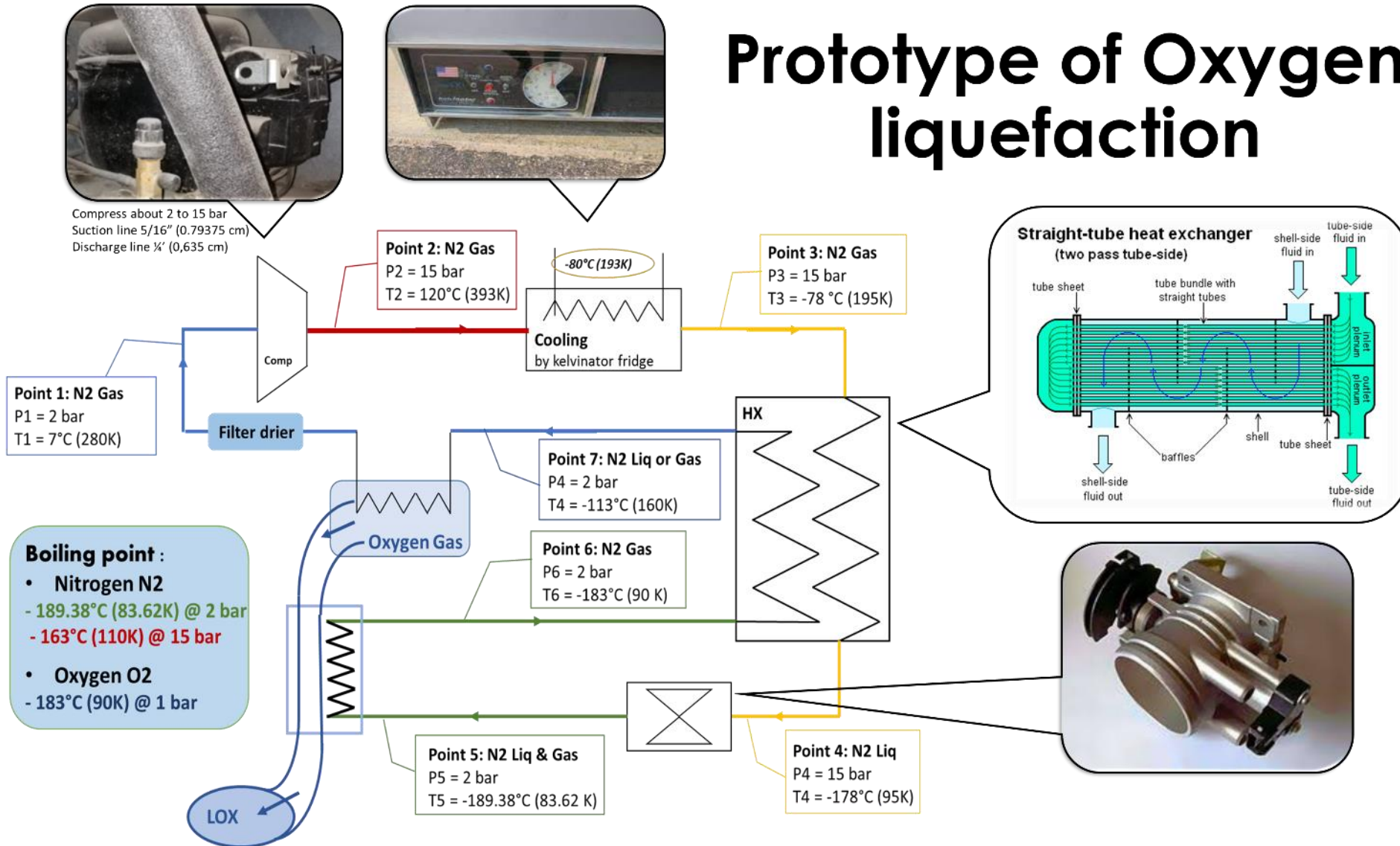


Air Compressor (Antar store)

- 10 bar , 50L price 165 dollars (makute company)
- 10 bar, 150L price 395 dollars
- 10 bar, 200 L price 450 dollars

1.2 Prototype cycle of Oxygen liquefaction

Prototype of Oxygen liquefaction



In this prototype the oxygen will be liquefied by cascade cooling of nitrogen.

The nitrogen gas will be compressed (from 2 bar to about 15 bar)[use for that the laboratory refrigerator], The nitrogen will then be cooled down to 195 K by means of a Kelvinator fridge operated with a cascade of R-502 and R-503 refrigerants.

Then the nitrogen will be cooled to lower temperatures (83.6 K) using the expansion valve and heat exchanger.

This nitrogen temperature (<90 K) would be sufficient to liquefy the oxygen at 1atm.

Oxygen gas can also be prepared and cooled to about 170 K in nitrogen before returning directly to the compressor (160 K).

1.3 Prototype Heat exchanger (HX - N₂/N₂)

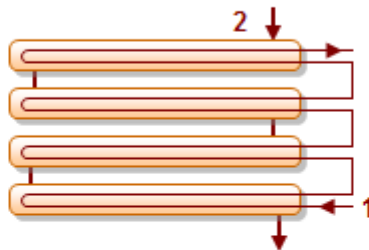
LMTD Correction Factor Charts

Calculates Logarithmic Mean Temperature Difference (LMTD) Correction factor for different configuration of exchangers.

1.3.1 Data:

Exchanger Type

4 Shell 8 Tube Tema E



Stream 1

Temperature In (T1)

195

Temperature Out (T2)

95

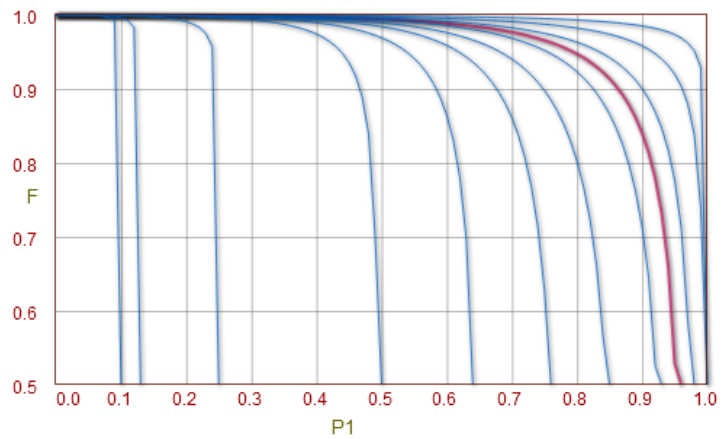
Stream 2

Temperature In (t1)

Temperature Out (t2)

1.3.2 Result:

$R1 = \frac{(t1 - t2)}{(T2 - T1)}$ $= 0.7000$
$P1 = \frac{(T2 - T1)}{(t1 - T1)}$ $= 0.9524$
$LMTD = 15.4170$
$F = 0.4706$ $LMTD_{Corrected} = 7.2549$



Shortcut Heat Exchanger Sizing

Estimates LMTD (Log Mean Temperature Difference), Exchanger surface area, number of tubes, shell diameter and number of shell in series.

1.3.3 Data:

Heat Duty

U Value

Hot Side

Temperature In

Temperature Out

System Design of LOX Production Prototype

Cold Side

Temperature In

 °K

Temperature Out

 °K

Geometry

Tube Pass

Tube Length

 m

Tube Outside Diameter (OD)

 mm

Tube Pattern

1.3.4 Result:

Tube Pitch	21.3500	mm
LMTD	23.39	°K
Correction Factor (F)	0.8381	
LMTD (Corrected)	19.61	°K
Shell in Series	3	
Total Area	0.04	m ²
Area per Shell	0.01	m ²
Tubes per Shell	0	
Shell ID (Estimate)	88.31	mm

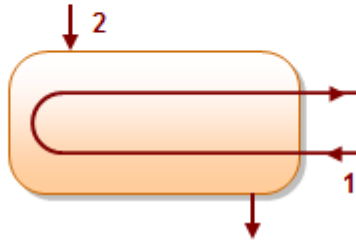
1.4 Prototype Heat exchanger (HX - N₂/O₂)

LMTD Correction Factor Charts

Calculates Logarithmic Mean Temperature Difference (LMTD) Correction factor for different configuration of exchangers.

1.4.1 Data:

Exchanger Type



Stream 1

Temperature In (T1)

Temperature Out (T2)

Stream 2

Temperature In (t1)

Temperature Out (t2)

System Design of LOX Production Prototype

1.4.2 Result:

$$R1 = (t1 - t2) / (T2 - T1)$$

$$= 0.0769$$

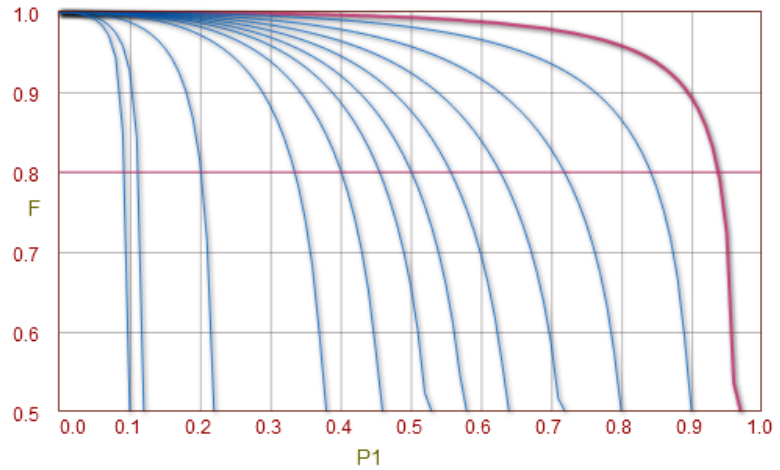
$$P1 = (T2 - T1) / (t1 - T1)$$

$$= 0.9381$$

$$LMTD = 31.0186$$

$$F = 0.7999$$

$$LMTD_{Corrected} = 24.8123$$



Model Number: 00402-01 (17 Series Sanitary HX, 4 Inch Tube Bundle)			
Tube Side (product)	Oxygen	Shell Side (working)	Nitrogen
Flow Rate	0.4 kg/hr	Flow Rate	25 kg/hr
Inlet Temperature	140 K	Inlet Temperature	83 K
Inlet Pressure	100 kPa	Inlet Pressure	200 kPa

Metric Units		
Heat Exchanger Model	00402-01	
	Tube Side	Shell Side
Fluid	Oxygen	Nitrogen
Temperature In	-133.15	-190.15 C
Temperature Out	-184.29	-189.43 C
Mass Flow	0.11	6.95 g/sec
Volumetric Flow	N/A	N/A lpm
Pressure Drop	0.01	11.04 kPa
Heat Transfer	5	Watts
Effectiveness	0.897	

¹ <http://calc.exergyllc.com/>

Shortcut Heat Exchanger Sizing

Estimates LMTD (Log Mean Temperature Difference), Exchanger surface area, number of tubes, shell diameter and number of shell in series.

1.4.3 Data:

Heat Duty

5	W
---	---

U Value

150	W/m ² .°K
-----	----------------------

Hot Side

Temperature In

140.00	°K
--------	----

Temperature Out

89.00	°K
-------	----

Cold Side

Temperature In

83.00	°K
-------	----

Temperature Out

90.00	°K
-------	----

System Design of LOX Production Prototype

Geometry

Tube Pass

Tube Length

Tube Outside Diameter (OD)

Tube Pattern

1.4.4 Result:

Tube Pitch	21.3500	mm
LMTD	20.75	°K
Correction Factor (F)	0.9623	
LMTD (Corrected)	19.97	°K
Shell in Series	2	
Total Area	0.00	m ²
Area per Shell	0.00	m ²
Tubes per Shell	0	
Shell ID (Estimate)	79.41	mm

2

² <https://checalc.com/calc/ShortExch.html>

2 Components of Oxygen liquefaction prototype

2.1 Overview

- Compressor: It is LR25B Laboratory refrigerator compressor
- Cooling of N₂: using kelvinator refrigerator
- Heat exchanger (HX-N₂ / N₂): should be manufactured
- Heat exchanger (HX-N₂ / O₂): should be manufactured
- Cooling of O₂: should be manufactured
- Expansion valve: Purchase
- Filter drier: Purchase
- Cryometer (measures up to 80 K): Purchase
- Connections: The available LR25B Laboratory refrigerator and air-conditioner parts can be used if they are suitable for work.
- Gaseous oxygen preservation tank: manufacture / purchase
- Liquid oxygen storage tank: manufacture / purchase
- Gaseous oxygen (volume?)
- Nitrogen (volume?)
- Thermal isolations

2.2 Cryometer



2.2.1 Features

Digitized the conventional type (MBM) to a more compact design.

- In combination with the MBS CRYO-METER, the accurate temperature can be observed at remote position.
- MBD CRYO-METER can be used as a power source unit of the MBS CRYO-METER.

Components of Oxygen liquefaction prototype

2.2.2 Specification

Display	Digital
Temperature range	10K~350K (-263°C~+77°C)
Accuracy	±2% (Full scale) (However,10~30K are ±1K)
Voltage	AC100V±10%
Cryo thermocouple thermometer power supply	DC24V (Internal)
Cable Length	Input power cable 3m Analog signal input cable 5m Power supply cable (MBS) 5m For power supply
Weight	520 g

3 Heat exchangers for prototype project

The central variables in any heat exchanger analysis are the heat transfer rate q [W], heat transfer area A [m²], heat capacity rates C ($=m\dot{c}_p$) [W/K], and the overall heat transfer coefficient U . On the basis of these variables and the fluid temperatures, we can write two basic equations for the heat transfer rate; first, for heat transfer rate it must hold that

$$q = U A \Delta T_m$$

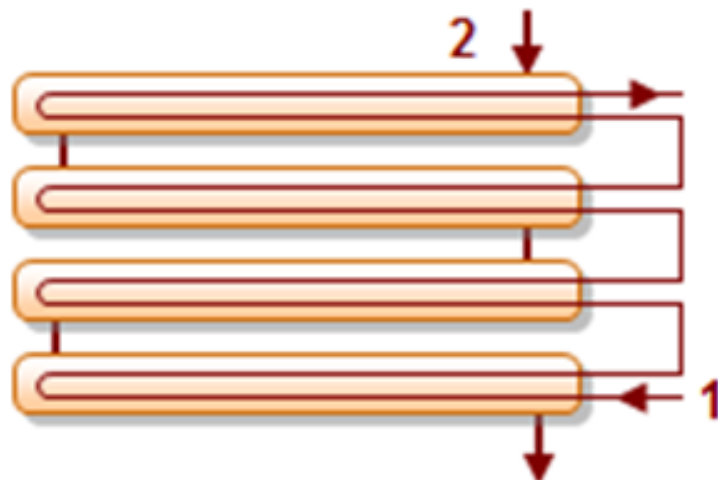
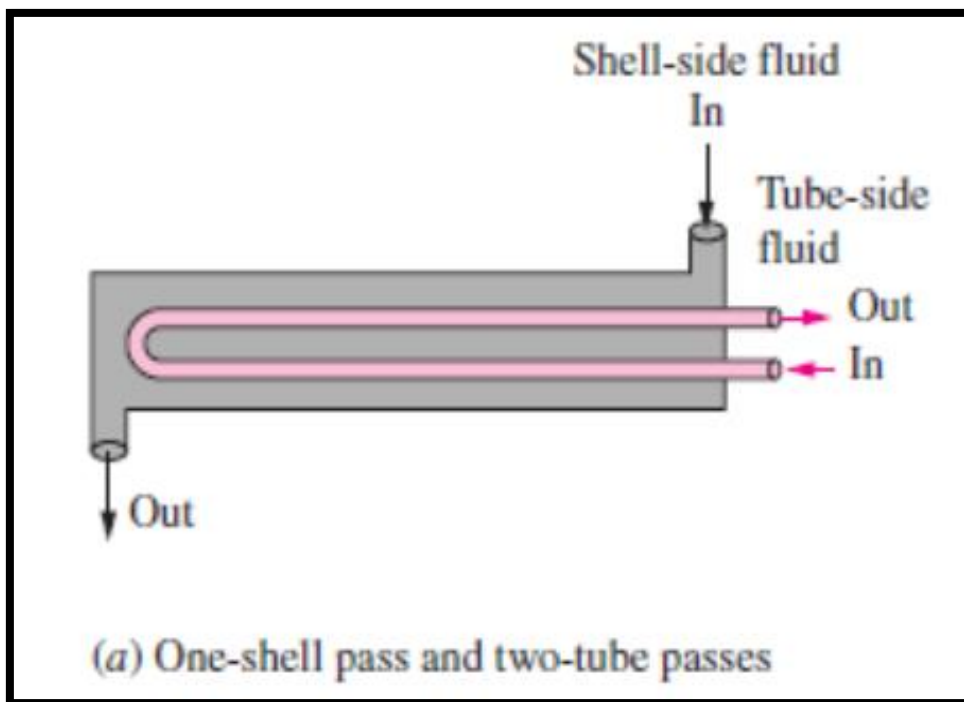
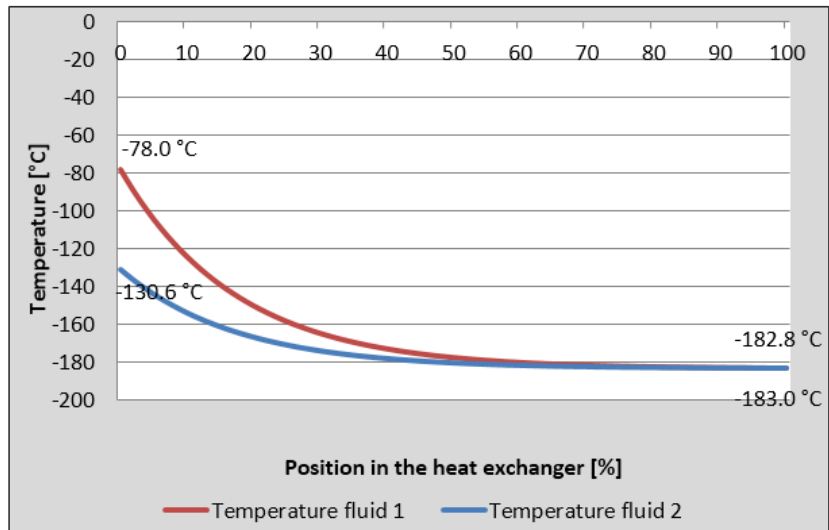
where ΔT_m is the average (mean) temperature difference of the two fluids in the heat exchanger, and the area A in equation the heat transfer area, meaning the contact area between one of the fluids, and the surface of the wall that separates the fluid.

Second, on the basis of 1st law of thermodynamics, the heat transfer rate q must also equal the rate of heat lost by the hot fluid stream and gained by the cold fluid stream:

$$q = \dot{C}_{hot} (T_{hot,in} - T_{hot,out}) = \dot{C}_{cold} (T_{cold,out} - T_{cold,in})$$

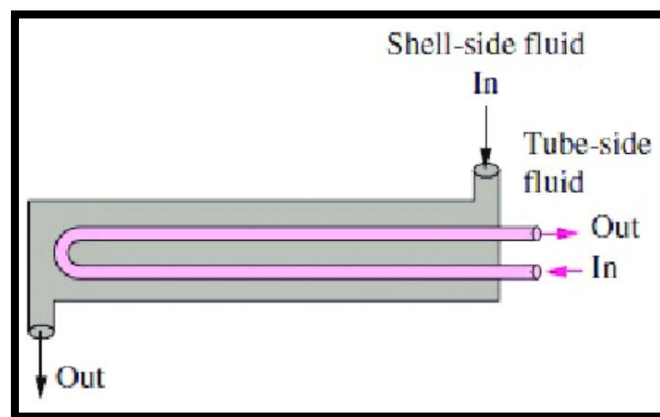
3.1 HX- N₂/N₂

Input		
Name of HX	HX-N2/N2	
Type of heat exchanger	Shell & tubes	
	Unit	
Heat duty	W	868
Heat transfer coefficient	W/m ² .°K	500
Area	m ¹	1.2
Fluid 1 _ hot side		
Mass flow 1	Kg/h	25
	Kg/s	0.00694
Inlet temperature 1	K	195
Heat capacity 1	KJ/Kg.K	1.251
Fluid 2 _ Cold side		
Mass flow 2	Kg/h	58.24
	Kg/s	0.01618
Inlet temperature 2	K	89
Heat capacity 2	KJ/Kg.K	1.074
Geometry		
Tube pass		Single
Tube length	m	0.4
Tube Outside Diameter (OD)	mm	9.525
Tube Pattern		square
Output		
Outlet temperature 1	K	90
	°C	-183
Outlet temperature 2	K	142.5
	°C	-130.5
Result		
Tube pitch	mm	15.875
Shell in Series		6
Total Area	cm ²	1637.95
No. of Tubes		2
Shell ID (Estimate)	mm	103.25



3.2 HX-N2/O2 main

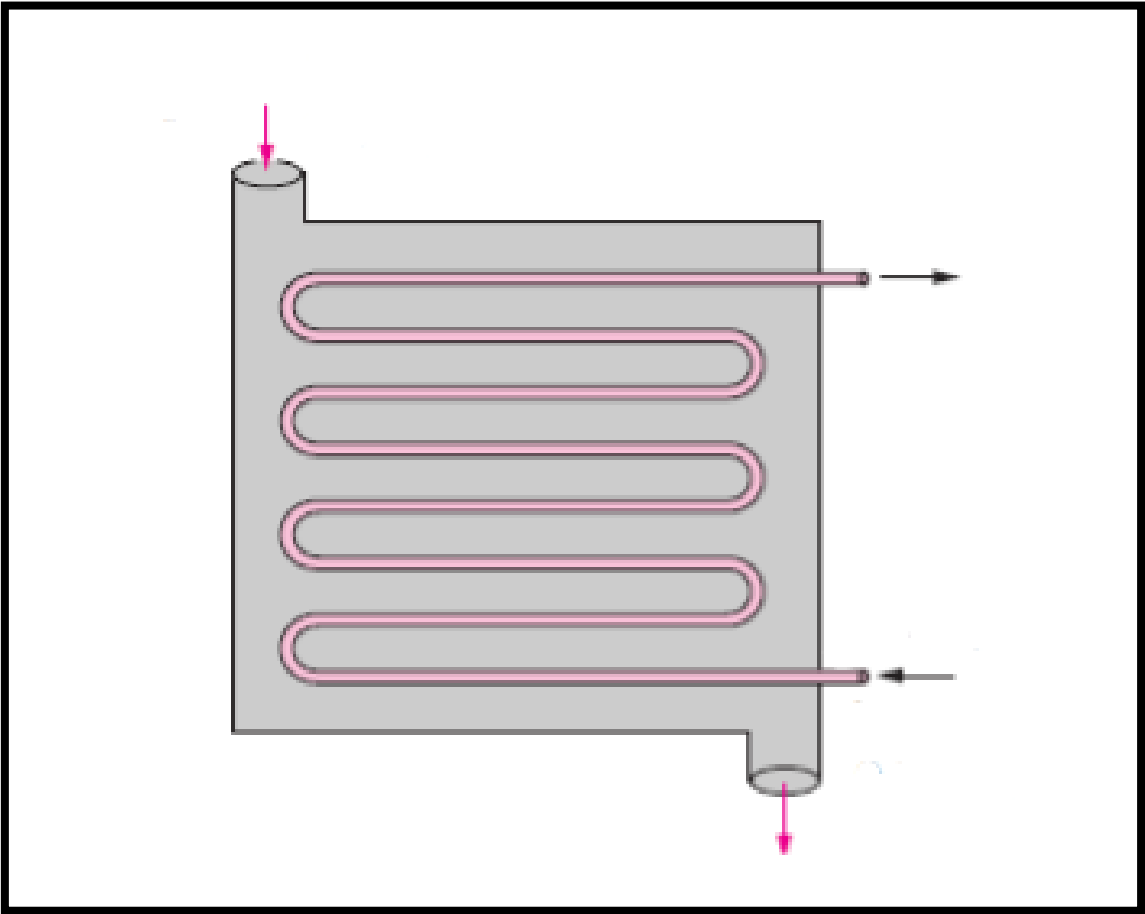
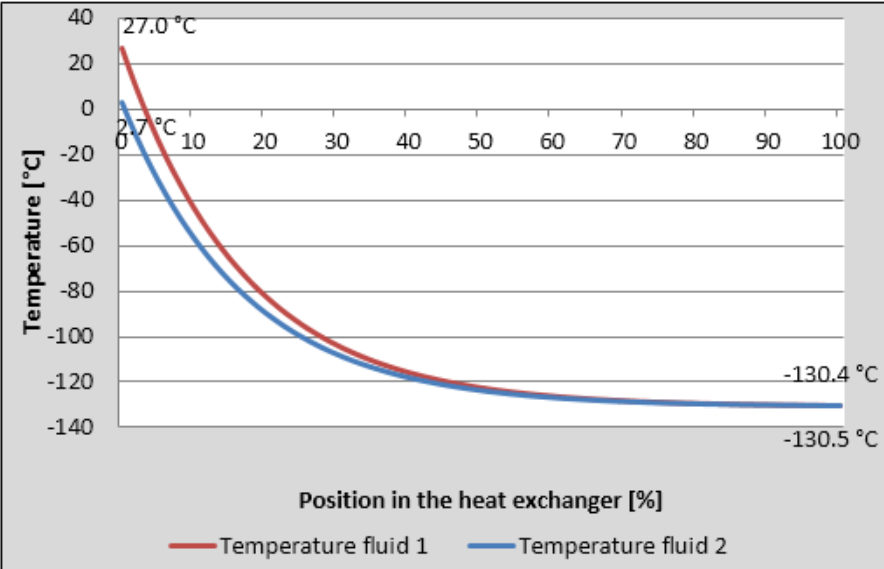
Input		
Name of HX	HX-N2/O2 Main	
Type of heat exchanger	shell & tubes	
	Unit	
Heat duty	W	92.42
Heat transfer coefficient	W/m ² .°K	500
Area	m ²	0.018
Fluid 1 _ hot side _ O2		
Mass flow 1	Kg/h	4.739
	Kg/s	0.001316
Inlet temperature 1	K	142.5
Heat capacity 1	KJ/Kg.K	0.9298
Fluid 2 _ Cold side _ N2		
Mass flow 2	Kg/h	25
	Kg/s	0.00694
Inlet temperature 2	K	83
Heat capacity 2	KJ/Kg.K	1.284
Geometry		
Tube pass		Single
Tube length	m	0.2
Tube Outside Diameter (OD)	mm	9.525
Tube Pattern		Square
Output		
Outlet temperature 1	K	88
	°C	-190.5
Outlet temperature 2	K	90
	°C	-183
Result		
Tube pitch	mm	15.875
Shell in Series		1
Total Area	cm ²	91.5
No. of Tubes		2
Shell ID (Estimate)	mm	98.35



3.2. HX-N2/O2 (2nd)

Input		
Name of HX	HX-N2/O2 (2nd)	
Type of heat exchanger	Shell & tubes	
	Unit	
Heat duty	W	2300
Heat transfer coefficient	W/m ² .°K	500
Area	m ²	1
Fluid 1 _ hot side _ O2		
Mass flow 1	Kg/h	56.52
	Kg/s	0.0157
Inlet temperature 1	K	300
Heat capacity 1	KJ/Kg.K	0.9142
Fluid 2 _ Cold side _ N2		
Mass flow 2	Kg/h	58.23
	Kg/s	0.0157
Inlet temperature 2	K	142.5
Heat capacity 2	KJ/Kg.K	1.047
Geometry		
Tube pass		Single
Tube length	m	0.2
Tube Outside Diameter (OD)	mm	9.525
Tube Pattern		Square
Output		
Outlet temperature 1	K	142.5
	°C	-130.5
Outlet temperature 2	K	275.7
	°C	2.7
Result		
Tube pitch	mm	15.875
Shell in Series		1
Total Area	cm ²	2456.98
No. of Tubes		8
Shell ID (Estimate)	mm	127.53

Heat exchangers for prototype project



3.3 HX- final calculation

For HX-N2/N2											
Stream data				Results			Units	Final results			Units
	Units	Hot	Cold	Heat capacity ratio	Cr			LMDT	LMDT		
Flow rate	Kg/hr	25	58.24	Number of transfer units	NTU	7.3548		Surface Area	S	0.65133467	m ²
Inlet temp.	K	195	89	Effectiveness	ξ	0.9434		Diameter of pipe	D	0.009525	m
Specific heat	KJ/Kg.K	1.1163	1.1995	Heat transfer	Q	775.17	W	Length	L	21.76653698	m
Outlet temp.	K	95	128.947	Overall U	U	47.51	W/m ² .K	Length per shell	L /shell	3.627756163	m
				Heat exchanger area	A	1.2	m ²	Tube length	Tl	1.793928082	m

For HX-N2/O2 [2nd]											
Stream data				Results			Units	Final results			Units
	Units	Hot	Cold	Heat capacity ratio	Cr			LMDT	LMDT		
Flow rate	Kg/hr	56.52	58.23	Number of transfer units	NTU	3.5192		Surface Area	S	0.507249982	m ²
Inlet temp.	K	300	129	Effectiveness	ξ	0.6316		Diameter of pipe	D	0.02222	m
Specific heat	KJ/Kg.K	0.9199	1.0677	Heat transfer	Q	1559.78	W	Length	L	7.266547442	m
Outlet temp.	K	192	219.317	Overall U	U	50.826	W/m ² .K	Tube length	Tl	0.85599343	m
				Heat exchanger area	A	1	m ²				

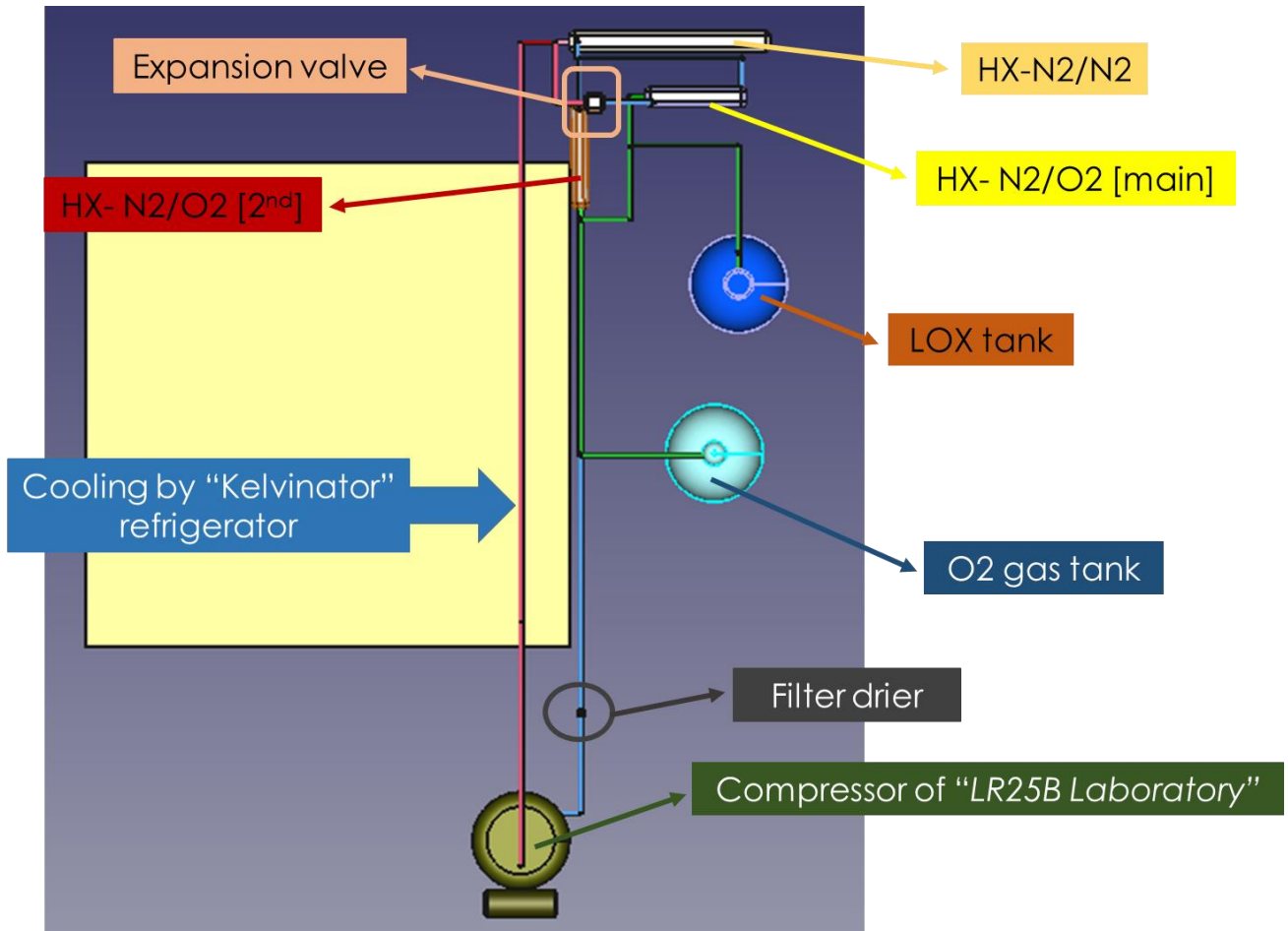
For HX-N2/O2 [Main]											
Stream data				Results			Units	Final results			Units
	Units	Hot	Cold	Heat capacity ratio	Cr			LMDT	LMDT		
Flow rate	Kg/hr	4.739	25	Number of transfer units	NTU	3.4197		Surface Area	S	0.027718617	m ²
Inlet temp.	K	192	83	Effectiveness	ξ	0.9541		Diameter of pipe	D	0.0025	m
Specific heat	KJ/Kg.K	0.915	2.08	Heat transfer	Q	52.8655	W	Length	L	3.529243881	m
Outlet temp.	K	88	91.672	Overall U	U	60	W/m ² .K	Tube length	Tl	1.750191941	m
				Heat exchanger area	A	0.01356	m ²				

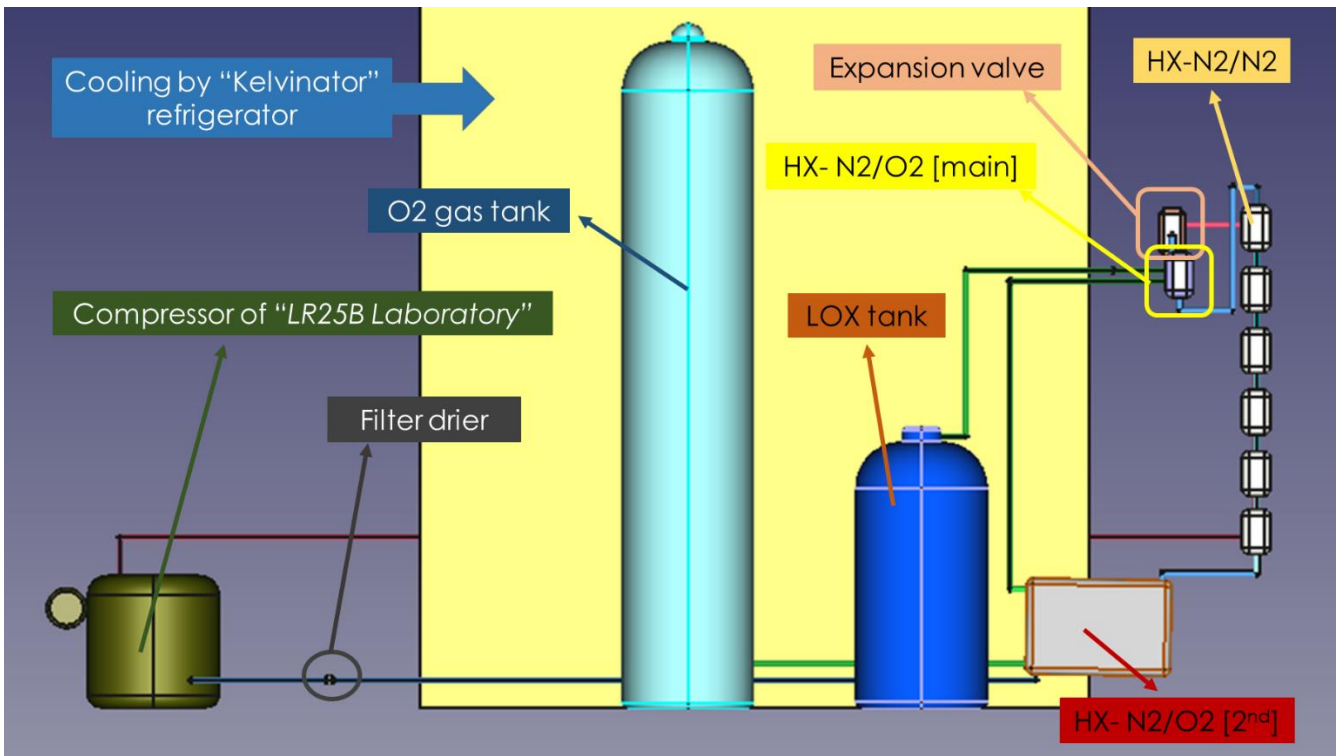
4 FreeCad Design

4.1 Prototype design on FreeCad



prototype cycle of oxygen liquefaction.FCStd





4.2 Heat exchanger design HX-N₂/N₂

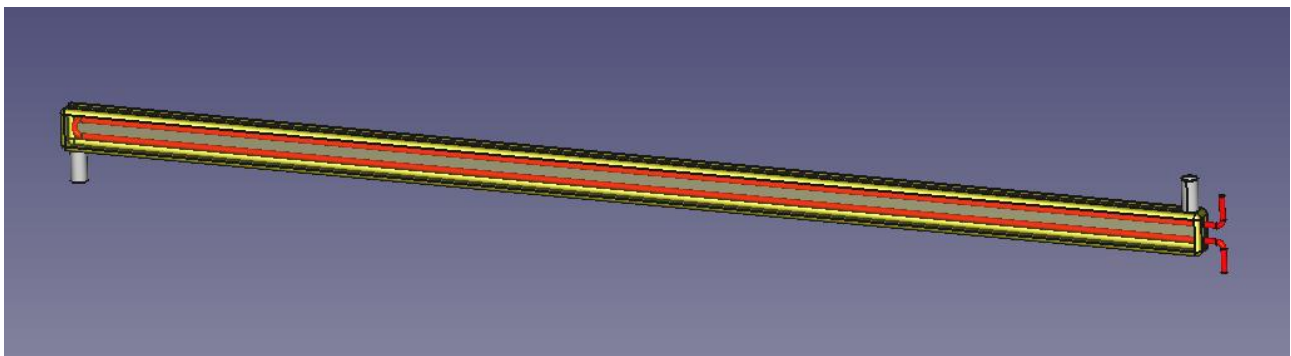
6 shell , 12 tubes

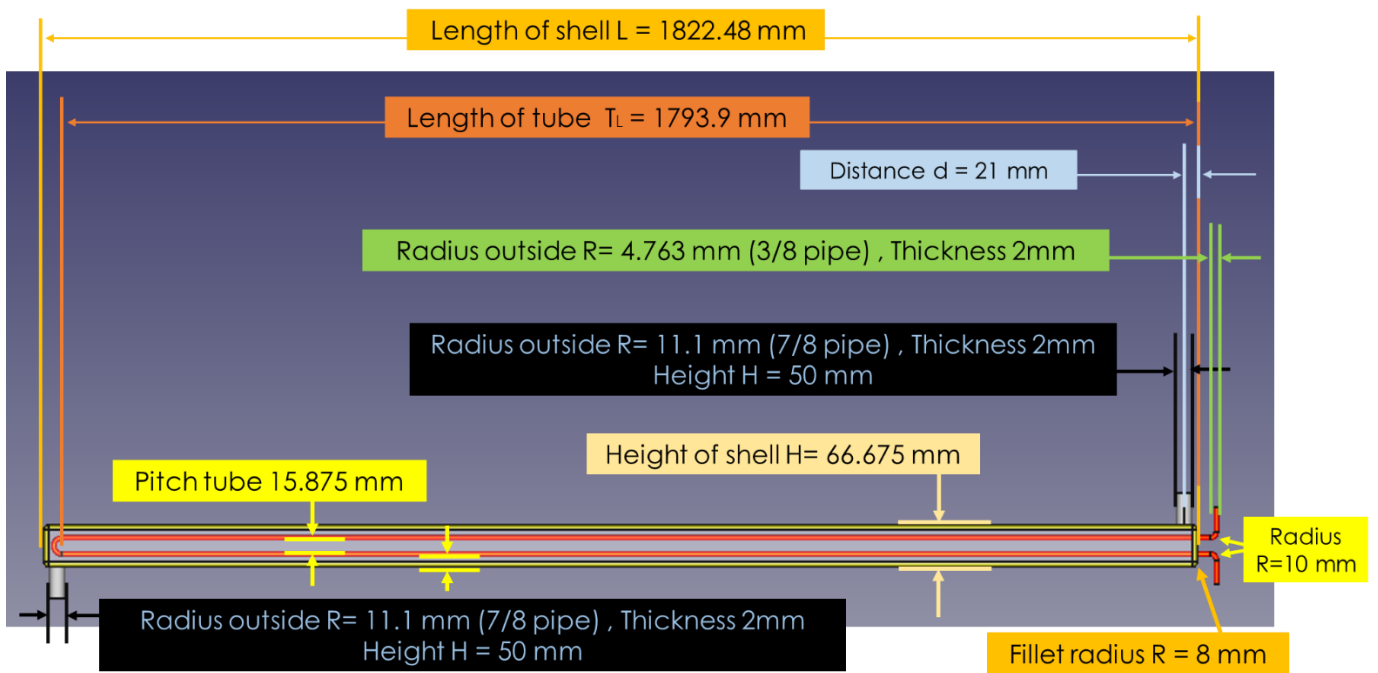
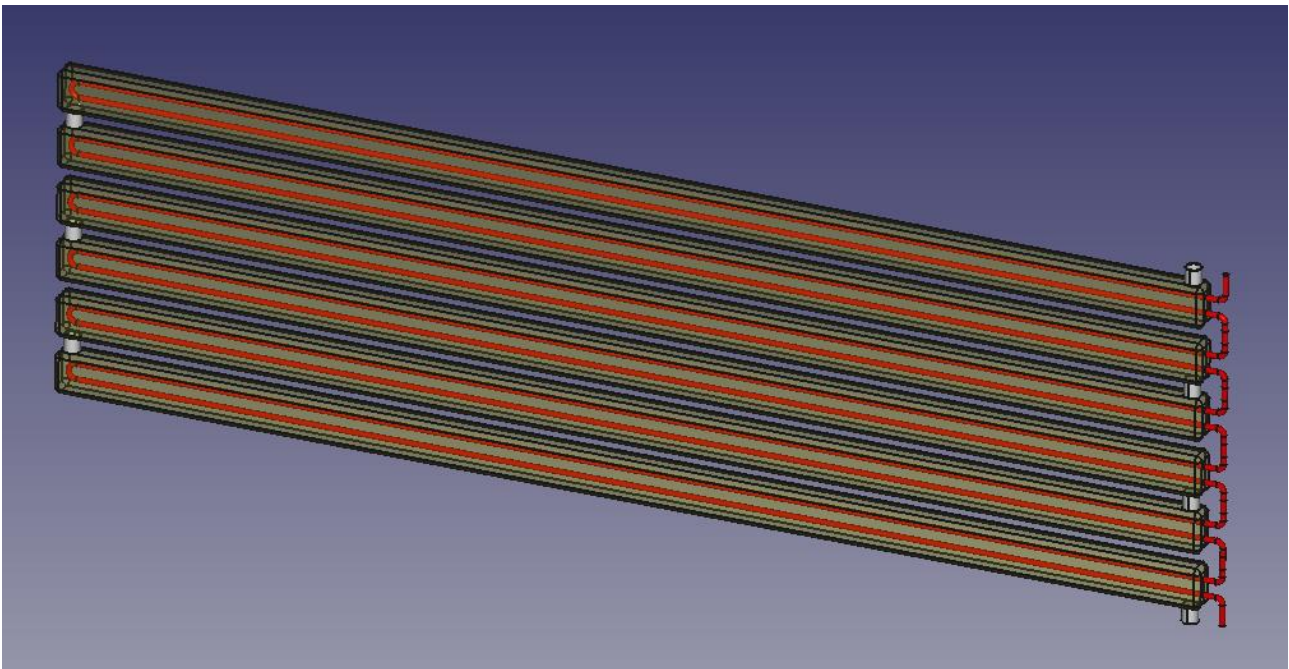
Shell – Cold side – N₂

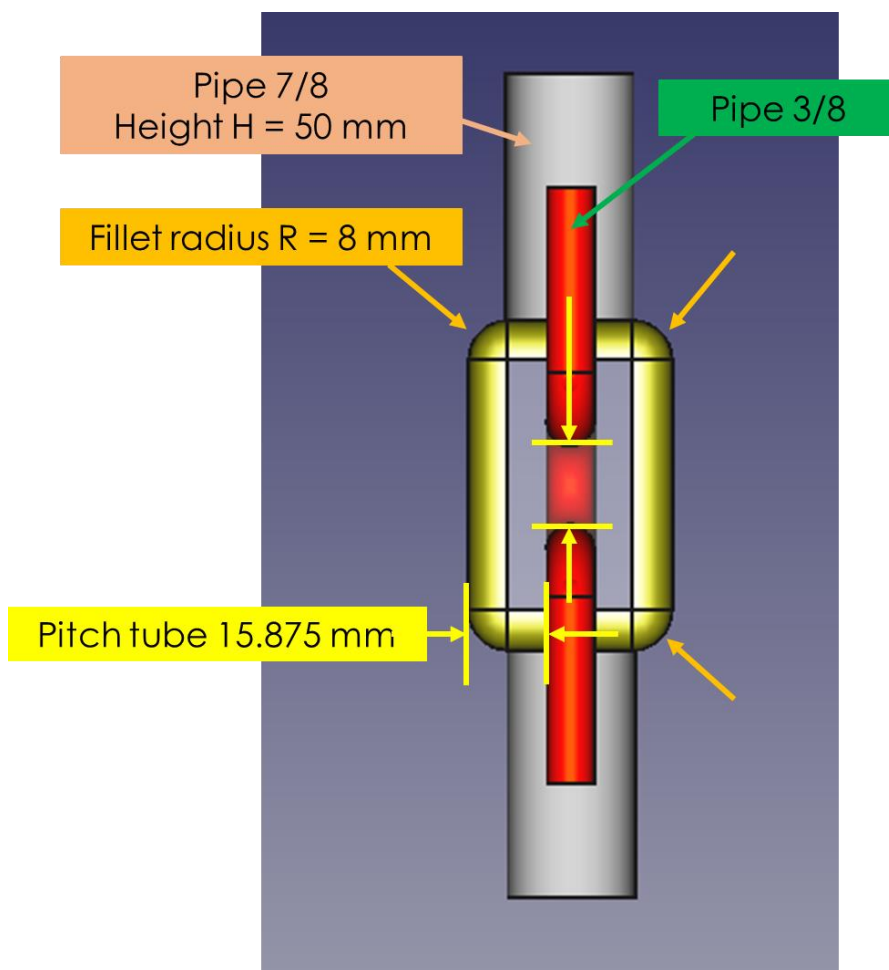
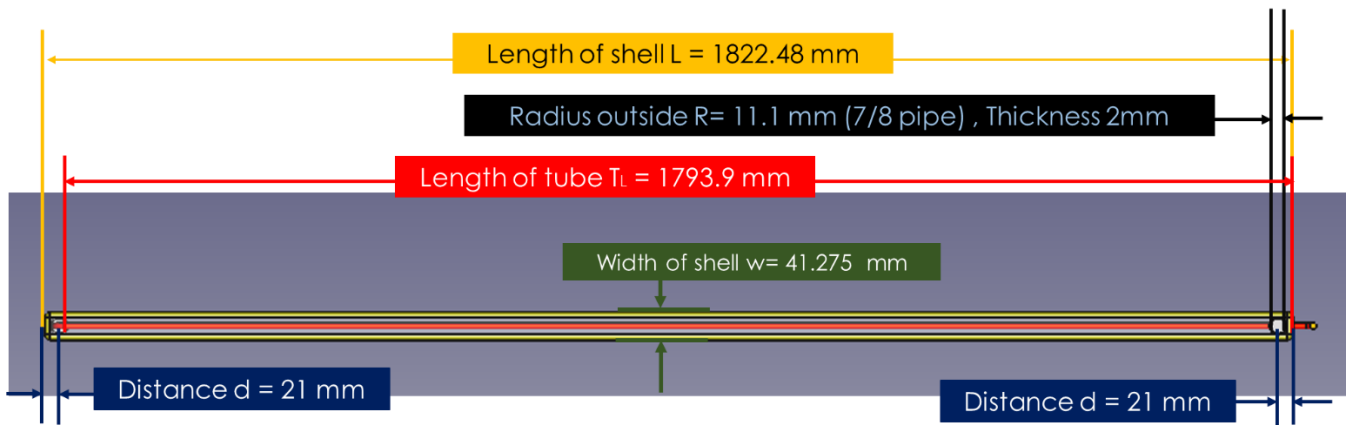
Tubes – Hot side – N₂

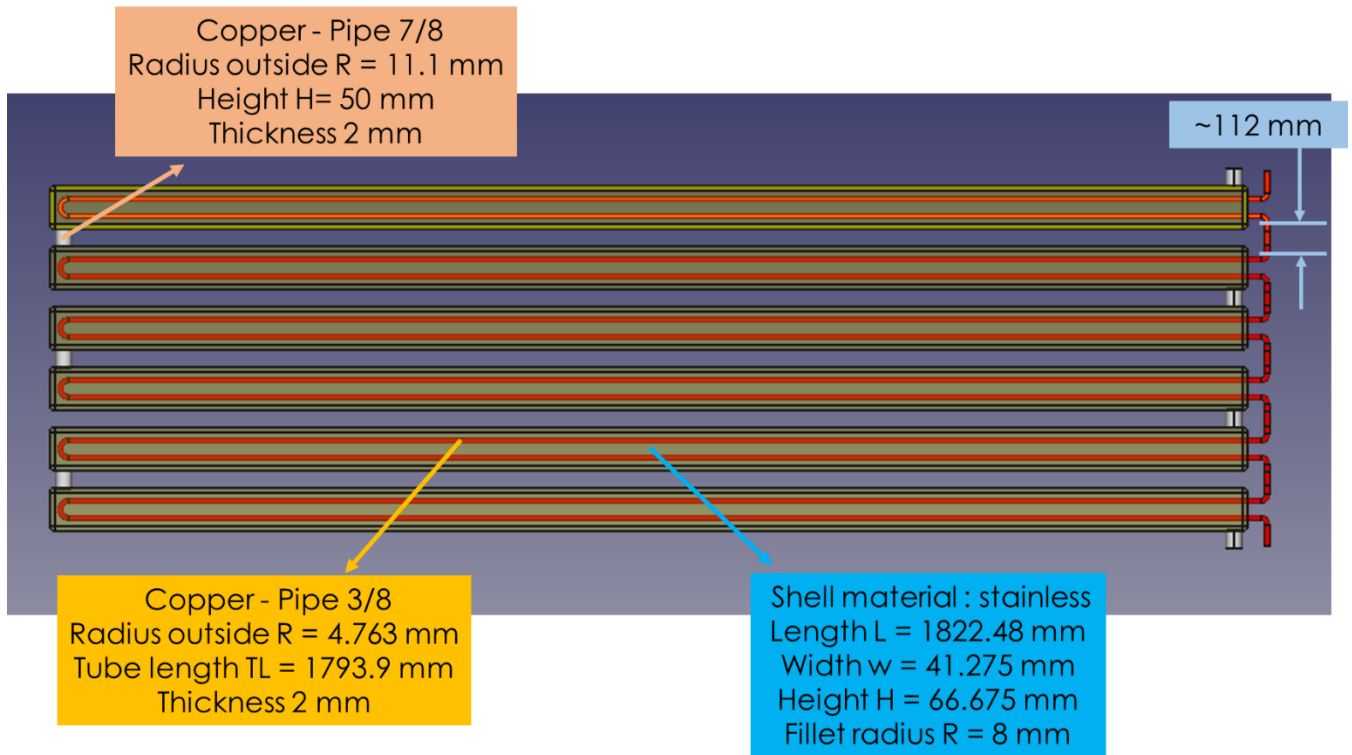

HX_N2-N2_ ONE SHELL.FCStd


HX_N2-N2.FCStd







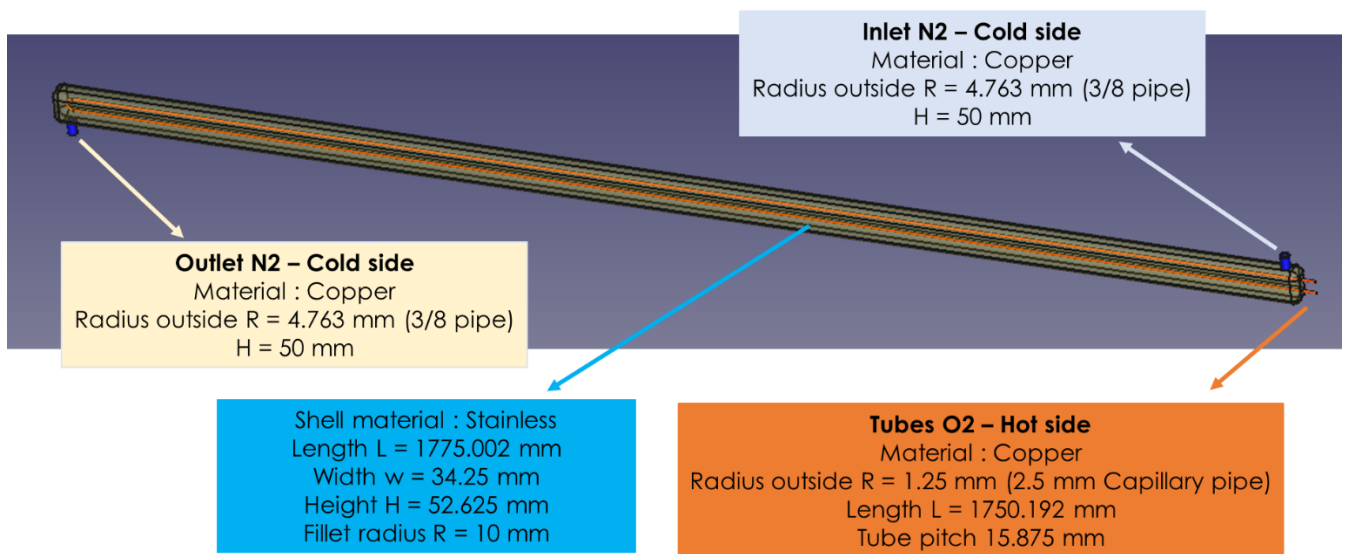


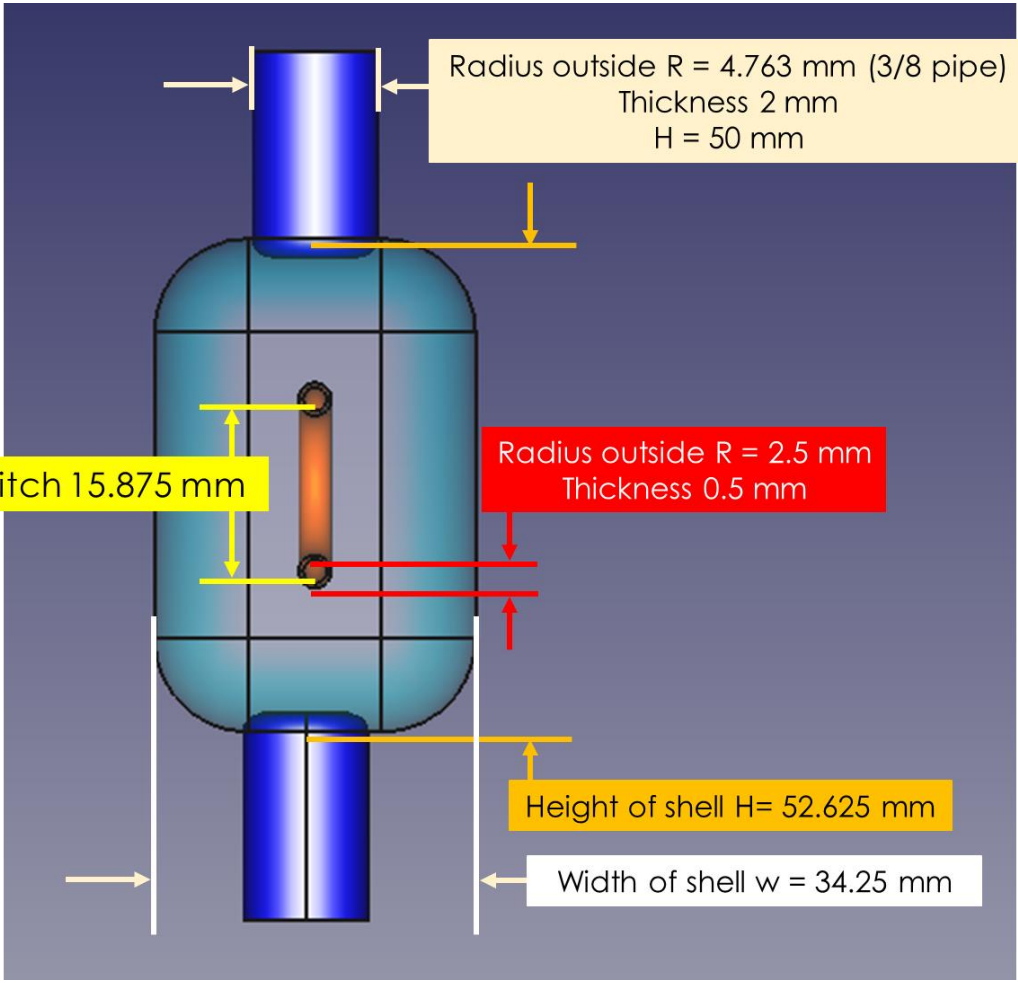
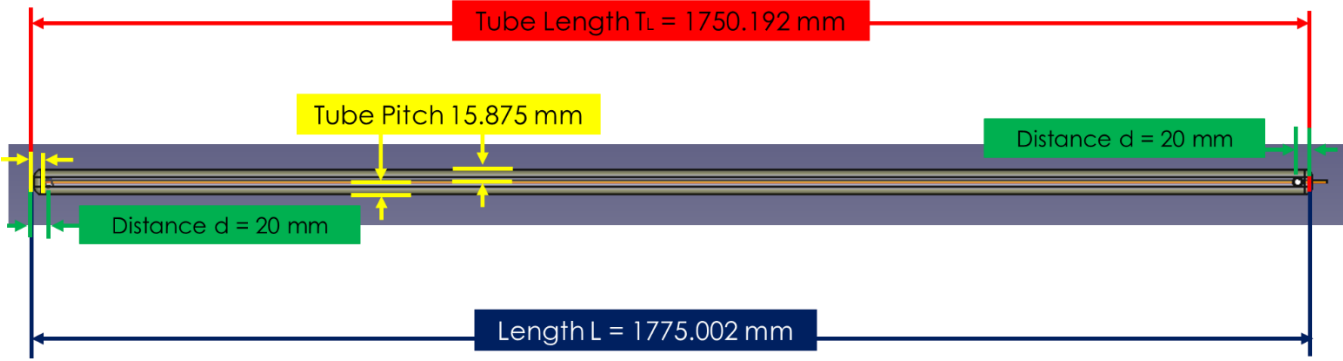
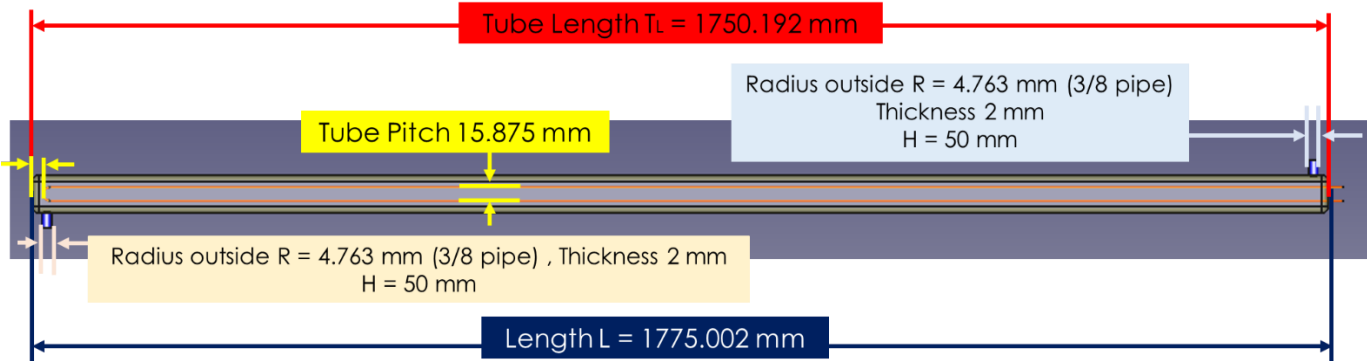
4.3 Heat exchanger design HX-N₂/O₂ [Main]

1 shell , 2 tubes

Shell – Cold side – N₂

Tubes – Hot side – O₂





4.4 Heat exchanger design HX-N₂/O₂ [2nd]

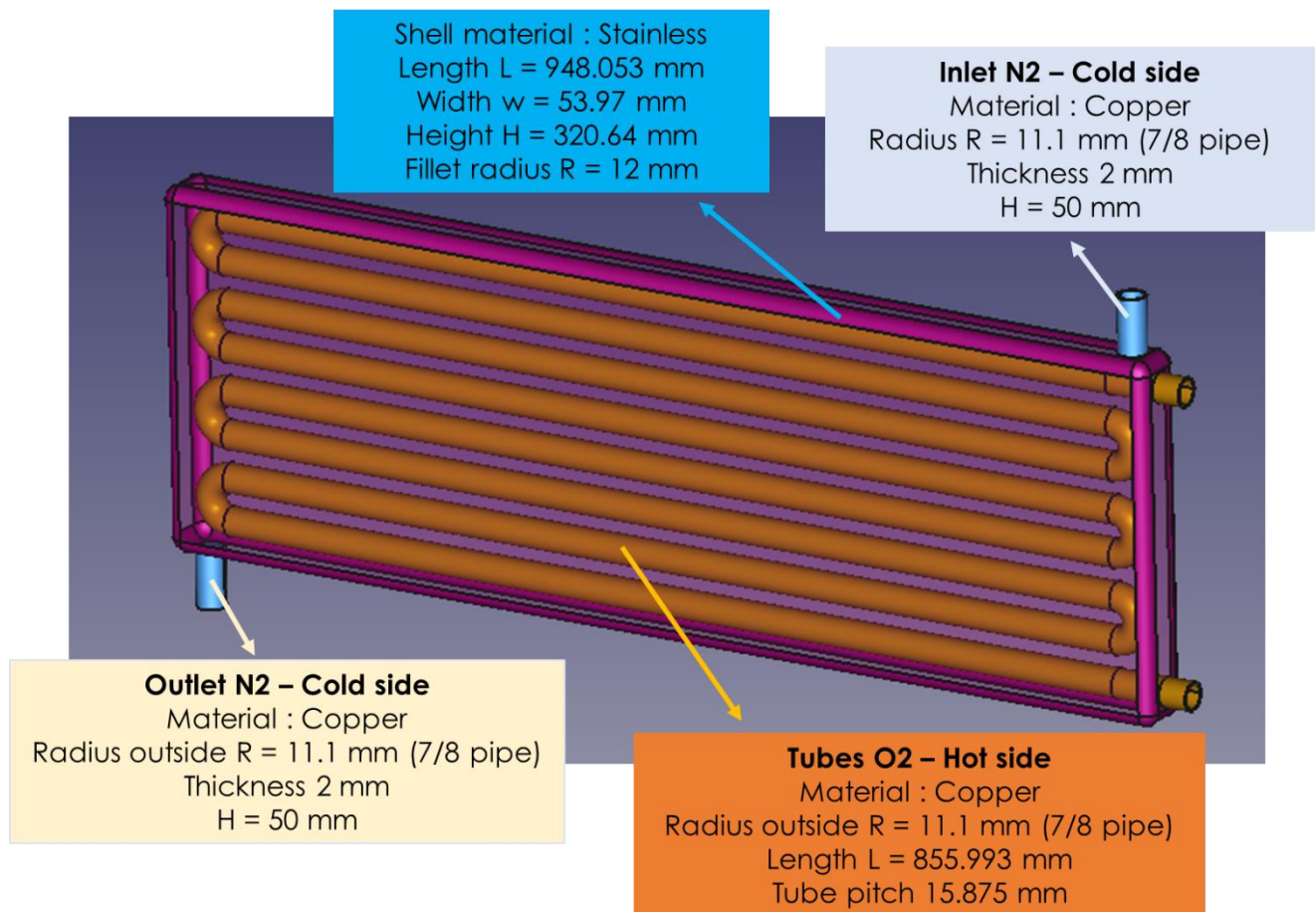
1 shell , 8 tubes

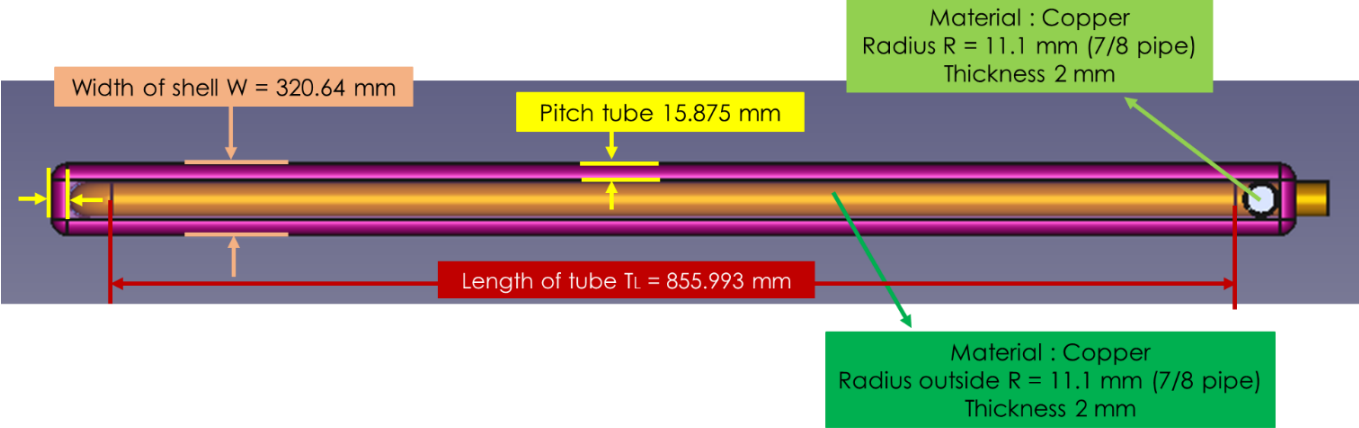
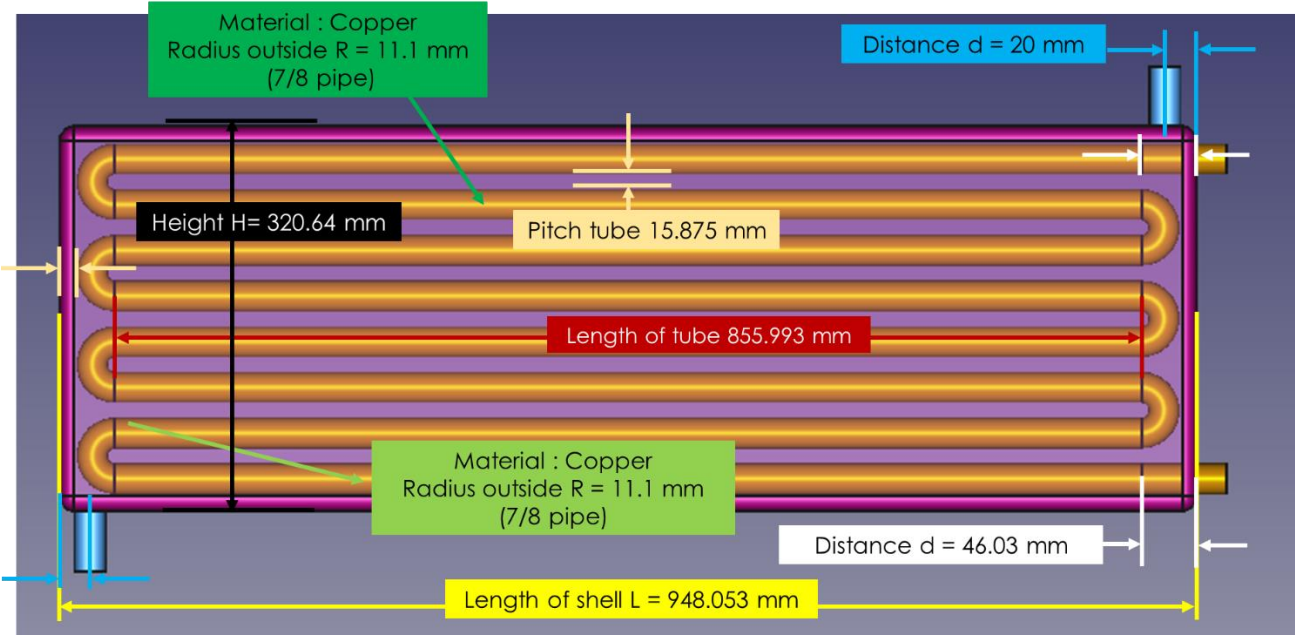
Shell – Cold side – N₂

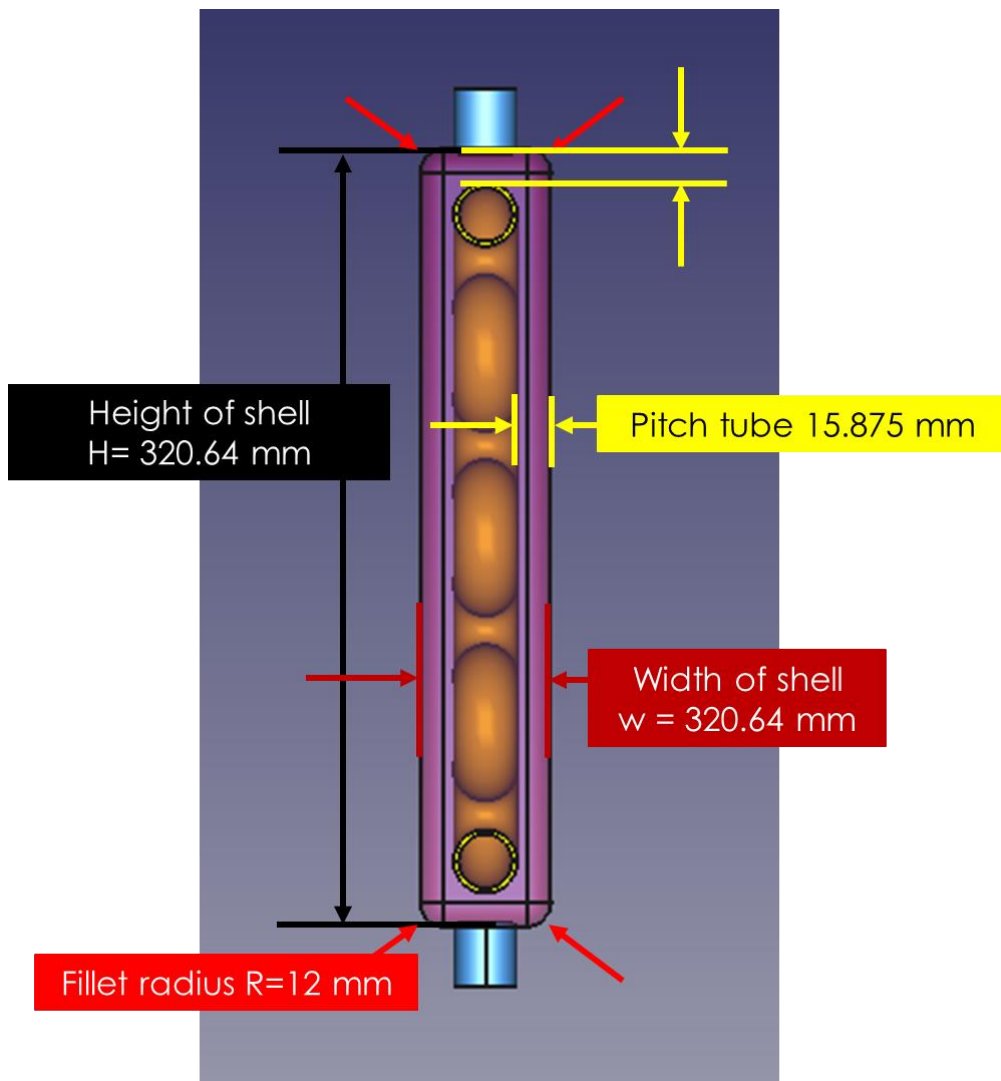
Tubes – Hot side – O₂



HX_N2-O2 (2nd).FCStd







4.5 Cooling design [Inside kelvinator]

$$\begin{aligned}
 Q_{\text{conv}} &= \dot{m} \cdot C_p \cdot (T_i - T_o) \\
 &= 25 \text{ kg/h} \cdot 1.088375 \text{ KJ/Kg.K} \cdot (335 - 195) \\
 &= 25/3600 \cdot 1.088375 \cdot 140 = 1.0575 \text{ KW} = 1057.5 \text{ W}
 \end{aligned}$$

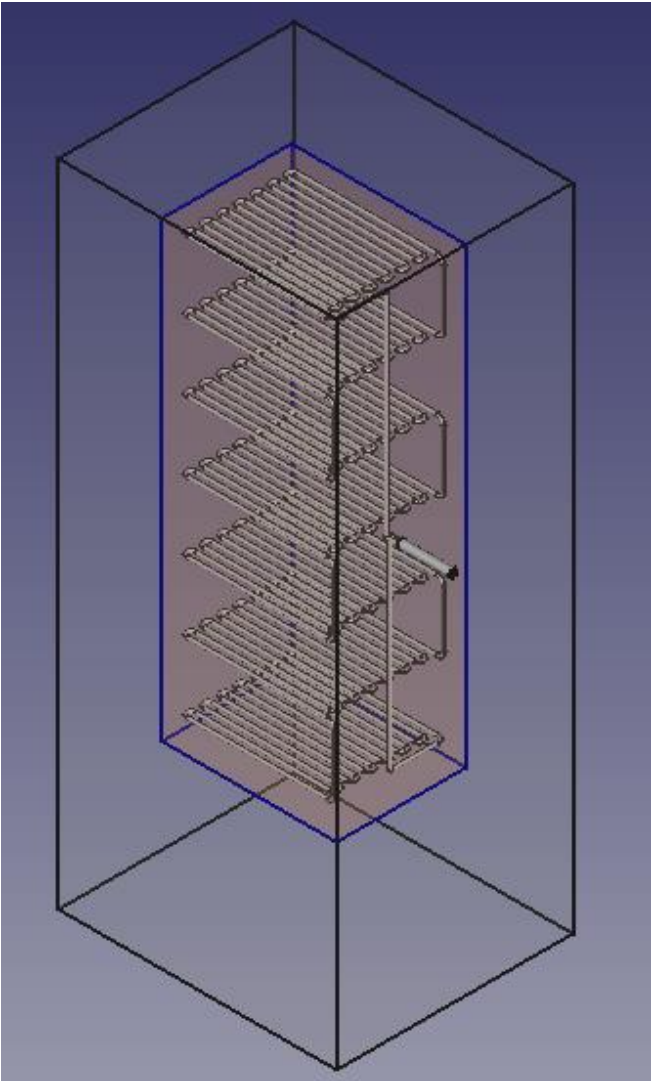
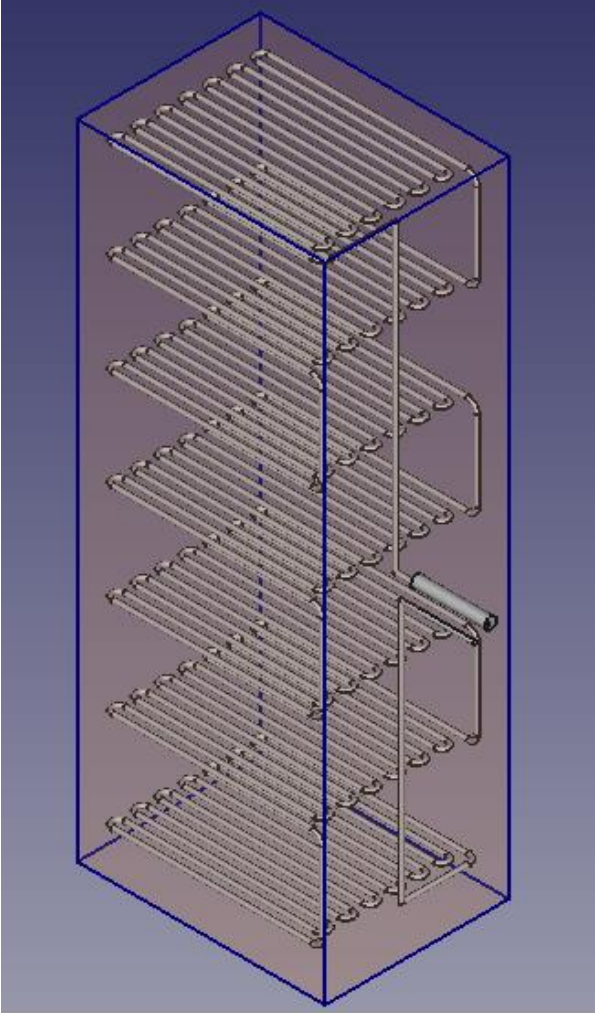
$$Q_{\text{conv}} = h \cdot A_s \cdot \text{LMTD} \quad \text{or} \quad \text{LMTD} = \frac{\Delta T_o - \Delta T_i}{\ln \left(\frac{\Delta T_o}{\Delta T_i} \right)} = 33.2$$

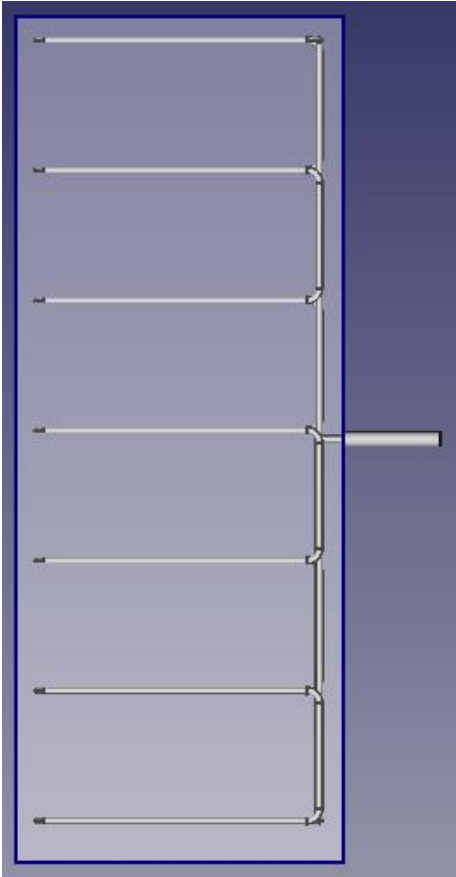
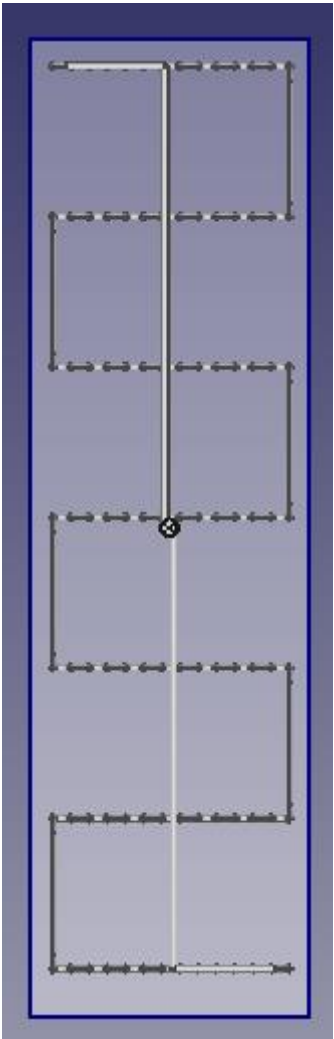
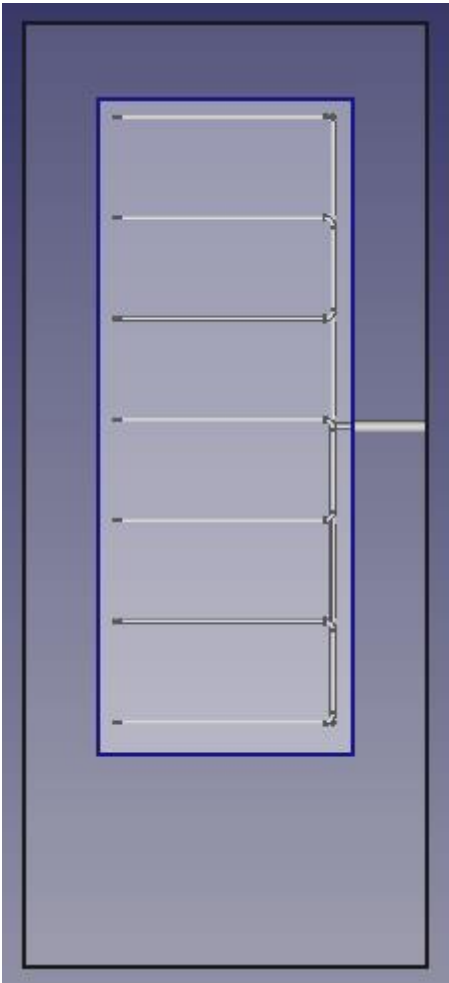
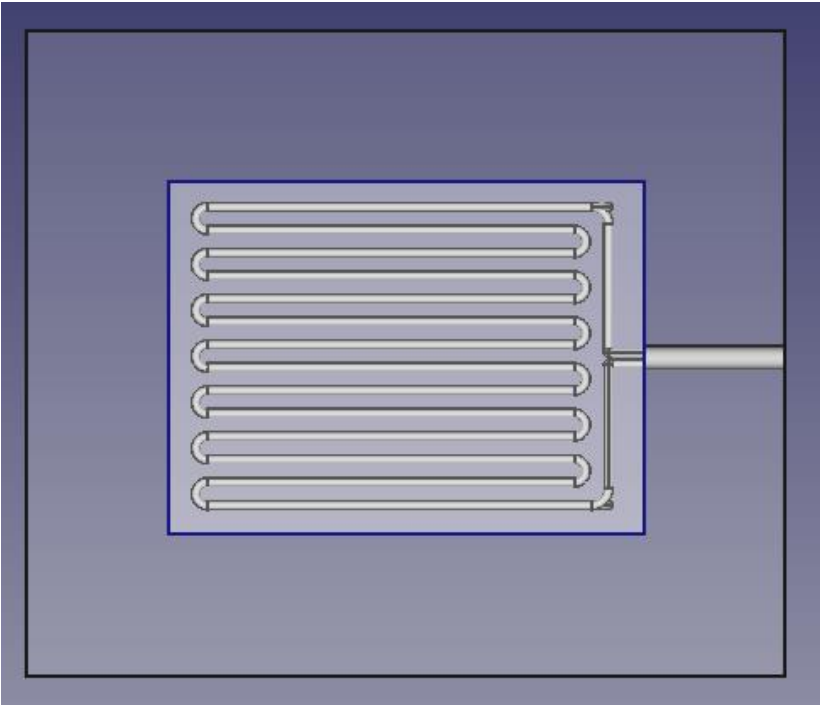
$$A_s = \frac{1057.5}{h \cdot 33.2} = \frac{1057.5}{25 \cdot 33.2} = 1.274 \text{ m}^2$$

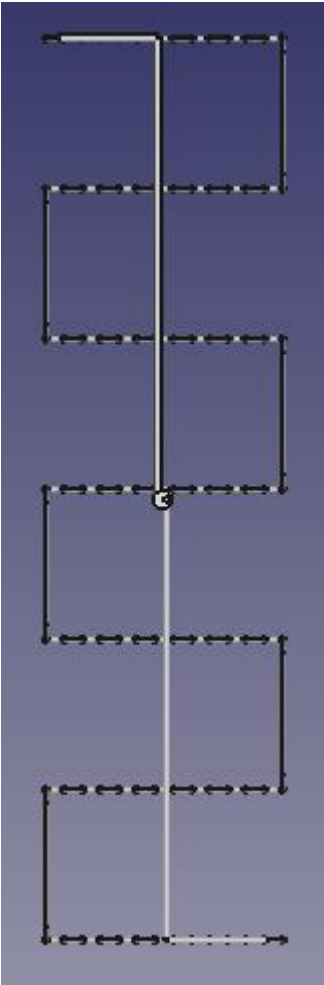
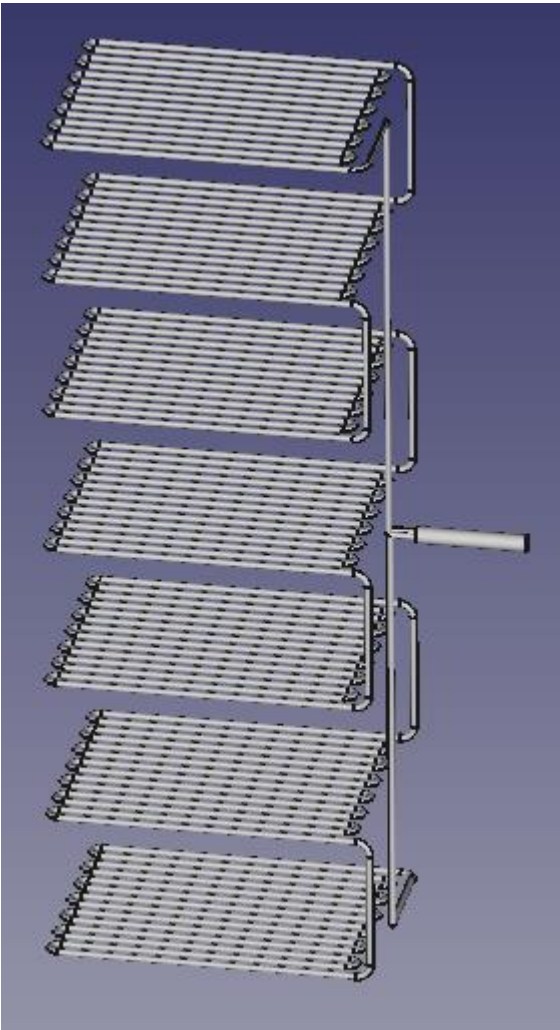
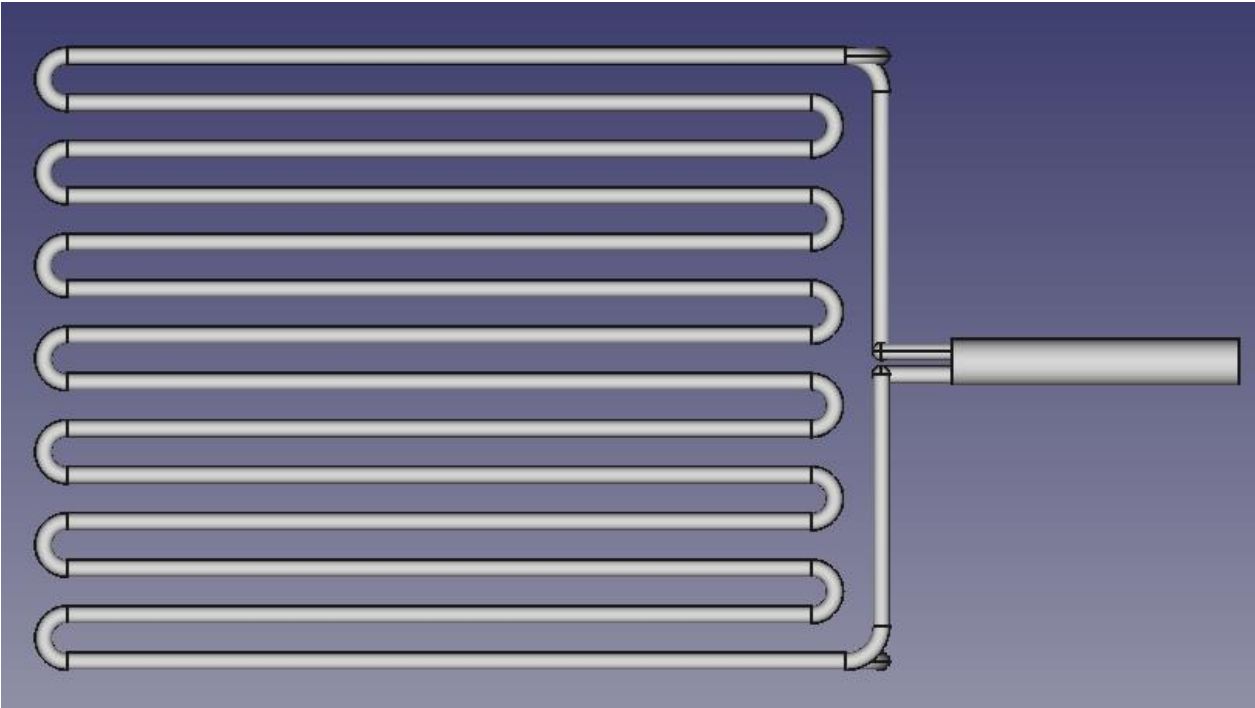
$$\text{Or } A_s = 2 \cdot \pi \cdot R \cdot h \rightarrow h = \frac{A_s}{2 \cdot \pi \cdot R} = \frac{1.274}{\pi \cdot 9.525 \cdot 10^{-3}} = 42.58 \text{ m}$$

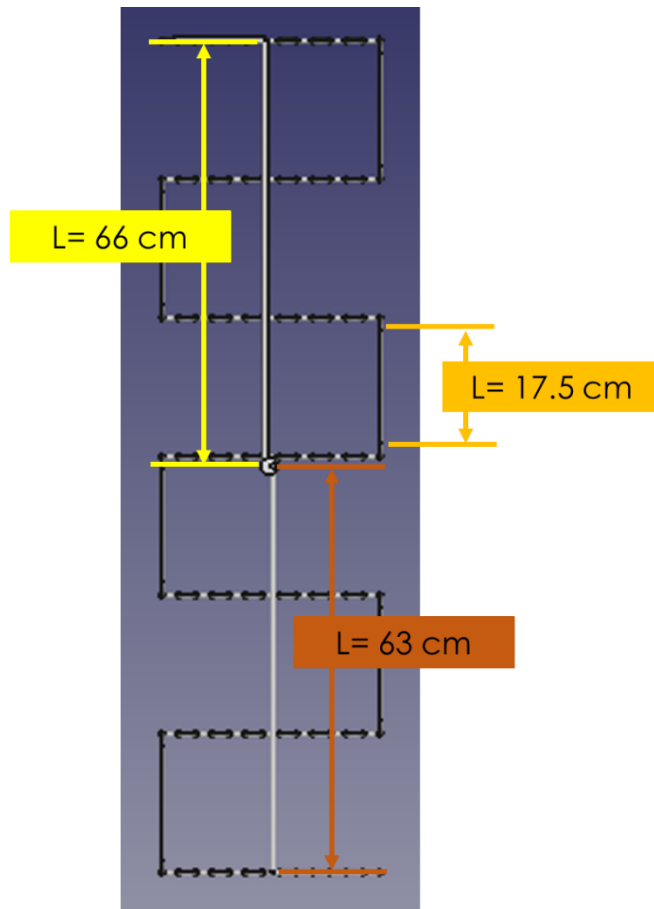
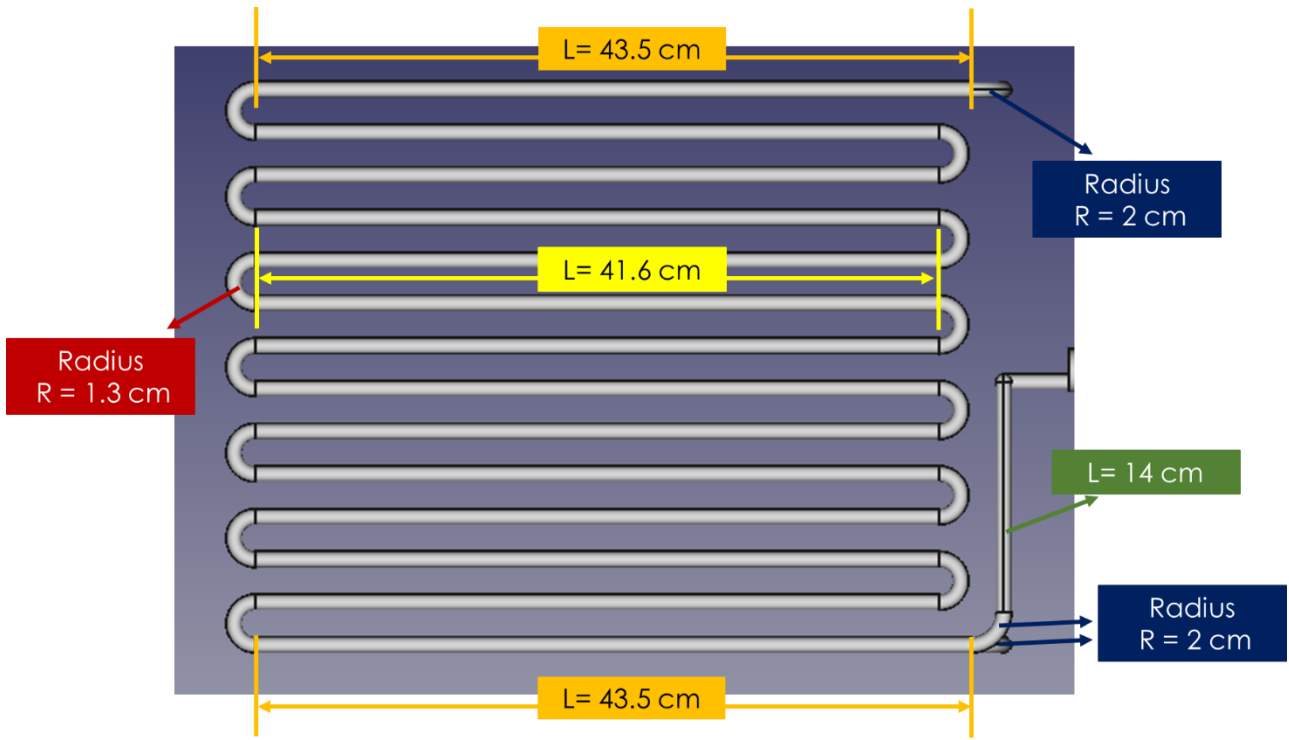
4.6 Cooling FreeCad design


COOLING.FCStd

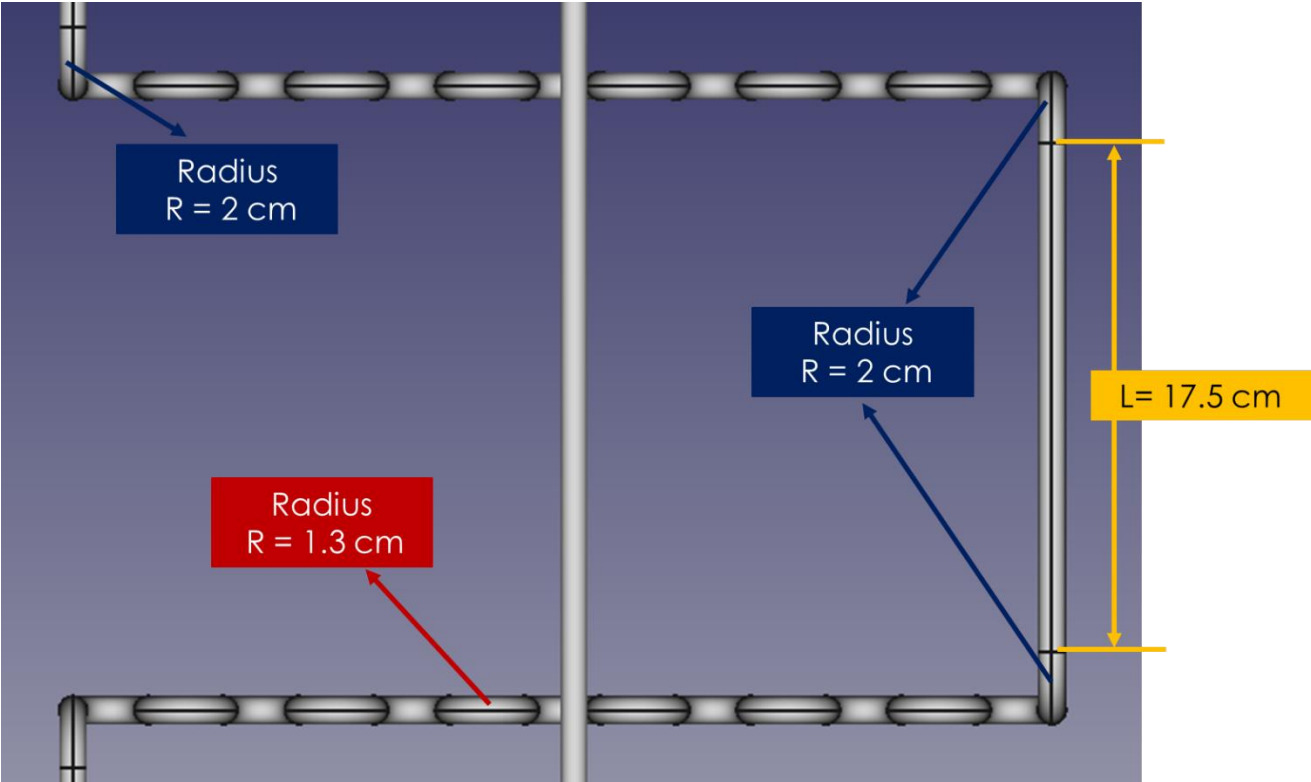








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5 Price of prototype components

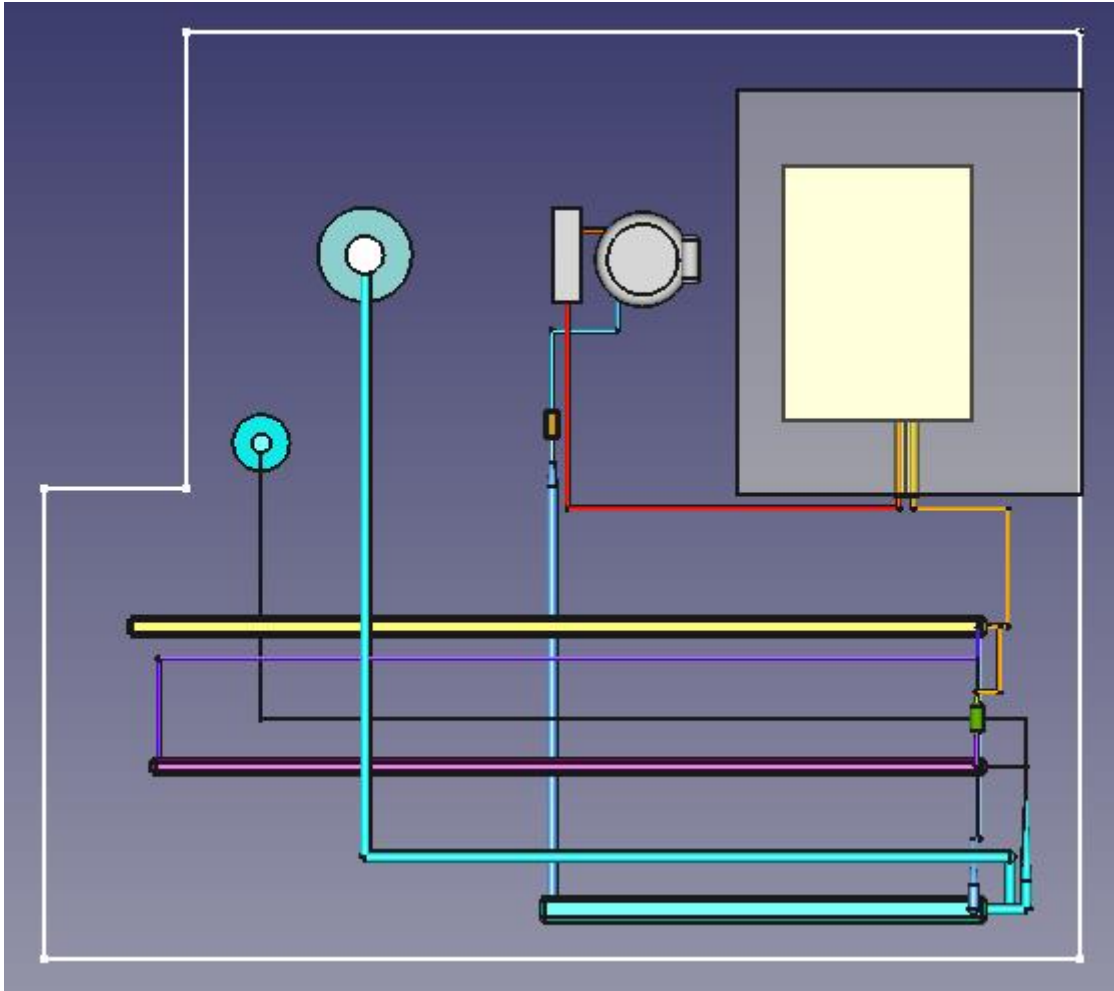
Components of prototype	Source	Characteristics	General price	# of piece	Total cost excluding hand cost	Notes	
Compressor	LR25B laboratory refrigerator	Press 2 bar to 15 bar	---	1	---		
Condenser	LR25B laboratory refrigerator	Air cooling	---	1	---		
Cooling	Kelvinator refrigerator	Copper pipes (3/8)	pipe (3/8) : 15 m / \$ 55	L= 43 m	\$ 157.70	Total pipe 3/8: L= 65.8 m , cost = \$ 241.3	
HX - N2/N2 (6 shells , 12 tubes)	Manufacture	Copper pipes (3/8)	pipe (3/8) : 15 m / \$ 55	L= 22.5 m (L= 3.63 m per shell)	\$ 27.50	Total capillaries copper pipes: L = 3.7 m , Cost = 111 000 L.L.	
		Copper pipes (7/8)	1.5 m / \$ 15 (or Roller 15 m , 140\$)	L= 0.6 m (L= 0.2 m per shell)	\$ 6.00	Total pipe 7/8: L= 8.2 m , Cost = \$ 82	
		Shell copper or stainless		Area = 2.4115 m2 (A = 0.402 m2 per shell)	17.4 - 26.1 \$ (2.9 - 4.35 \$/shell)		Total volume V = 0.003391912 Kg/m3 , Costs = (Stainless 38.2 \$, Steel 8.2 \$, Copper 287 \$)
		Expansion valve	Purphase	15 bar, 80 K	1	\$ 35.00	
HX - N2/O2 [main] (1 shell , 2 tubes)	Manufacture	Capillaries copper pipes (2.5 mm outside)	1 m / 30 000 L.L.	L= 3.7 m	L.L. 111 000		
		Copper pipes (3/8)	15 m / \$ 55	L= 0.1m	\$ 0.37		
		Shell copper or stainless		Area A = 0.3134 m2			
HX - N2/O2 [2nd] (1 shell , 8 tubes)	Manufacture	Copper pipes (7/8)	1.5 m / \$ 15 (or Roller 15 m , 140\$)	L= 7.4 m	\$ 102.00		
		Shell copper or stainless		Area A = 0.7457 m2			
Filter drier	Purphase	N2 gas, mass flow 25 Kg/hr		1	\$ 15.00		
Pressure valve	Purphase	Gas 15 bar		1			
Check valve	Purphase			1	\$ 10.00		
Thermal insulation materials	Purphase	Area per meter					
Cryometer	Purphase (not available)	Low than 80 K		5			
Solenoid valve	Purphase			1			
N2 gas	Purphase						
O2 gas	Purphase						
O2 gas tank	Purphase			1			

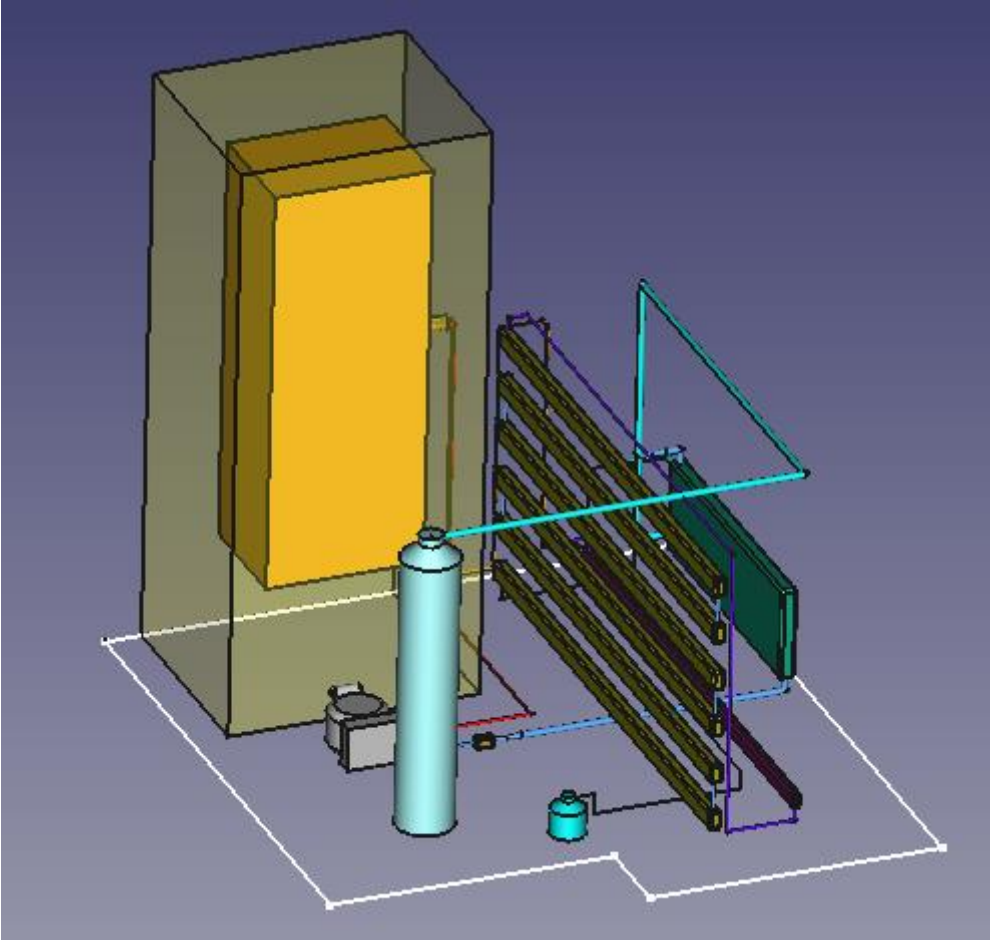
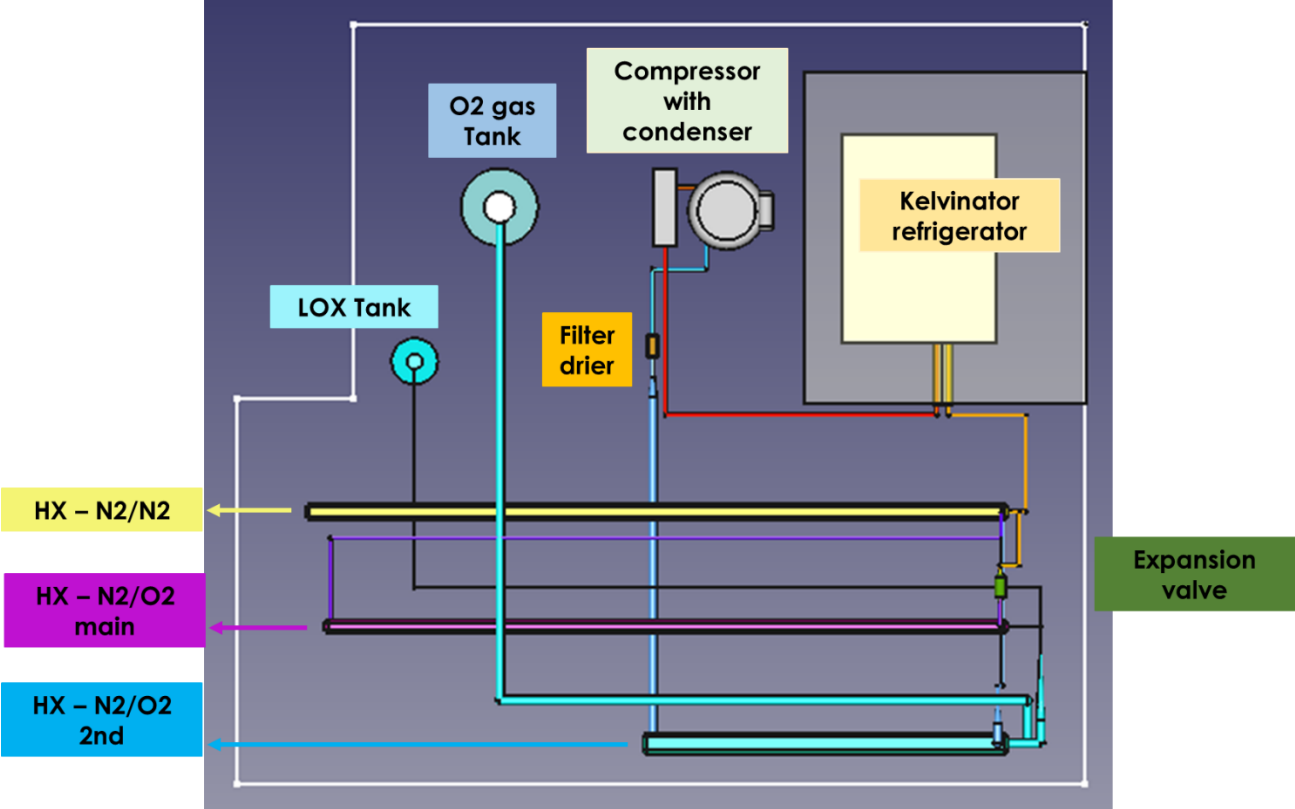
- General space of prototype is : L * W * H = 1.93 m * 2 m * 1.2 m (except height of kelvinator refrigerator = ~ 1.7 m)

		Stainless steel	Steel	Copper
Price		1 - 1.5 \$/Kg	100 - 300 \$/Ton	9.35 \$/Kg
Density		7500 Kg/m ³	8050 Kg/m ³	8.96 g/cm ³
HX-N ₂ /N ₂	Volume needed	0.002348004 m ³	0.002348004 m ³	2348.004 cm ³
	Mass	17.61 Kg	18.90 Kg	21.038 Kg
	Cost	17.61 - 26.415 \$	1.89 - 5.67 \$	196.71 \$
HX-N ₂ /O ₂ main	Volume needed	0.000305524 Kg/m ³	0.000305524 Kg/m ³	305.524 Kg/cm ³
	Mass	2.29 Kg	2.46 Kg	2.737 Kg
	Cost	2.29 - 3.435 \$	0.246 - 0.738 \$	25.6 \$
HX-N ₂ /O ₂	Volume needed	0.000738384 Kg/m ³	0.000738384 Kg/m ³	738.384 Kg/cm ³
	Mass	5.54 Kg	5.94 Kg	6.91 Kg
	Cost	5.54 - 8.31 \$	0.594 - 1.782 \$	64.61 \$
Total volume		0.003391912 Kg/m ³	0.003391912 Kg/m ³	0.003391912 Kg/m ³
Total mass		25.44 Kg	27.305 Kg	30.685 Kg
Total cost		25.44 - 38.16 \$	2.731 - 8.192 \$	286.91 \$

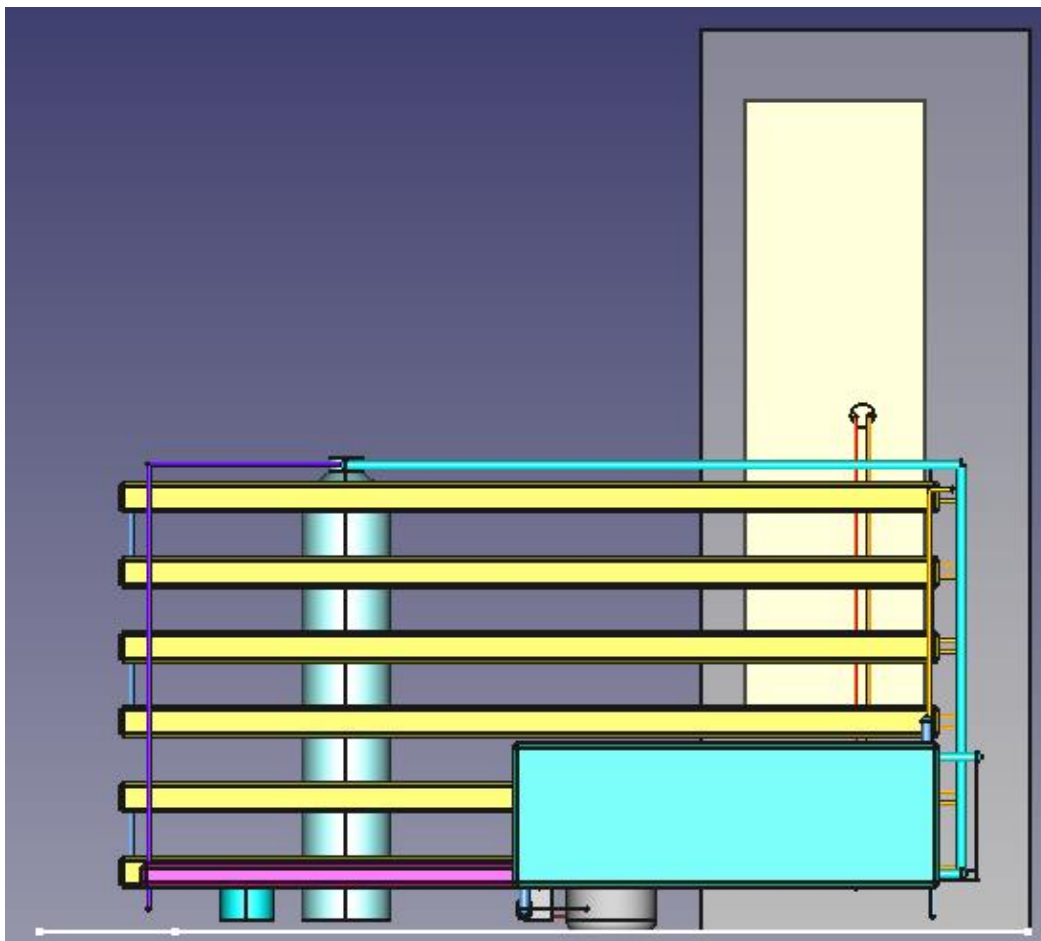
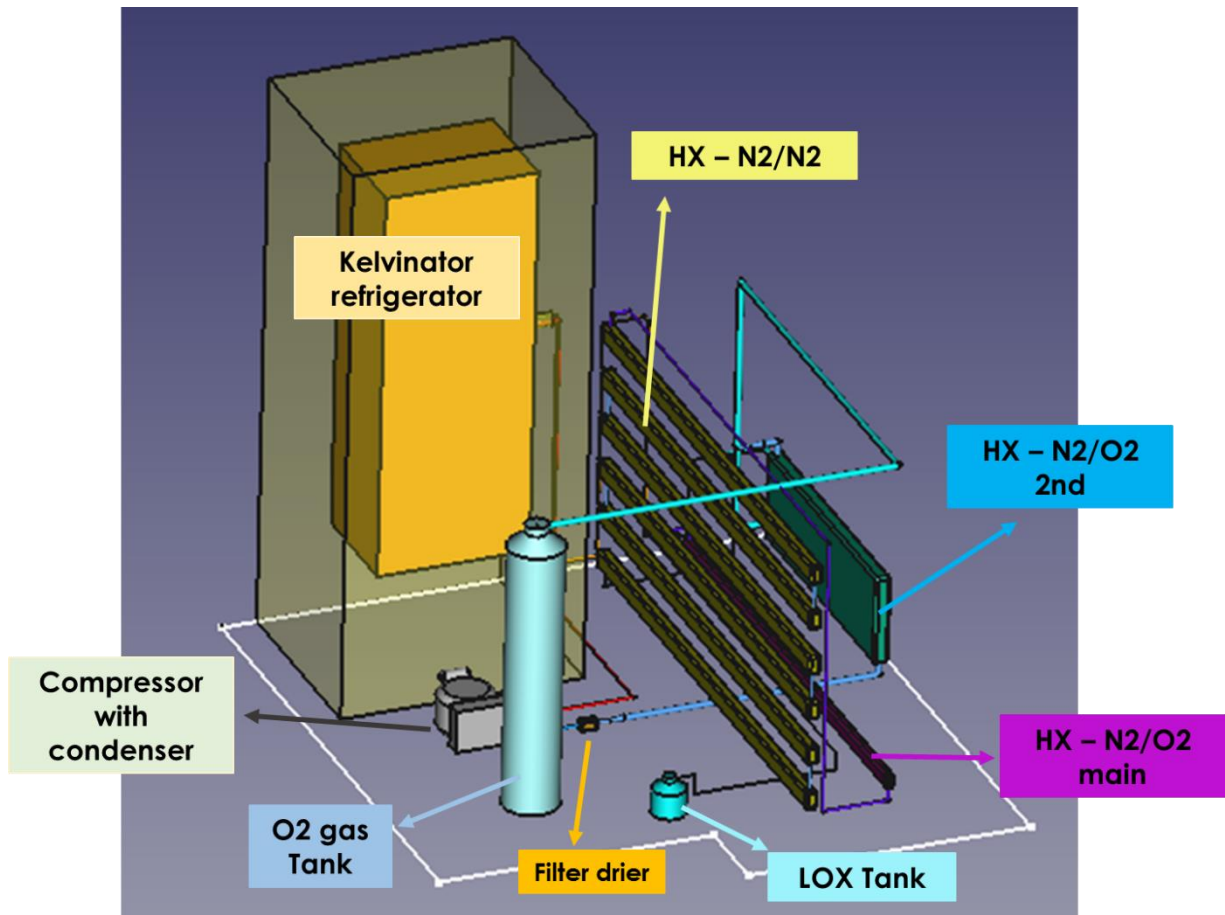
6 Real layout design of prototype in AECENAR Facility

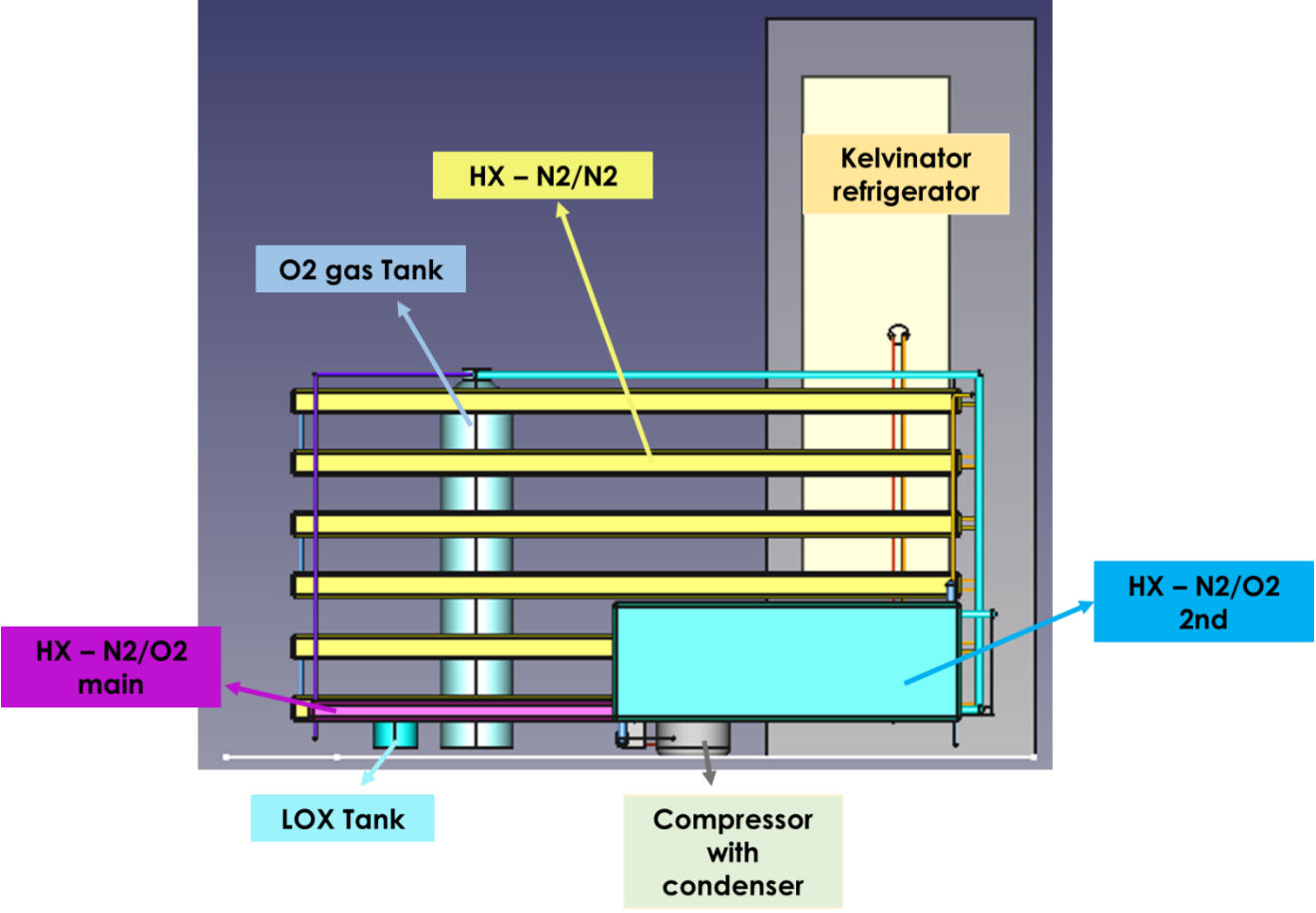
real prototype.FCStd





Real layout design of prototype in AECENAR Facility





Real layout design of prototype in AECENAR Facility





Real layout design of prototype in AECENAR Facility



7 Real design of cooling (inside kelvinator refrigerator)



In this evaporator, we have 20 pipes (size 3/8, length $L \approx 32$ cm) with 19 tees (Radius $R = 1.5$ cm)

$$\text{So: } (32\text{cm} \times 20 \text{ pipes}) + \left(\frac{2 \times \pi \times 1.5\text{cm} \times 180^\circ}{360} \times 19 \text{ tees} \right) = 729.535 \text{ cm} = \sim 7.29 \text{ m}$$

Real design of cooling (inside kelvinator refrigerator)

The length required for cooling was previously calculated : 42.58 m \approx 43 m

43 m / 7.29 m = 5.98 floor \rightarrow we need 6 floor for cooling

But the measurements of evaporator are not accurate so we will use 7 floors or pieces of this evaporator

Price of one piece of evaporator = \sim 200 000 L.L.

Total price excluding hand cost = \sim 200 000 x 7 = \sim 1 400 000 L.L.

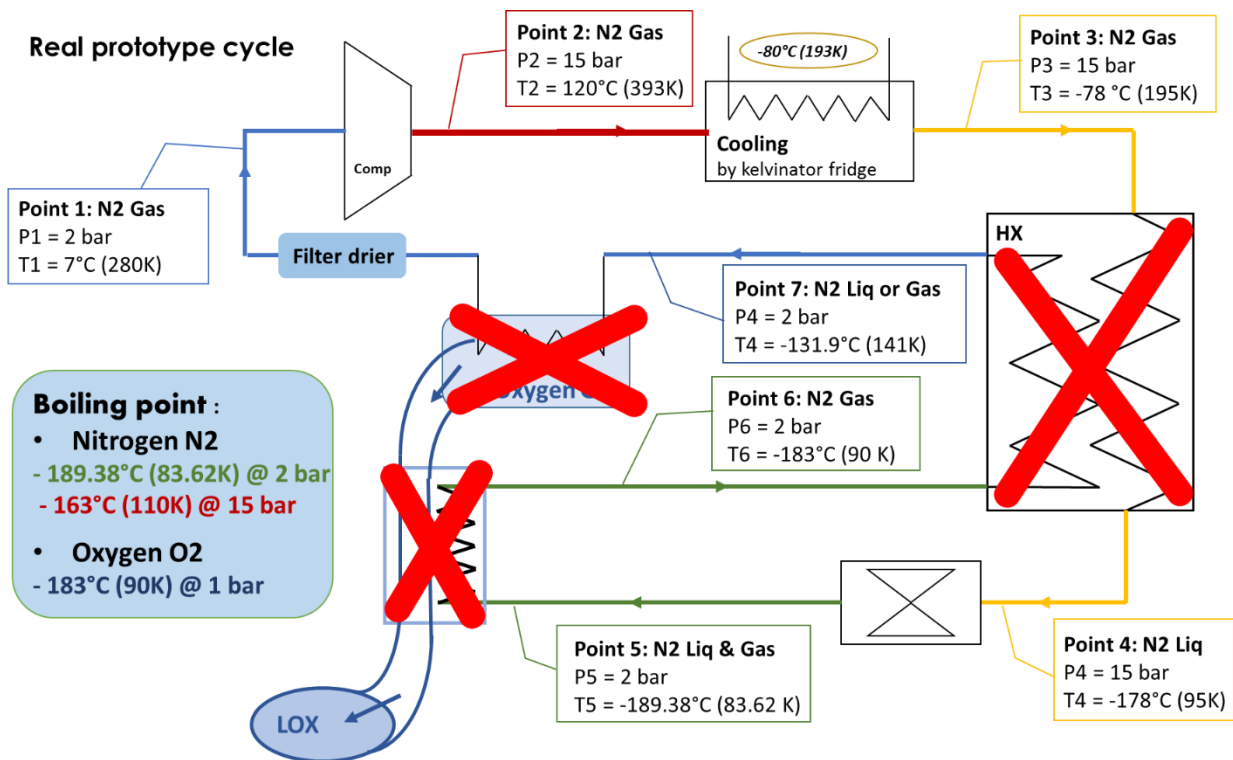
8 First experiment (Expr #1)

The first experiment (Expr #1) aims to:

- 1- Compressor operation test with nitrogen gas instead of R-134a,
- 2- Make sure that the Kelvinator refrigerator is running correctly
- 3- Ensure that the expansion valve is compatible with the design.

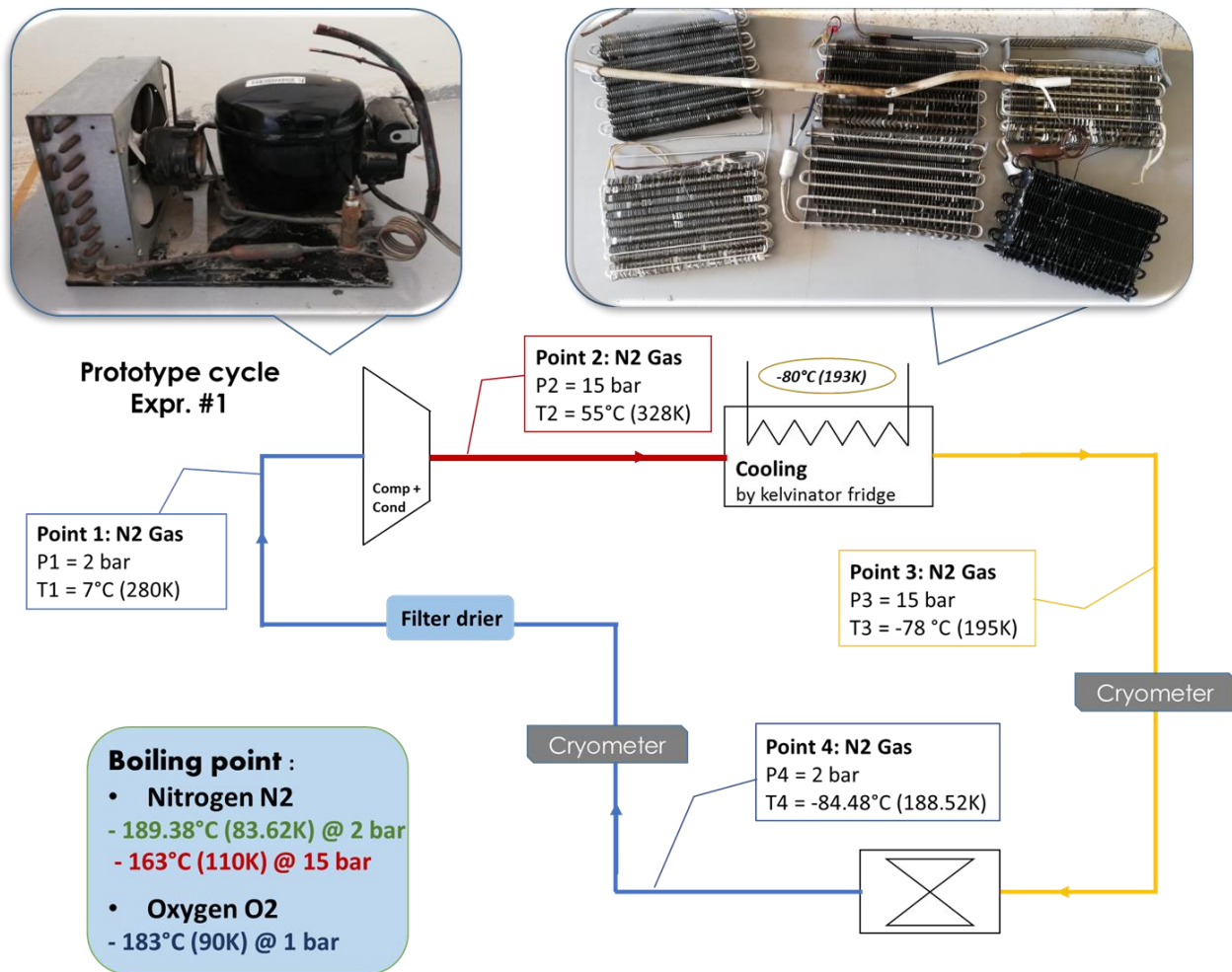
Therefore, the three heat exchangers (HX-N₂/N₂, HX-N₂/O₂ main, HX-N₂/O₂ 2nd) will be excluded from this experiment.

In this experiment, the oxygen will not be liquefied, but only the components will be tested and designed to ensure the proper functioning of the refrigeration cycle.



The first experiment consists of a simple cycle consisting of a compressor (LR25B Laboratory) with a condenser, cooling through a Kelvinator refrigerator, and an expansion valve (taken from an LR25B Laboratory refrigerator).

First experiment (Expr #1)



The components that must be provided to carry out this experiment:

- 1- Filling the design with nitrogen gas, immediately before the pump.
- 2- Covering the design with a thermal insulation material to maintain the temperature of the refrigeration cycle,
- 3- The presence of a thermometer (below -100°C (173 K)) to measure the cooling outlet (inlet of the expansion valve) and the outlet of the expansion valve,
- 4- Also, a weather thermometer (from -10°C to 20°C (263 K to 293 K)) to measure the temperature of the compressor inlet.

For **the safety of the compressor**:

- In the **first hour of operation**, a 5-minute break must be taken for the compressor every 15 minutes of operation, in order to avoid an explosion of the compressor or one of the designed cables.
- Also, the compressor must **not run for more than two hours** in a row.
- Also, **cold nitrogen gas must be entered into the compressor** to reduce the speed of nitrogen flow, in addition to its role in cooling the compressor.

During this experiment (Expr. #1), the **amount of nitrogen gas filled** to the cycle, the **time of the experiment**, the **temperature reached** by the refrigeration cycle, the **pressure during operation** will be calculated.

Literature

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